

FILE COPY

ARK. KANSAS CORE ANALYSIS REPORT
FOR
STEVEN TRIPLE I ENERGY CORPORATION
GOOD NO. 25-W WELL
MIAMI COUNTY, KANSAS



SEPTEMBER 9, 1983

TRIPLE I ENERGY CORPORATION
6600 COLLEGE BOULEVARD
SUITE 310
OVERLAND PARK, KANSAS 66211

ATTN: MR. STEVE ALLEE

SUBJECT: CORE ANALYSIS DATA
GOOD NO. 25-W WELL
MIAMI COUNTY, KANSAS
CLI FILE NO. 3406-02484

GENTLEMEN:

DIAMOND CORES WERE TAKEN IN THE SUBJECT WELL AND LATER TRANSPORTED TO OUR CHANUTE LABORATORY FOR ANALYTICAL PURPOSE. THE MEASURED DATA FOLLOWS ON THE ACCOMPANYING PAGES OF THIS REPORT.

THE ACCOMPANYING COREGRAPH PRESENTS THE SURFACE CORE GAMMA LOG AND BINOMIALLY AVERAGED CORE ANALYSIS DATA IN GRAPHICAL FORM TO AID CORRELATION WITH DOWNHOLE ELECTRICAL SURVEYS.

PRODUCTIVITY INDICATED FROM THE RESIDUAL FLUID SATURATION DATA IN THE INTERVAL ANALYZED BETWEEN 472 AND 478 FEET WOULD LIKELY BE OIL AFTER FORMATION TREATMENT.

ZONAL AVERAGES ALONG WITH ESTIMATES OF RECOVERABLE OIL (WHERE APPLICABLE) ARE PRESENTED ON THE CORE SUMMARY PAGE OF THIS REPORT.

SECONDARY RECOVERY FROM A PRUDENT WATER FLOOD PROGRAM MAY APPROXIMATE PRIMARY RECOVERY BARRELS PER ACRE FOOT.

WE APPRECIATE THIS OPPORTUNITY OF SERVING YOU.

VERY TRULY YOURS

CORE LABORATORIES, INC.

J. Michael Edwards/REP
J. MICHAEL EDWARDS
DISTRICT MANAGER

5 CC - ADDRESSEE

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
 DALLAS, TEXAS

TRIPLE I ENERGY CORPORATION
 GOOD NO. 25-W WELL
 LOUISBURG FIELD
 MIAMI COUNTY, KANSAS

DATE: 9/09/83
 FORMATION: WEISER
 DRLG. FLUID: AIR/SALT WATER MIST
 LOCATION: 1980'NSL 660'WEL; SE 1/4; SEC. 11-17S-24E

FILE NO: 3406-02484
 ENGINEER: PRITCHARD
 ELEVATION: 1025.8 FT.

| SMP. NO. | DEPTH | STB/ AC.FT. | PERM. TO AIR MD. PLUG | POROSITY PERCENT | FLUID SATS. OIL WTR. | GR. DEN. | DESCRIPTION |
|----------------------------|------------|----------------|-----------------------------|---------------------|-------------------------|-------------|-----------------|
| CONVENTIONAL PLUG ANALYSIS | | | | | | | |
| | 465.0-66.0 | | | | | | SH,SL/SDY |
| 1 | 466.0-67.0 | 584.0 | 0.7 | 20.9 | 14.2 62.6 | | SD,DOL,SHY,SLTY |
| 2 | 467.0-68.0 | 488.0 | 0.2 | 19.9 | 15.0 67.2 | | SD,DOL,SHY,SLTY |
| 3 | 468.0-69.0 | 702.0 | 0.6 | 21.7 | 22.9 56.6 | | SD,DOL,SHY,SLTY |
| 4 | 469.0-70.0 | 635.0 | 0.5 | 21.1 | 20.3 59.6 | | SD,DOL,SHY,SLTY |
| 5 | 470.0-71.0 | 685.0 | 43.0 | 21.8 | 20.7 57.8 | | SD,DOL,SHY,SLTY |
| 6 | 471.0-72.0 | 728.0 | 14.0 | 21.6 | 26.3 54.8 | | SD,DOL,SHY |
| 7 | 472.0-73.0 | 1276.0 | 1.1 | 23.0 | 55.1 25.6 | | SD,DOL,SHY,SLTY |
| 8 | 473.0-74.0 | 1133.0 | 9.8 | 23.3 | 42.4 34.7 | | SD,DOL,SHY |
| 9 | 474.0-75.0 | 1581.0 | 9.4 | 26.3 | 61.5 19.4 | | SD,DOL,SHY |
| 10 | 475.0-76.0 | 788.0 | 154.0 | 14.1 | 52.3 25.2 | | SD,LMY,DOL,SHY |
| 11 | 476.0-77.0 | 854.0 | 49.0 | 15.6 | 52.8 26.4 | | SD,LMY,DOL,SLTY |
| 12 | 477.0-78.0 | 789.0 | 0.1 | 14.5 | 47.5 27.2 | | SD,LMY,DOL,SLTY |
| | 478.0-79.0 | | | | | | SD,V/SHY |
| | 479.0-81.0 | | | | | | SH |

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
 Oklahoma District

Company TRIPLE I ENERGY CORPORATION

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Well GOOD NO. 25-W

CLI File 3406-02484

CORE SUMMARY AND CALCULATED RECOVERABLE OIL

| FORMATION NAME | WEISER | | | | |
|---|---------|--|--|--|--|
| DEPTH INTERVAL | 472-478 | | | | |
| FEET OF CORE RECOVERED FROM ABOVE INTERVAL | 6 | | | | |
| FEET OF CORE INCLUDED IN AVERAGES | 6 | | | | |
| AVERAGE PERMEABILITY: MILLIDARCYS | 37 | | | | |
| PRODUCTIVE CAPACITY: MILLIDARCY-FEET | 222 | | | | |
| AVERAGE POROSITY: PER CENT | 19.5 | | | | |
| AVERAGE RESIDUAL OIL SATURATION: PER CENT OF PORE SPACE | 51.9 | | | | |
| AVERAGE TOTAL WATER SATURATION: PER CENT OF PORE SPACE | 26.4 | | | | |
| AVERAGE CONNATE WATER SATURATION: PER CENT OF PORE SPACE (e) | 24.0 | | | | |
| OIL GRAVITY: °API | | | | | |
| ORIGINAL SOLUTION GAS-OIL RATIO: CUBIC FEET PER BARREL | | | | | |
| ORIGINAL FORMATION VOLUME FACTOR: BARRELS SATURATED OIL PER BARREL STOCK-TANK OIL | 1.04 | | | | |
| CALCULATED ORIGINAL STOCK-TANK OIL IN PLACE: BARRELS PER ACRE-FOOT | 1106 | | | | |

Calculated maximum solution gas drive recovery is **133** barrels per acre-foot, assuming production could be continued until reservoir pressure declined to zero psig. These recovery estimates represent theoretical maximum values for solution gas drive and do not take into account any prior production or drainage to other areas. The difference between the calculated stock-tank oil in place and the solution gas drive recovery estimates, which are barrels per acre-foot, represent that portion of the reservoir oil which is available for possible secondary recovery techniques. Estimates of additional recoverable oil by secondary or enhanced methods would necessitate a complete engineering study of the subject reservoir.

(c) calculated

(e) estimated

(m) measured



ANY TRIPLE I ENERGY CORPORATION FILE NO. 3406-02484
 GOOD NO. 25-W DATE 09/09/83
 LOUISBURG FORMATION WEISER ELEV. 1025.8 FT.
 COUNTY MIAMI STATE KANSAS DRUG. FLD. AIR/SALT WATER MISCIBLES
 SECTION 1980'NSL 660'WEL; SE 1/4; SEC. 11-17S-24E

CORRELATION COREGRAPH

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VERTICAL SCALE: 5" = 100'

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Total Water _____

PERCENT PORE SPACE
100 80 60 40 20 0

Oil Saturation _____

PERCENT PORE SPACE

Gamma Ray
RADIATION INCREASE →

Permeability _____
MILLIDARCIES

Porosity _____
PERCENT

