

OPERATOR

Company: BLACK DIAMOND OIL, INC.
 Address: P.O. BOX 641
 HAYS, KS 67601

Contact Geologist: KENNETH VEHIGE
 Contact Phone Nbr: (785) 625-5891
 Well Name: LOGAN NW #1
 Location: E2 NE NW SE Sec. 24 - 3S - 21W
 API: 15-137-20725-00-00
 Pool:
 State: KANSAS
 Field: UNNAMED
 Country: USA

Scale 1:240 Imperial

Well Name: LOGAN NW #1
 Surface Location: E2 NE NW SE Sec. 24 - 3S - 21W
 Bottom Location:
 API: 15-137-20725-00-00
 License Number: 7076
 Spud Date: 12/2/2014 Time: 5:15 PM
 Region: NORTON COUNTY KANSAS
 Drilling Completed: 12/7/2014 Time: 10:22 PM
 Surface Coordinates: 2310' FSL & 1600' FEL
 Bottom Hole Coordinates:
 Ground Elevation: 2196.00ft
 K.B. Elevation: 2201.00ft
 Logged Interval: 3100.00ft To: 3770.00ft
 Total Depth: 3770.00ft
 Formation: LANSING - KANSAS CITY
 Drilling Fluid Type: FRESH WATER / CHEMICAL GEL

SURFACE CO-ORDINATES

Well Type: Vertical
 Longitude: -99.6329161
 Latitude: 39.7765756
 N/S Co-ord: 2310' FSL
 E/W Co-ord: 1600' FEL

LOGGED BY

Company: BIG CREEK CONSULTING, INC.
 Address: 1909 MAPLE
 ELLIS, KS 67637
 Phone Nbr: (785) 259-3737
 Logged By: Geologist Name: JEFF LAWLER

CONTRACTOR

Contractor: WW DRILLING, LLC
 Rig #: 6
 Rig Type: MUD ROTARY
 Spud Date: 12/2/2014 Time: 5:15 PM
 TD Date: 12/7/2014 Time: 10:22 PM
 Rig Release: 12/10/2014 Time: 3:00 AM

ELEVATIONS

K.B. Elevation: 2201.00ft Ground Elevation: 2196.00ft
 K.B. to Ground: 5.00ft

NOTES

THE LOGAN NW #1 WAS A RELATIVE WILDCAT WELL WITH THE NEAREST WELLS DRILLED APPROXIMATELY 2 MILES IN ALL DIRECTIONS. THE LOGAN NW #1 RAN HIGH TO SURROUNDING WELLS AND CARRIED SHOWS AND POROSITY DEVELOPMENT THROUGHOUT. SIX DRILL STEM TESTS WERE TAKEN. DRILL STEM TESTS TWO THROUGH SIX HAD SEVERE TO PARTIAL PLUGGING THROUGHOUT THE FLOW PERIODS THAT IS VISABLE ON THE DST CHART INCLUDED IN THE REPORT. AFTER DRILL STEM TEST FIVE A DIFFERENT HYDRAULIC TOOL WAS SWITCHED OUT. THERE WAS PARTIAL PLUGGING ON DRILL STEM TEST SIX BUT WAS CONCLUDED AS A VALID TEST. WITH THE LACK OF ECONOMICAL RECOVERY ON ALL OF THE DRILL

CONCLUDED AS A VALID TEST. DUE TO THE LACK OF FLOW ON ALL OF THE LOGAN NW #1 STEM TESTS IT WAS DECIDED TO PLUG AND ABANDON THE LOGAN NW #1.

RESPECTFULLY SUBMITTED,
JEFF LAWLER

WELL COMPARISON SHEET

| FORMATION | LOGAN NW #1 | | | | | | | | BLACK DIAMOND OIL, INC. | | | | NORTHERN ORDANCE | | | | JONES, SHELburne, & FARMER | | | | | | | |
|---------------|---------------------|-------------|-------|-------|--------------------|-------|-------|-------|-------------------------|-------|-------|-------|------------------|-------|-------|-------|----------------------------|-------|-------|-------|-------|-------|-------|--|
| | ARLENE MULDER #1-26 | | | | SCHEMPER #1 | | | | PERRY #1 | | | | SMITH #1 | | | | | | | | | | | |
| | NW SW SE NW 26-3-21 | | | | NESW NE SW 20-2-20 | | | | SW SW 20-320 | | | | SW SW NE 15-3-21 | | | | | | | | | | | |
| | KB | 2201 | GL | 2196 | KB | 2275 | | | KB | 2165 | | | KB | 2195 | | | KB | 2313 | | | | | | |
| | LOG TOPS | SAMPLE TOPS | LOG | LOG | SMPL. | LOG | LOG | SMPL. | LOG | LOG | SMPL. | LOG | LOG | SMPL. | LOG | LOG | SMPL. | LOG | LOG | SMPL. | | | | |
| DEPTH | DATUM | DEPTH | DATUM | DEPTH | DATUM | CORR. | CORR. | DEPTH | DATUM | CORR. | CORR. | DEPTH | DATUM | CORR. | CORR. | DEPTH | DATUM | CORR. | CORR. | DEPTH | DATUM | CORR. | CORR. | |
| ANHYDRITE TOP | 1854 | 347 | 1857 | 344 | 1953 | 322 | + 25 | + 22 | 1811 | 354 | - 7 | - 10 | 1843 | 352 | - 5 | - 8 | 2011 | 302 | + 45 | + 42 | | | | |
| BASE | 1879 | 322 | 1882 | 319 | 1978 | 297 | + 25 | + 22 | 1836 | 329 | - 7 | - 10 | | | | | | | | | | | | |
| TOPEKA | 3220 | -1019 | 3219 | -1018 | 3301 | -1026 | + 7 | + 8 | 3187 | -1022 | + 3 | + 4 | 3224 | -1029 | + 10 | + 11 | | | | | | | | |
| HEEBNER SHALE | 3423 | -1222 | 3426 | -1225 | 3499 | -1224 | + 2 | - 1 | 3394 | -1229 | + 7 | + 4 | 3422 | -1227 | + 5 | + 2 | 3545 | -1232 | + 10 | + 7 | | | | |
| TORONTO | 3450 | -1249 | 3453 | -1252 | 3525 | -1250 | + 1 | - 2 | 3422 | -1257 | + 8 | + 5 | 3446 | -1251 | + 2 | - 1 | 3569 | -1256 | + 7 | + 4 | | | | |
| LKC | 3468 | -1267 | 3470 | -1269 | 3545 | -1270 | + 3 | + 1 | 3440 | -1275 | + 8 | + 6 | 3465 | -1270 | + 3 | + 1 | 3586 | -1273 | + 6 | + 4 | | | | |
| BKC | 3658 | -1457 | 3670 | -1469 | 3738 | -1463 | + 6 | - 6 | 3632 | -1467 | + 10 | - 2 | | | | | 3736 | -1423 | - 34 | - 46 | | | | |
| ARBUCKLE | | | 3746 | -1545 | 3813 | -1538 | | - 7 | 3707 | -1542 | | - 3 | 3739 | -1544 | | - 1 | 3856 | -1543 | | - 2 | | | | |
| TOTAL DEPTH | 3769 | -1568 | 3770 | -1569 | 3925 | -1650 | + 82 | + 81 | 3747 | -1582 | + 14 | + 13 | 3790 | -1595 | + 27 | + 26 | 3868 | -1555 | - 13 | - 14 | | | | |

DST #1 LKC C - D 3480' - 3526'

DRILL STEM TEST REPORT

Black Diamond Oil Inc. **24/3s/21w**

P.O. Box 641 **Logan NW #1**
Hays, Ks 67601 Job Ticket: 61042 **DST#: 1**

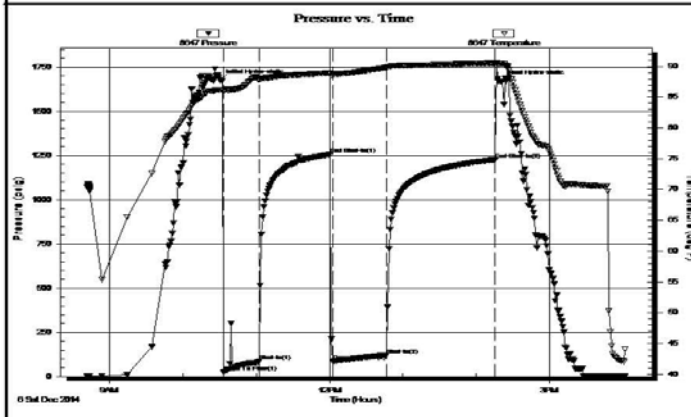
ATTN: Jeff Lawler Test Start: 2014.12.06 @ 08:42:00

GENERAL INFORMATION:

Formation: **LKC "C-D"**
 Deviated: No Whipstock: ft (KB)
 Time Tool Opened: 10:33:30
 Time Test Ended: 16:02:00
 Test Type: Conventional Bottom Hole (Initial)
 Tester: Brandon Quintana
 Unit No: 57
 Interval: **3480.00 ft (KB) To 3526.00 ft (KB) (TVD)**
 Total Depth: 3480.00 ft (KB) (TVD)
 Hole Diameter: 7.88 inches Hole Condition: Fair
 Reference Elevations: 2201.00 ft (KB)
 2196.00 ft (CF)
 KB to GR/CF: 5.00 ft

Serial #: 8647 **Inside**
 Press@RunDepth: 122.48 psig @ 3481.00 ft (KB) Capacity: 8000.00 psig
 Start Date: 2014.12.06 End Date: 2014.12.06 Last Calib.: 2014.12.06
 Start Time: 08:42:01 End Time: 16:02:00 Time On Btm: 2014.12.06 @ 10:30:30
 Time Off Btm: 2014.12.06 @ 14:19:30

TEST COMMENT: 30 - IF - Opened w/ surface blow, built to 7 1/2"
 60 - ISI - No Return
 45 - FF - Blow built to 9 1/2"
 90 - FSI - No Return



| Time (Min.) | Pressure (psig) | Temp (deg F) | Annotation |
|-------------|-----------------|--------------|----------------------|
| 0 | 1675.28 | 86.17 | Initial Hydro-static |
| 3 | 26.78 | 85.98 | Open To Flow (1) |
| 32 | 87.81 | 87.80 | Shut-In(1) |
| 90 | 1255.80 | 88.90 | End Shut-In(1) |
| 92 | 85.43 | 88.75 | Open To Flow (2) |
| 136 | 122.48 | 89.80 | Shut-In(2) |
| 225 | 1226.40 | 90.54 | End Shut-In(2) |
| 229 | 1669.84 | 90.42 | Final Hydro-static |

Recovery

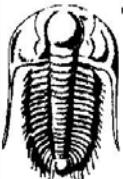
| Length (ft) | Description | Volume (bbl) |
|-------------|-----------------|--------------|
| 182.00 | MWV 80%w, 20% m | 1.45 |
| 50.00 | 100% m | 0.70 |

Gas Rates

| Choke (inches) | Pressure (psig) | Gas Rate (Mcf/d) |
|----------------|-----------------|------------------|
| | | |

| | | |
|--|--|--|
| | | |
| | | |
| | | |

DST #2 LKC J - K 3622' - 3662'

| | | |
|--|---|---|
|  TRILOBITE TESTING, INC. | DRILL STEM TEST REPORT | |
| | Black Diamond Oil Inc. P.O. Box 641 Hays, Ks 67601 ATTN: Jeff Lawler | 24/3s/21w Logan NW #1 Job Ticket: 61043 DST#: 2 Test Start: 2014.12.07 @ 09:22:00 |

GENERAL INFORMATION:

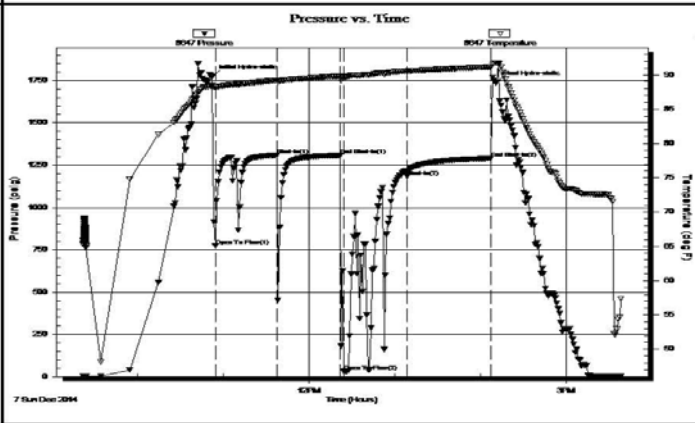
Formation: **LKC "J-K"**
 Deviated: No Whipstock: ft (KB)
 Time Tool Opened: 10:54:30
 Time Test Ended: 15:39:00
Interval: 3622.00 ft (KB) To 3662.00 ft (KB) (TVD)
 Total Depth: 3662.00 ft (KB) (TVD)
 Hole Diameter: 7.88 inches-Hole Condition: Fair

Test Type: Conventional Bottom Hole (Initial)
 Tester: Brandon Quintana
 Unit No: 57
 Reference Elevations: 2201.00 ft (KB)
 2196.00 ft (CF)
 KB to GR/CF: 5.00 ft

Serial #: 8647 Inside

| | |
|--|-------------------------------------|
| Press@RunDepth: 1183.01 psig @ 3623.00 ft (KB) | Capacity: 8000.00 psig |
| Start Date: 2014.12.07 End Date: 2014.12.07 | Last Calib.: 2014.12.07 |
| Start Time: 09:22:01 End Time: 15:39:00 | Time On Btm: 2014.12.07 @ 10:52:30 |
| | Time Off Btm: 2014.12.07 @ 14:11:30 |

TEST COMMENT: 45 - IF - Opened w/ surface blow, built to 1/2" then died back to surface
 45 - ISI - No Return
 45 - FF - No Blow
 60 - FSI - No Return



| PRESSURE SUMMARY | | | |
|------------------|-----------------|--------------|----------------------|
| Time (Min.) | Pressure (psig) | Temp (deg F) | Annotation |
| 0 | 1775.88 | 88.41 | Initial Hydro-static |
| 2 | 773.13 | 88.20 | Open To Flow (1) |
| 45 | 1308.37 | 89.19 | Shut-In(1) |
| 89 | 1307.53 | 89.82 | End Shut-In(1) |
| 92 | 32.28 | 89.56 | Open To Flow (2) |
| 136 | 1183.01 | 90.53 | Shut-In(2) |
| 195 | 1290.12 | 91.16 | End Shut-In(2) |
| 199 | 1738.71 | 91.78 | Final Hydro-static |

| Recovery | | |
|-------------|-------------|--------------|
| Length (ft) | Description | Volume (bbl) |
| 10.00 | 100% mud | 0.05 |
| | | |
| | | |
| | | |
| | | |

| Gas Rates | | | |
|-----------|----------------|-----------------|------------------|
| | Choke (inches) | Pressure (psig) | Gas Rate (Mcf/d) |
| | | | |
| | | | |
| | | | |

DST #3 (STRADDLE) LKC J - K 3610' - 3655'



TRILOBITE TESTING, INC.

DRILL STEM TEST REPORT

Black Diamond Oil Inc.

24/3s/21w

P.O. Box 641
Hays, Ks 67601

Logan NW #1

Job Ticket: 61044

DST#: 3

ATTN: Jeff Lawler

Test Start: 2014.12.08 @ 08:32:00

GENERAL INFORMATION:

Formation: **LKC "J-K"**

Deviated: No Whipstock: ft (KB)

Test Type: Conventional Straddle (Initial)

Time Tool Opened: 10:46:30

Tester: Brandon Quintana

Time Test Ended: 15:06:00

Unit No: 57

Interval: **3610.00 ft (KB) To 3655.00 ft (KB) (TVD)**

Reference Elevations: 2201.00 ft (KB)

Total Depth: 3769.00 ft (KB) (TVD)

2196.00 ft (CF)

Hole Diameter: 7.88 inches Hole Condition: Fair

KB to GR/CF: 5.00 ft

Serial #: 8647

Press@RunDepth: 1301.86 psig @ ft (KB)

Capacity: 8000.00 psig

Start Date: 2014.12.08

End Date: 2014.12.08

Last Calib.: 1899.12.30

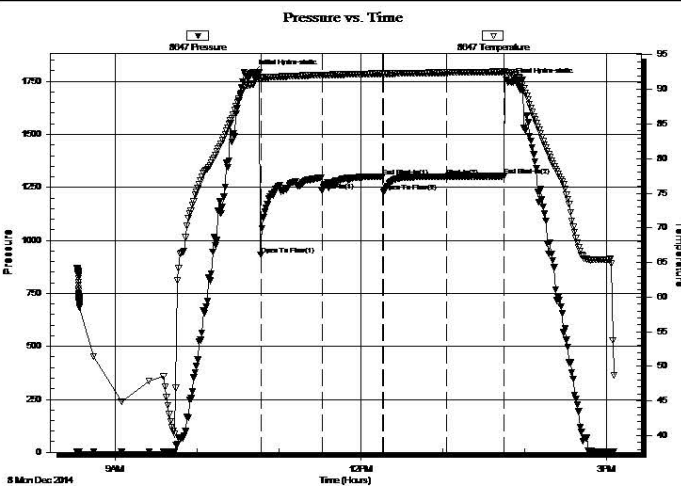
Start Time: 08:32:01

End Time: 15:06:00

Time On Btm: 2014.12.08 @ 10:40:30

Time Off Btm: 2014.12.08 @ 13:48:30

TEST COMMENT: 30 - IF - Opened w / surface blow , w ent straight to 2", died back to 1 1/2"
30 - ISI - No Return
30 - FF - No Blow
30 - FSI - No Return



PRESSURE SUMMARY

| Time (Min.) | Pressure (psig) | Temp (deg F) | Annotation |
|-------------|-----------------|--------------|----------------------|
| 0 | 1790.55 | 90.76 | Initial Hydro-static |
| 6 | 930.16 | 91.69 | Open To Flow (1) |
| 51 | 1234.09 | 92.07 | Shut-In(1) |
| 95 | 1299.16 | 92.29 | End Shut-In(1) |
| 96 | 1228.33 | 92.25 | Open To Flow (2) |
| 142 | 1301.86 | 92.43 | Shut-In(2) |
| 184 | 1302.99 | 92.55 | End Shut-In(2) |
| 188 | 1747.59 | 92.42 | Final Hydro-static |

Recovery

| Length (ft) | Description | Volume (bbl) |
|-------------|-------------|--------------|
| 70.00 | 100% mud | 0.34 |
| | | |
| | | |
| | | |
| | | |

Gas Rates

| | Choke (inches) | Pressure (psig) | Gas Rate (Mcf/d) |
|--|----------------|-----------------|------------------|
| | | | |

Trilobite Testing, Inc

Ref. No: 61044

Printed: 2014.12.08 @ 15:25:49

DST #4 (STRADDLE) TORONTO - LKC A 3420' - 3480' (BOTTOM PACKER CHART AT END OF REPORT)



TRILOBITE TESTING, INC.

DRILL TEST TEST REPORT

Black Diamond Oil Inc.

24/3s/21w

P.O. Box 641
Hays, Ks 67601

Logan NW #1

Job Ticket: 61045

DST#: 4

ATTN: Jeff Lawler

Test Start: 2014.12.08 @ 16:59:00

GENERAL INFORMATION:

Formation: **Toronto & "A"**

Deviated: No Whipstock: ft (KB)

Time Tool Opened: 18:56:30

Time Test Ended: 23:12:30

Test Type: Conventional Straddle (Initial)

Tester: Brandon Quintana

Unit No: 57

Interval: **3420.00 ft (KB) To 3480.00 ft (KB) (TVD)**

Reference Elevations: 2201.00 ft (KB)

Total Depth: 3769.00 ft (KB) (TVD)

2196.00 ft (CF)

Hole Diameter: 7.88 inches Hole Condition: Fair

KB to GR/CF: 5.00 ft

Serial #: 8647

Press@RunDepth: 1271.39 psig @ ft (KB)

Capacity: 8000.00 psig

Start Date: 2014.12.08

End Date: 2014.12.08

Last Calib.: 2014.12.08

Start Time: 16:59:01

End Time: 23:12:30

Time On Btm: 2014.12.08 @ 18:50:30

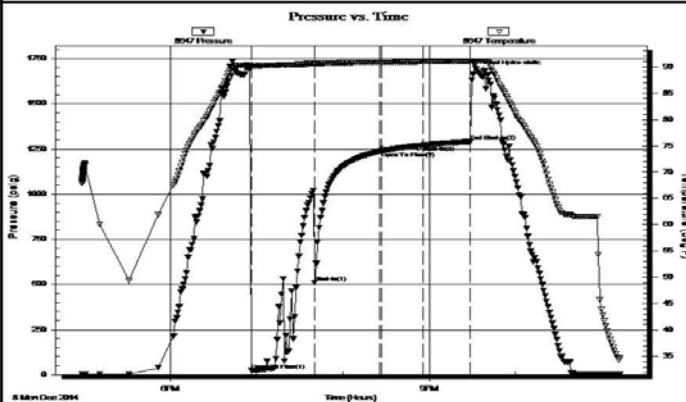
Time Off Btm: 2014.12.08 @ 21:33:30

TEST COMMENT: 45 - IF - Opened w / surface blow , built to 1"

45 - ISI - No Return

30 - FF - No Blow

30 - FSI - No Return



PRESSURE SUMMARY

| Time (Min.) | Pressure (psig) | Temp (deg F) | Annotation |
|-------------|-----------------|--------------|----------------------|
| 0 | 1661.89 | 90.25 | Initial Hydro-static |
| 6 | 23.50 | 90.06 | Open To Flow (1) |
| 50 | 508.89 | 90.52 | Shut-In(1) |
| 95 | 1235.58 | 90.85 | End Shut-In(1) |
| 96 | 1237.50 | 90.85 | Open To Flow (2) |
| 125 | 1271.39 | 90.94 | Shut-In(2) |
| 158 | 1289.96 | 91.02 | End Shut-In(2) |
| 163 | 1679.74 | 91.12 | Final Hydro-static |

Recovery

| Length (ft) | Description | Volume (bbl) |
|-------------|-------------|--------------|
| 10.00 | 100% mud | 0.05 |
| | | |
| | | |
| | | |
| | | |

Gas Rates

| | Choke (inches) | Pressure (psig) | Gas Rate (Mcf/d) |
|--|----------------|-----------------|------------------|
| | | | |

Trilobite Testing, Inc

Ref. No: 61045

Printed: 2014.12.08 @ 23:30:31

ROCK TYPES

| | | | |
|---------|------------|------------|------|
| Cht | Lmst fw7> | Shblk | Stst |
| Congl | shale, gry | shale, red | |
| Dolprim | Carbon Sh | Arg/Shale | |

ACCESSORIES

STRINGER

~~~~ Chert






### OTHER SYMBOLS

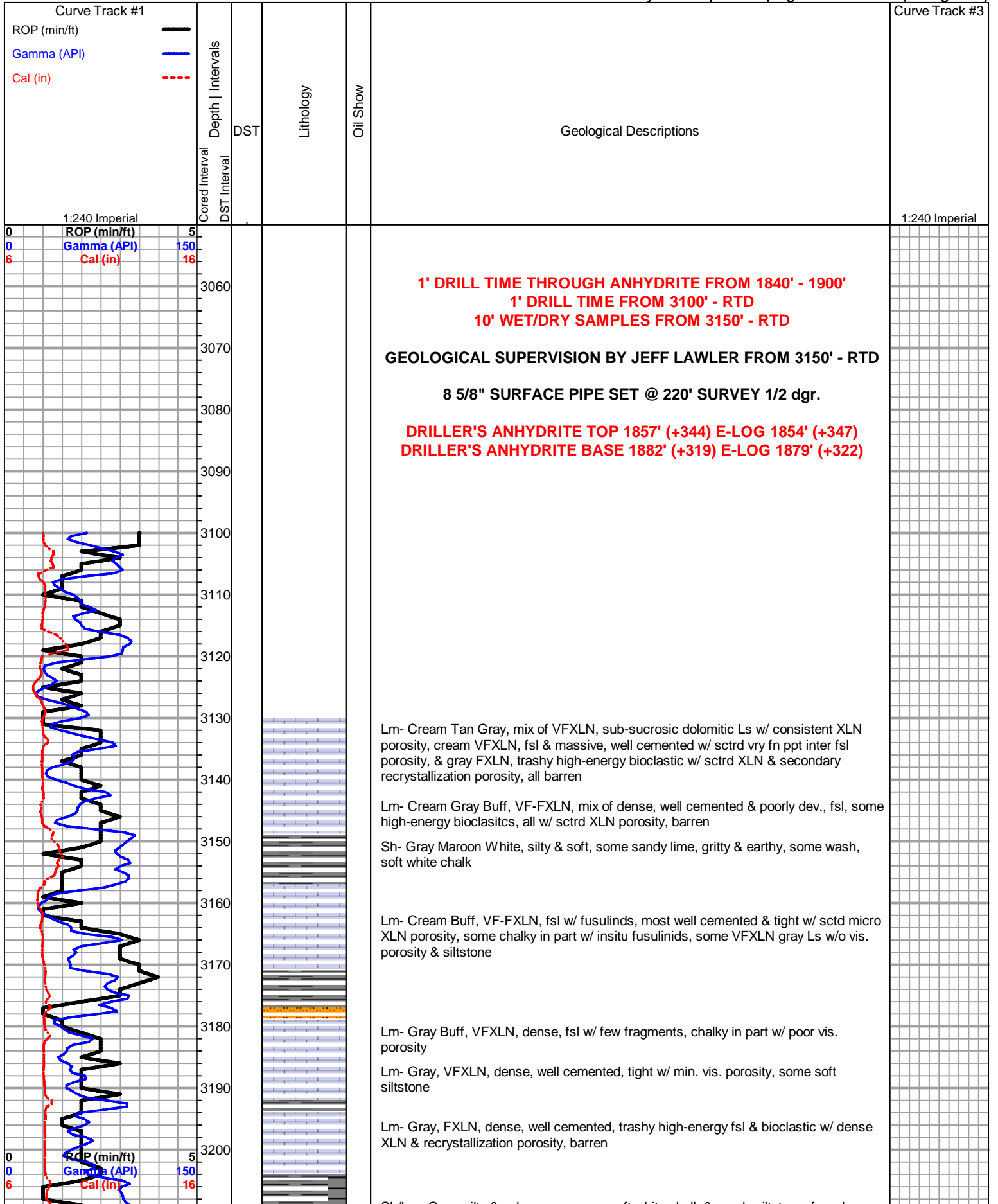
#### MISC

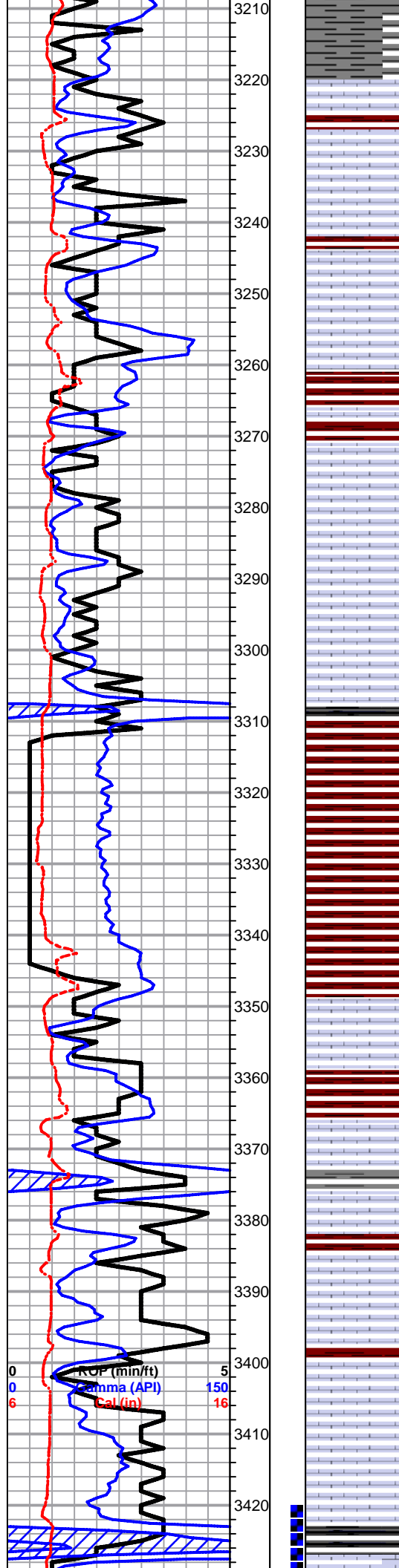
- Daily Report
- Digital Photo
- Document
- Folder

#### DST

- DST Int
- DST alt

-  Link
-  Vertical Log File
-  Horizontal Log File
-  Core Log File
-  Drill Cuttings Rpt





Sh/Lm- Gray, silty & calcareous, some soft white chalk & sandy siltstone, few clumps of gummy gray wash, chalky Lm Green siltstone

**TOPEKA 3219' (-1018) E-LOG 3220' (-1019)** Lm- Cream Tan Buff, FXLN, mix of massive, fsl, some fragments & bioclastic recrystallization, sctrd-dense XLN porosity, some trashy high-energy bioclastic w/ dense XLN & recrystallization porosity

Lm- Gray, VFXLN, dense, tight w/ min. vis. porosity, some lithographic

Lm- Tan Cream, F-Med XLN, fsl w/ fusulinids & fragments, dense recrystallization, clear replacement cementation, barren

Lm- Cream Buff, VF-FXLN, sl fsl, some chalky in part & sl mottled, poor vis. to sctrd micro XLN & XLN porosity, vry clean & barren

Sh- Maroon Gray, gritty & earthy, dense & silty, some unconsolidated & trashy Ss, well cemented & barren

Lm- Cream Off White, VF-FXLN, fusulinids & oolitic, poorly dev., well cemented & dense, some w/ clear replacement cementation, sctrd to dense XLN porosity, some chalky in part, w/ poor vis. porosity, barren, few pcs of fresh bedded oolitic & clean chert w/o vis. porosity

Lm- Cream, VFXLN mix or dense, sl chalky in part, well cemented w/o vis. porosity or matrix & sl fsl, poorly dev. & mostly tight w/ rare sctrd micro XLN porosity, all vry clean & barren

Lm- A/A w/ incr. in milky tan vitreous fresh bedded chert & soft white chalk

Lm- Cream Off White, VF-FXLN, dense, well cemented, fsl & oolitic, poorly dev. w/ sctrd clear replacement cementation, poor effective porosity, some massive, some loosely cemented, crumbly, & chalky

Sh- Black Maroon, fissile, slaty, carbonaceous, gritty & earthy

Sh- Maroon Gray White, gritty & earthy, semi-sandy gummy wash, silty & calcareous & soft white chalk/lime

Sh- A/A w/ incr. in sandy gummy wash, & maroon & buff Fn Grn consolidated & well sorted Ss, barren

Lm- Cream Off White, VFXLN, dense, well cemented, massive & grainy w/ dense micro XLN porosity, barren

Lm- Gray Buff Lt Maroon, Fn Grn, arenaceous Ls, some chalky in part, some calcaerous siltstone

Sh- Drk Gray, dense & silty, soft, few trashy & unconsolidated

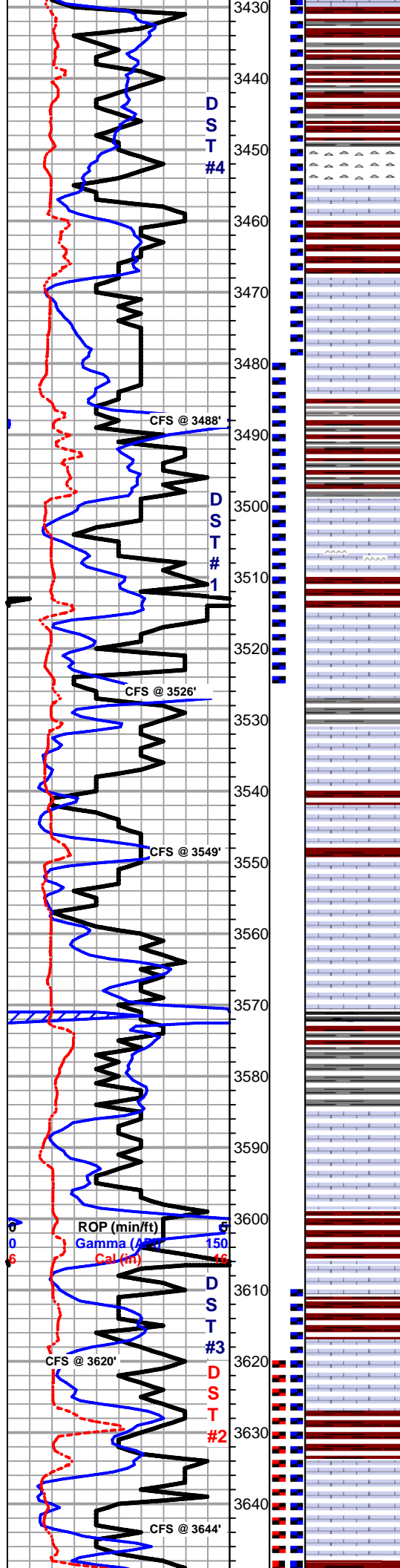
Lm- Cream Buff, VFXLN, dense, well cemented, tight w/ sctrd micro XLN & XLN porosity, several pcs of chalky sl fsl w/ fusulinid, loosely cemented & crumbly

Lm- Cream Off White, VF-FXLN, dense, sl oolitic w/ fusulinids, clear replacement cementation, dense XLN porosity & recrystallization, few pcs of fsl biomicrite w/o vis. porosity, some VFXLN, dense & tight w/o vis. porosity, all vry clean & barren

Lm- Cream Off White, Fn Grn, loosely cemented & semi-crumbly arenaceous Ls w/ poor vis. porosity, chalky

Lm- Buff, VFXLN Vf Grn, dense tight mix, some chalky & loosely cemented, all w/ min. vis. porosity

**HIEBNER 3426' (-1225) E-LOG 3423' (-1222)** Sh- Black Maroon Gray, fissile & carbonaceous, gritty & earthy, gummy wash



Sh- Maroon Gray, A/A w/ gummy maroon wash & sandy gray shale/lime

**TOPEKA 3453' (-1252) E-LOG 3450' (-1249)** Chert- Golden Brown Cream Salmon, vitreous fresh bedded chert, some sl fsl, w/o vis. porosity

Lm- Cream Off White, VF-FXLN, fsl mix, poorly dev. w/ sctrd-dense micro XLN porosity, well cemented & chalky loosely cemented crumbly w/ fusulinids & several loose fusulinids, barren

**LKC 3470' (-1269) E-LOG 3468' (-1267)** Lm- Cream Off White, fsl & sl oolitic, sl sctrd dev. & XLN porosity, few w/ rare vry fn ppt inter oolite porosity, WK SPOTTY STN, 1 PCS W/ SL TR FO UPON CRUSH, TR ODR, DULL HALO FLOR., NO STRM WET CUT, (4-6 pcs total)

Lm- Cream Off White, VF-FXLN, dense, mostly tight, sl fsl, poorly dev. w/ sctrd micro XLN & XLN porosity, some chalky in part, some lithographic w/o vis. porosity

Lm/Chert- Cream Off White, Vf-FXLN, dense, well cemented, consistent micro XLN & vry fn ppt porosity throughout, SCTRD DRK STN, TR FO, TR ODR, BRT YLW FLOR, much barren porosity Golden Brown & Tan fresh bedded chert

Lm/Chert- Cream Off White, VF-FXLN, sl fsl, some chalky in part, mostly tight w/ sctrd XLN porosity at best, barren, several pcs of golden brown, tan, & salmon, some gritty dolomitic chert

Lm- Cream Off White, A/A w/ poorly dev. FXLN oolitic Ls w/ rare sctrd vry fn ppt inter oolite & XLN porosity

Sh- Gray Lm Green Maroon, silty & soft, dense & silty, gritty & earthy

Lm/Chert- Cream Off White, VF-FXLN, oolitic w/ porosity varying w/ min. vis. & clear replacement cementation to sl dev. w/ sctrd XLN & some sctrd fn ppt inter oolite porosity, all well cemented & vry clean & barren, some soft white chalk, much Tan, Milky White, Cream & Salmon fresh bedded chert

Lm- Cream Off White, VFXLN Vf Grn, dense tight mix, sctrd micro XLN & XLN porosity, all vry clean & barren, much soft white chalk

Lm- Cream Mint Green, VFXLN Vf Grn, dense, well cemented mix, all mostly tight w/ poor vis. porosity, some sl oolitic w/ sctrd micro XLN porosity, & well cemented siltstone w/ no vis. porosity, all vry clean & barren, golden brown fresh bedded chert

Sh- Black Drk Gray Maroon Lm Green, fissile & carbonaceous, silty & dense, dense & gritty, soft & semi-calcareous

Sh- A/A w/ gummy wash

Lm- Gray Buff, VF-FXLN, dense, well cemented, mostly tight w/ porosity, some sl fsl

Lm- Tan, VF-FXLN, dense, well cemented, some sl oolitic w/ dense micro XLN & XLN porosity, poorly dev. w/ tight VFXLN w/ no vis. porosity, lithographic

Sh- Maroon Purple Gray, gritty & earthy, some maroon wash, silty & soft

Lm- Cream Off White, FXLN, sl dev. w/ sctrd to dense micro XLN & vry fn ppt porosity, some loosely cemented & crumbly, all clean & barren

Lm- Cream Buff, VF-FXLN, mix of oolitic FXLN w/ sctrd XLN & fn ppt inter oolite porosity, SCTRD DRK STN, TR FO, NO ODR (many pcs.), & dense, vry well cemented & tight VFXLN w/ min. vis. porosity, barren

Lm- Buff Mint Green, VF-FXLN, dense, most well cemented w/ rare ppt & sctrd XLN porosity, some carrying STN A/A, much soft white chalk

Lm- Cream Mustard Yellow, FXLN, oolitic mix, some poorly dev. w/ sctrd-dense XLN porosity, loosely-well cemented & musatrd ylw. oolitic biomicrite w/o vis. porosity & clear replacement cementation, all barren, much soft white chalk

DST #4 (STRADDLE) TORONTO - LKC A 3420' - 3480'

10' MUD

IFP: 23-508#  
FFP: 1237-1271#  
SIP: 1235-1289#

**\*\*SEVERE PLUGGING\*\***

BOTTOM PACKER CHART BELOW

3474.jpg

3474\_2.jpg

3495.jpg

SHORT TRIP SURVEY 1 1/4 dgr STRAP +1.00'

DST #1 LKC C - D 3480' - 3526' 30-60-45-90

50' MUD 182' MW (80%W, 20%M)

IFP: 26-87#  
FFP: 85-122#  
SIP: 1255-1226#

SHORT TRIP SURVEY 3/4 dgr.

DST #2 LKC J - K 3622' - 3662' 45-45-45-60

10' MUD

IFP: 773-1308#  
FFP: 32-1183#  
SIP: 1307-1290#

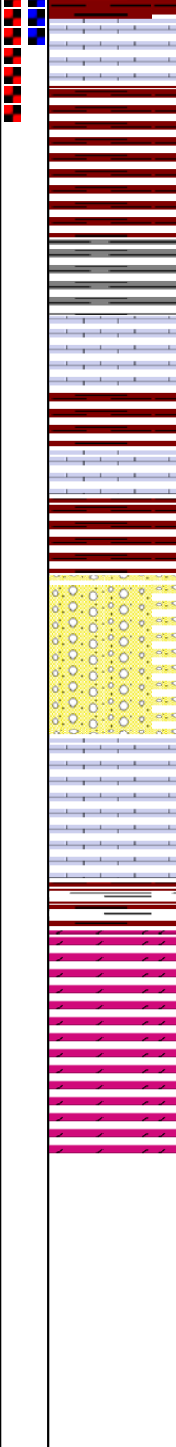
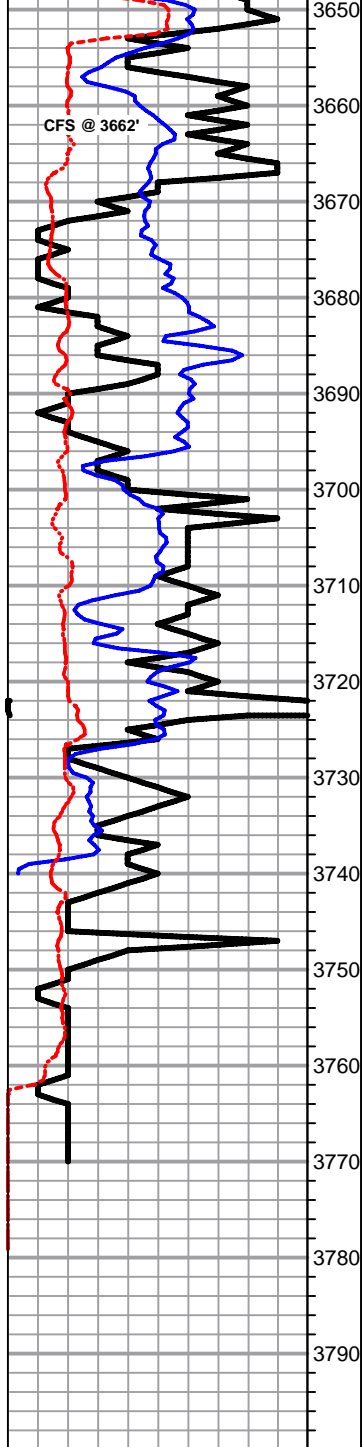
**\*\*NOTE: SEVERE PLUGGING DURING OPEN CYCLES\*\***

3632.jpg

DST #3 LKC J - K STRADDLE 3610' - 3655'

30-30-30-30





Lm- Cream Tan, VF-FXLN, sl fsl, poorly dev. w/ sctrd XLN porosity, some chalky in part, barren

**BKC 3670' (-1469) E-LOG 3658' (-1457)** Sh- Maroon Gray Lm Green, gritty & earthy, some sl sandy gummy wash, silty & unconsolidated, dense & sl calcareous

Lm- Buff Cream Tan, mix of sl unconsolidated & fsl, loosely cemented w/ dense XLN porosity & tight dense VFXLN w/o vis. porosity

Lm- Cream Off White, FXLN, fsl, poorly dev., mostly well cemented & tight w/ sctrd XLN porosity, barren

Conglomerate- Maroon/Pink Cream, unconsolidated & spkld, some loosely cemented & crumbly, FXLN, dense XLN porosity, some chalky mud supported matrix, all w/ poor vis. porosity

Conglomerate- A/A w/ massive fsl, mud supported matrix & FXLN, trashy & well cemented w/ fsl fragments, well cemented w/ sctrd XLN porosity, some maroon sandy lime

Lm- Cream Off White, VF-FXLN Vf Grn, dense, mix of vry well cemented & tight w/ micro XLN porosity & tight, vry dense XLN porosity throughout, & gummy white chalk, some sl sandy, all vry clean & barren

**ARBUCKLE 3746' (-1545)** Dolomite- Cream, FXLN, massive, vry well cemented, tight w/ micro XLN porosity, clean & barren

Dolomite- VFXLN, dense, vry well cemented, tight w/ min. vis. porosity, vry clean & barren, few pcs of chert & cherty dolomitic w/o vis. porosity, barren

**RTD 3770' (-1569) LTD 3769' (-1568) @ 22:22 12/7/2014**

- DST 4\_btmpkr.jpg
- DST 5.jpg
- DST 6.jpg
- DST 6\_BTMPKR.jpg

70' MUD  
IFP: 930-1234#  
FFP: 1228-1301#  
SIP: 1299-1301#

**\*\*SEVERE PLUGGING\*\***

**DST #5 LKC K (STRADDLE) 3627' - 3657'**

**(MISRUN)**

**308' MUD**

**DST #6 LKC K (STRADDLE) 3622' - 3644'**

**DIFFERENT HYDRAULIC SECTION OF TOOL STRING**

**45-60-45-60**

**70' MUD**

**IFP: 30-485#  
FFP: 71-84#  
SIP: 1280-1247#**

**SEE CHARTS BELOW**

**PARTIAL PLUGGING DURING 1st OPEN**

**10 STAND SHORT TRIP CTCH 1 1/2 HR. SURVEY 1 dgr. TOH FOR LOG**



0.2 mm

3474' x 35





0.2 mm

3495' x30



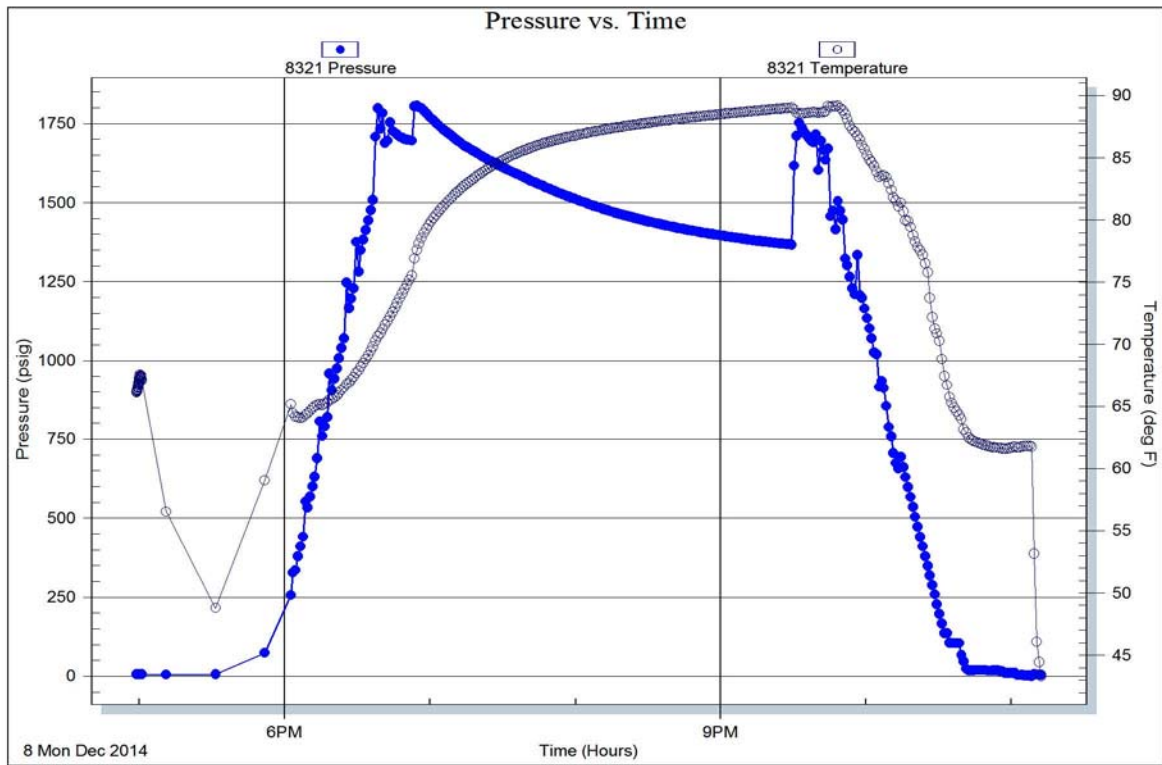
# DST 4\_btmpkr.jpg

Serial #: 8321

Black Diamond Oil Inc.

Logan NW #1


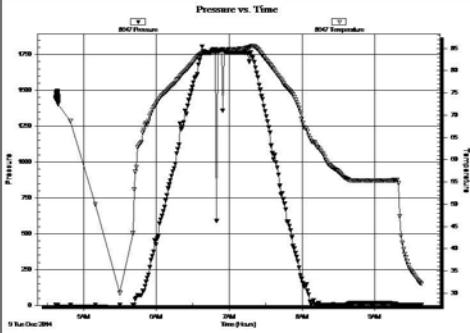
DST Test Number: 4


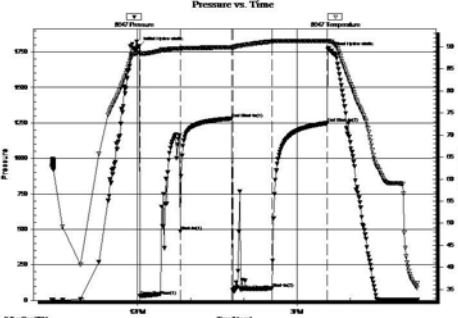


Trilobite Testing, Inc

Ref. No: 61045

Printed: 2014.12.08 @ 23:30:32

|  <b>TRILOBITE TESTING, INC</b>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | <b>DRILL STEM TEST REPORT</b> |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------|-----------------------------------------------------------------------------------------------------------------|-------------|--------------|-----------------|--------------|------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|----------------|-----------------|------------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|
| Black Diamond Oil Inc.<br>P.O. Box 641<br>Hays, Ks 67601<br>ATTN: Jeff Lawler                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                               | <b>24/3s/21w</b><br><b>Logan NW #1</b><br>Job Ticket: 61046 <b>DST#: 5</b><br>Test Start: 2014.12.09 @ 00:00:00 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| <b>GENERAL INFORMATION:</b><br>Formation: <b>LKC "J-K"</b><br>Deviated:      No      Whipstock:                  ft (KB)      Test Type:      Conventional Straddle (Initial)<br>Time Tool Opened:      Tester:      Brandon Quintana<br>Time Test Ended:      Unit No:      57<br><br>Interval: <b>3627.00 ft (KB) To 3657.00 ft (KB) (TVD)</b> Reference Elevations:      2201.00 ft (KB)<br>Total Depth:      3769.00 ft (KB) (TVD)      2196.00 ft (CF)<br>Hole Diameter:      7.88 inches Hole Condition: Fair      KB to GR/CF:      5.00 ft                                                                                                                                                                                                                                                                                                                     |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| <b>Serial #: 8647</b><br>Press@RunDepth:      psig @      ft (KB)      Capacity:      8000.00 psig<br>Start Date:      2014.12.09      End Date:      2014.12.09      Last Calib.:      2014.12.09<br>Start Time:      04:37:01      End Time:      09:38:30      Time On Btm:      Time Off Btm:                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| <b>TEST COMMENT:</b> 30 - IF -<br>30 - ISI - MISRUN<br>30 - FF - PACKER FAILURE<br>30 - FSI -                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | <b>PRESSURE SUMMARY</b>       |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 15%;">Time (Min.)</th> <th style="width: 15%;">Pressure (psig)</th> <th style="width: 15%;">Temp (deg F)</th> <th style="width: 55%;">Annotation</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td></tr> </tbody> </table> |                               |                                                                                                                 |             | Time (Min.)  | Pressure (psig) | Temp (deg F) | Annotation |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Time (Min.)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | Pressure (psig)               | Temp (deg F)                                                                                                    | Annotation  |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| <b>Recovery</b>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               | <b>Gas Rates</b>                                                                                                |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 20%;">Length (ft)</th> <th style="width: 60%;">Description</th> <th style="width: 20%;">Volume (bbl)</th> </tr> </thead> <tbody> <tr> <td>308.00</td> <td>100%Mud</td> <td>3.22</td> </tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>                                                                                                                                                                                                                                                                                                                                                 |                               | Length (ft)                                                                                                     | Description | Volume (bbl) | 308.00          | 100%Mud      | 3.22       |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 30%;">Choke (inches)</th> <th style="width: 30%;">Pressure (psig)</th> <th style="width: 40%;">Gas Rate (Mcf/d)</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table> |  | Choke (inches) | Pressure (psig) | Gas Rate (Mcf/d) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Length (ft)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | Description                   | Volume (bbl)                                                                                                    |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 308.00                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | 100%Mud                       | 3.22                                                                                                            |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Choke (inches)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | Pressure (psig)               | Gas Rate (Mcf/d)                                                                                                |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                               |                                                                                                                 |             |              |                 |              |            |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |  |                |                 |                  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                                               |                                                                                                      |                |                      |                  |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------|----------------|----------------------|------------------|
| <br><b>TRILOBITE TESTING, INC.</b>                                                                                                                                                                                                                                                                                                                                                                                       | <b>DRILL STEM TEST REPORT</b>                                                 |                                                                                                      |                |                      |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Black Diamond Oil Inc.<br>P.O. Box 641<br>Hays, Ks 67601<br>ATTN: Jeff Lawler | <b>24/3s/21w</b><br><br><b>Logan NW #1</b><br>Job Ticket: 61047<br>Test Start: 2014.12.09 @ 10:24:00 | <b>DST#: 6</b> |                      |                  |
| <b>GENERAL INFORMATION:</b><br>Formation: <b>LKC "J-K"</b><br>Deviated: No Whipstock: ft (KB)<br>Time Tool Opened: 12:03:30<br>Time Test Ended: 17:15:30<br>Interval: <b>3622.00 ft (KB) To 3644.00 ft (KB) (TVD)</b><br>Total Depth: <b>3769.00 ft (KB) (TVD)</b><br>Hole Diameter: <b>7.88 inches</b> Hole Condition: Fair<br>Test Type: Conventional Straddle (Initial)<br>Tester: Brandon Quintana<br>Unit No: 57<br>Reference Elevations: 2201.00 ft (KB)<br>2196.00 ft (CF)<br>KB to GR/CF: 5.00 ft |                                                                               |                                                                                                      |                |                      |                  |
| <b>Serial #: 8647</b> Inside<br>Press@RunDepth: 84.17 psig @ 3633.00 ft (KB)<br>Start Date: 2014.12.09 End Date: 2014.12.09<br>Start Time: 10:24:01 End Time: 17:15:30<br>Capacity: 8000.00 psig<br>Last Calib.: 2014.12.09<br>Time On Btm: 2014.12.09 @ 12:02:30<br>Time Off Btm: 2014.12.09 @ 15:37:30                                                                                                                                                                                                  |                                                                               |                                                                                                      |                |                      |                  |
| <b>TEST COMMENT:</b> 45 - IF - Opened w / surface blow , built to 3 1/2"<br>60 - ISI - No Return<br>45 - FF - Blow built to 2 1/4"<br>60 - FSI - No Return                                                                                                                                                                                                                                                                                                                                                |                                                                               |                                                                                                      |                |                      |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                         | <b>PRESSURE SUMMARY</b>                                                       |                                                                                                      |                |                      |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Time (Min.)                                                                   | Pressure (psig)                                                                                      | Temp (deg F)   | Annotation           |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 0                                                                             | 1791.72                                                                                              | 88.65          | Initial Hydro-static |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 1                                                                             | 30.40                                                                                                | 88.37          | Open To Flow (1)     |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 46                                                                            | 485.04                                                                                               | 89.48          | Shut-In(1)           |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 104                                                                           | 1280.86                                                                                              | 89.85          | End Shut-In(1)       |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 105                                                                           | 71.53                                                                                                | 89.72          | Open To Flow (2)     |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 149                                                                           | 84.17                                                                                                | 91.15          | Shut-In(2)           |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 211                                                                           | 1247.93                                                                                              | 91.27          | End Shut-In(2)       |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 215                                                                           | 1755.13                                                                                              | 91.14          | Final Hydro-static   |                  |
| <b>Recovery</b>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                                               | <b>Gas Rates</b>                                                                                     |                |                      |                  |
| Length (ft)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | Description                                                                   | Volume (bbl)                                                                                         | Choke (inches) | Pressure (psig)      | Gas Rate (Mcf/d) |
| 70.00                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 100% mud                                                                      | 0.34                                                                                                 |                |                      |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                                               |                                                                                                      |                |                      |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                                               |                                                                                                      |                |                      |                  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                                                                               |                                                                                                      |                |                      |                  |



# DST 6\_BTMPKR.jpg

