

FILE COPY

ENERGY CORPORATION
GE BOULEVARD
CORE ANALYSIS REPORT

APK, KANSAS 66211 FOR

STEVE
TRIPLE I ENERGY CORPORATION
GOOD NO. 29-W WELL
MIAMI COUNTY, KANSAS

CORE AN
GOOD NO



SEPTEMBER 12, 1983

TRIPLE I ENERGY CORPORATION
6600 COLLEGE BOULEVARD
SUITE 310
OVERLAND PARK, KANSAS 66211

ATTN: MR. STEVE ALLEE

SUBJECT: CORE ANALYSIS DATA
GOOD NO. 29-W WELL
MIAMI COUNTY, KANSAS
CLI FILE NO. 3406-02514

GENTLEMEN:

DIAMOND CORES WERE TAKEN IN THE SUBJECT WELL AND LATER TRANSPORTED TO OUR CHANUTE LABORATORY FOR ANALYTICAL PURPOSE. THE MEASURED DATA FOLLOWS ON THE ACCOMPANYING PAGES OF THIS REPORT.

THE ACCOMPANYING COREGRAPH PRESENTS THE SURFACE CORE GAMMA LOG AND BINOMIALLY AVERAGED CORE ANALYSIS DATA IN GRAPHICAL FORM TO AID CORRELATION WITH DOWNHOLE ELECTRICAL SURVEYS.

PRODUCTIVITY INDICATED FROM THE RESIDUAL FLUID SATURATION DATA IN THE INTERVAL ANALYZED BETWEEN 382 AND 391 FEET WOULD LIKELY BE OIL AFTER FORMATION TREATMENT.

ZONAL AVERAGES ALONG WITH ESTIMATES OF RECOVERABLE OIL (WHERE APPLICABLE) ARE PRESENTED ON THE CORE SUMMARY PAGE OF THIS REPORT.

SECONDARY RECOVERY FROM A PRUDENT WATER FLOOD PROGRAM MAY APPROXIMATE PRIMARY RECOVERY BARRELS PER ACRE FOOT.

WE ARE PLEASED TO HAVE BEEN OF SERVICE AND TRUST THESE DATA WILL AID THE PRELIMINARY EVALUATION OF THIS WELL.

VERY TRULY YOURS

CORE LABORATORIES, INC.

J. Michael Edwards
J. MICHAEL EDWARDS REP
DISTRICT MANAGER

5 CC - ADDRESSEE

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
DALLAS, TEXAS

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TRIPLE I ENERGY CORPORATION
GOOD NO. 29-W WELL
LOUISBURG FIELD
MIAMI COUNTY, KANSAS

DATE: 9/12/83
FORMATION: KNOBTOWN/WEISER
DRLG. FLUID: WATER BASE MUD
LOCATION: 2310'NSL 2310'WEL; SE 1/4; SEC. 11-17S-24E

FILE NO: 3406-02514
ENGINEER: PRITCHARD
ELEVATION: 969.3 FT.

SMP. NO.	DEPTH	STB/ AC.FT.	PERM. TO AIR MD. PLUG	POROSITY PERCENT	FLUID SATS. OIL WTR.	GR. DEN.	DESCRIPTION
CONVENTIONAL PLUG ANALYSIS							
	200.0-03.0						SH,SD LAM
	203.0-10.2						SH
1	210.2-11.0	565.0	11.0	19.4	22.8 61.3		SD,SHY,PYR,LMY,MIC
2	211.0-12.0	688.0	7.2	19.8	25.3 54.0		SD,LIG,SHY,PYR,LMY
3	212.0-13.0	678.0	0.9	18.6	27.0 51.5		SD,LIG,SHY,PYR,LMY
4	213.0-14.0	945.0	149.0	22.0	26.9 42.9		SD,SL/LMY,PYR,MIC
5	214.0-15.0	1466.0	165.0	25.8	54.5 24.7		SD,SL/LMY,PYR,MIC
6	215.0-16.0	1267.0	89.0	23.2	46.7 27.6		SD,SL/LMY,PYR,MIC
7	216.0-16.6	309.0	82.0	11.5	19.9 64.2		SD,SL/LMY,PYR,MIC
	216.6-17.5						LM
	217.5-18.0						SH
	218.0-82.0						DRILLED
8	382.0-83.0	1193.0	9.7	23.1	48.6 30.8		SD,SHY,PYR,LMY,MIC
9	383.0-84.0	1148.0	13.0	22.6	44.0 32.0		SD,SHY,PYR,LMY,MIC
10	384.0-85.0	924.0	30.0	17.6	41.7 29.6		SD,LMY,PYR,MIC
11	385.0-86.0	419.0	<0.1	9.1	46.8 38.0		LM,SL/SDY,PYR,MIC
12	386.0-87.0	1348.0	54.0	24.8	43.5 27.2		SD,PYR,LMY,MIC
13	387.0-88.0	1392.0	101.0	26.1	42.1 28.6		SD,PYR,LMY,MIC
14	388.0-89.0	1021.0	40.0	22.4	33.7 38.9		SD,LIG,PYR,LMY,MIC
15	389.0-90.0	1297.0	18.0	22.7	58.9 23.4		SD,GIL,PYR,LMY,MIC
16	390.0-91.0	934.0	31.0	19.4	49.6 35.4		SD,GIL,PYR,LMY,MIC
	391.0-91.3						SH,SDY
	391.3-96.7						SH

CORE LABORATORIES, INC.

Petroleum Reservoir Engineering

CHANUTE, KANSAS

LITHOLOGICAL ABBREVIATIONS

sand - sd
sandy - sdy
shale - sh
shaly - shy
lime - lm
limey - lmy
fine - fn
medium - md
coarse - cs
grain - gr
slightly - sl/
very - v/
with - w/
silty - slty
vuggy - vgy
brown - brn
dark - dk

laminated - lam
pyrite - pyr
gilcinite - gil
lignite - lig
dolomite - dol
chert - ch
cementations - cmt
calcareous - cal
mica or micaceous - mic
inclusions - incl
pin point porosity - pp
fossiliferous - foss
conglomerate - cong
clay - cl
TBA - too broken to analyze

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
 Oklahoma District

Company TRIPLE I ENERGY CORPORATION
 Well GOOD NO. 29-W

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CORE SUMMARY AND CALCULATED RECOVERABLE OIL

FORMATION NAME	KNOBTOWN				
DEPTH INTERVAL	210 - 217				
FEET OF CORE RECOVERED FROM ABOVE INTERVAL	7				
FEET OF CORE INCLUDED IN AVERAGES	7				
AVERAGE PERMEABILITY: MILLIDARCYS	72				
PRODUCTIVE CAPACITY: MILLIDARCY-FEET	504				
AVERAGE POROSITY: PER CENT	20.0				
AVERAGE RESIDUAL OIL SATURATION: PER CENT OF PORE SPACE	31.9				
AVERAGE TOTAL WATER SATURATION: PER CENT OF PORE SPACE	46.6				
AVERAGE CONNATE WATER SATURATION: PER CENT OF PORE SPACE (e)	45.0				
OIL GRAVITY: °API					
ORIGINAL SOLUTION GAS-OIL RATIO: CUBIC FEET PER BARREL					
ORIGINAL FORMATION VOLUME FACTOR: BARRELS SATURATED OIL PER BARREL STOCK-TANK OIL	1.03				
CALCULATED ORIGINAL STOCK-TANK OIL IN PLACE: BARRELS PER ACRE-FOOT	829				

Calculated maximum solution gas drive recovery is * barrels per acre-foot, assuming production could be continued until reservoir pressure declined to zero psig. These recovery estimates represent theoretical maximum values for solution gas drive and do not take into account any prior production or drainage to other areas. The difference between the calculated stock-tank oil in place and the solution gas drive recovery estimates, which are barrels per acre-foot, represent that portion of the reservoir oil which is available for possible secondary recovery techniques. Estimates of additional recoverable oil by secondary or enhanced methods would necessitate a complete engineering study of the subject reservoir.

(c) calculated

(e) estimated

(m) measured

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CORE SUMMARY AND CALCULATED RECOVERABLE OIL

FORMATION NAME	WEISER				
DEPTH INTERVAL	382 - 391				
FEET OF CORE RECOVERED FROM ABOVE INTERVAL	9				
FEET OF CORE INCLUDED IN AVERAGES	9				
AVERAGE PERMEABILITY: MILLIDARCYS	33				
PRODUCTIVE CAPACITY: MILLIDARCY-FEET	297				
AVERAGE POROSITY: PER CENT	20.9				
AVERAGE RESIDUAL OIL SATURATION: PER CENT OF PORE SPACE	45.4				
AVERAGE TOTAL WATER SATURATION: PER CENT OF PORE SPACE	31.5				
AVERAGE CONNATE WATER SATURATION: PER CENT OF PORE SPACE (e)	30.0				
OIL GRAVITY: °API					
ORIGINAL SOLUTION GAS-OIL RATIO: CUBIC FEET PER BARREL					
ORIGINAL FORMATION VOLUME FACTOR: BARRELS SATURATED OIL PER BARREL STOCK-TANK OIL	1.04				
CALCULATED ORIGINAL STOCK-TANK OIL IN PLACE: BARRELS PER ACRE-FOOT	1091				

Calculated maximum solution gas drive recovery is **131** barrels per acre-foot, assuming production could be continued until reservoir pressure declined to zero psig. These recovery estimates represent theoretical maximum values for solution gas drive and do not take into account any prior production or drainage to other areas. The difference between the calculated stock-tank oil in place and the solution gas drive recovery estimates, which are barrels per acre-foot, represent that portion of the reservoir oil which is available for possible secondary recovery techniques. Estimates of additional recoverable oil by secondary or enhanced methods would necessitate a complete engineering study of the subject reservoir.

(c) calculated

(e) estimated

(m) measured

CORE LABORATORIES, INC.**Petroleum Reservoir Engineering**COMPANY TRIPLE I ENERGY CORPORATIONFILE NO. 3406-02514L GOOD NO. 29-WDATE 9/12/83LD LOUISBURGFORMATION KNOBTOWN/WEISERELEV. 969.3JNTY MIAMISTATE KANSASDRLG. FLD. WATER BASE MUDCORES LOCATION 2310'NSL 2310'WEL; SE 1/4; SEC. 11-17S-24E

CORRELATION COREGRAPH

These analyses, opinions or interpretations are based on observations and material supplied by the client to whom, and for whose exclusive and confidential use, this report is made. The interpretations or opinions expressed represent the best judgment of Core Laboratories, Inc., (all errors or omissions excepted); but Core Laboratories, Inc., and its officers and employees, assume no responsibility and make no warranty or representations as to the productivity, proper operation, or profitability of any oil, gas or other mineral well or sand in connection with which such report is used or relied upon.

VERTICAL SCALE: 5" = 100'

Gamma Ray

RADIATION INCREASE →

Permeability

MILLIDARCIES

Porosity

PERCENT

Total Water

PERCENT PORE SPACE

100 80 60 40 20 0

Oil Saturation

PERCENT PORE SPACE

1000

100

10

1

Depth
Feet

30

20

10

0

0

20

40

60

80

100

200

218

382

397

