August 29, 1950

Deep Rook Oil Corporation Atlas Life Building Tules, Oklahoma

Attention: Nr. T. F. Laury

dentlement

Enclosed herewith is the report of the analysis made on the 26" Rotary core taken from the Roselle Lease, Well No. RO-39, Anderson County, Eansas, and submitted to our laboratory on August 20, 1950.

Very truly yours,

OIL FIRED RESEARCH LABORATORIES

Carl L. Pate

CLP:bb c.c. to Mr. Nell Henderson Mr. Jack Hetueney

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ROSELLE LEAGE SELL NO. RC-39

AND PRIEDRICH GRONTY. KANSIAS

OIL PIECO AND ARCH LABORATORIUS ESTANDITIS KANEAS AUGUST 89. 1950

#### GENERAL INFORMATION & SUMMARY

Company Been Rook 011 Corporation		Well No.
ocation 330' from South Line & 999	from Rast Line,	
Section Twp. 23 Rge. 23	County And State	State State
Name of Sand		Squirrel
Cop of Core		616.83
Bottom of Core		653.96
Cop of Sand		625.55
Bottom of Sand		652.38
Cotal Feet of Permeable Sand		19.82
Distribution of Permeable Sand:		
Permeability Range Millidarcys	Feet	Cum. Ft.
0 - 5 5 - 10 10 - 20 20 - 40	8.33 3.43 3.75 3.75	8.93 11.77 15.52 18.87
Average Permeability, Millidarcys		11.96
Average Percent Porosity		18.55
Average Percent Oil Saturation		54-12
verage Percent Water Saturation		31.34
average Oil Content, Bbls./A. Ft.		787.
Cotal Oil Content, Bbls./Acre		12,322.
Average Percent Oil Recovery by Laboratory Floodin	g Tests	30.53
verage Oil Recovery by Laboratory Flooding Tests,	Bbls./A. Ft.	465.
otal Oil Recovery by Laboratory Flooding Tests, B	ols./Acre	6,093.
otal Calculated Oil Recovery, Bbls./Acre		3,850.
	are for that par extending from the ottom of the core	t of peaker 625.50

Water was used as a circulating fluid in the coring of the sand in this well. There were two losses in the bottom part of the cored section that were not shown in the core as we received it in the laboratory and, as a result, the shot recommendation was based on the core as received.

#### FORMASTION CORED

The detailed log of the formation cored is as follows:

Depth Interval, Description Feet

616.83 - 617.00 - Gray shale.

617.00 - 617.50 - Oray shale containing a vertical fracture.

617.50 - 618.60 - Gray chale.

618.60 - 619.30 - Rard brown fine grained micaceous shaley sandstone.

619.30 - 620.75 - Laminated sandstone and shale centaining a vertical fracture.

620.75 - 620.95 - Laminated sandstone and shale.

620.95 - 621.15 - Brown fine grained laminated micageous shaley sandstone.

621.15 - 621.55 - Laminated sandy shale.

621.55 - 621.90 - Brown fine grained laminated micaceous shaley sandstone.

621.90 - 622.15 - Laminated sandy shale.

622.15 - 622.75 - Brown fine grained laminated micaceous shaley sandstone.

622.75 - 625.32 - Gray shale.

625.32 - 625.55 - Laminated shaley sandstone.

625.55 - 626.05 - Brown fine grained micaccous sandstone.

626.05 - 626.24 - Laminated sandy chale.

626.24 - 627.80 - Brown fine grained elightly laminated sicaceous shaley sandstone.

627.80 - 628.20 - Laminated sandy shale.

628.20 - 628.75 - Brown fine grained finely laminated micaceous shaley candetone.

628.75 - 630.58 - Gray shale.

630.58 - 632.30 - Brown fine grained micageous sandstone.

632.30 - 632.72 - Gray sandy shale.

632.72 - 633.00 - Brown fine grained laminated micaceous chaley candstone.

633.00 - 633.50 - Brown fine grained slightly laminated micaccous shaley candstone.

633.50 - 633.95 - Alternate layers of shale and sandatone.

633.95 - 634.50 - Brown fine grained micaccous sandstone.

634.50 - 634.85 - Alternate layers of chale and sandatone.

634.85 - 635.40 - Brown fine grained micaceous sandstone.

635.40 - 635.65 - Brown fine grained slightly laminated misaccous chaley

635.65 - 636.30 - Brown fine grained michocous sandatone.

636.30 - 636.46 - Laminated sandy shale.

636.46 - 637.40 - Brown fine grained micaceous sandstone.

637.40 - 638.05 - Brown fine grained slightly laminated micaceous shaley sandstone.

638.05 - 638.30 - Laminated candy shale.

638.30 - 639.18 - Brown fine grained laminated micaceous shaley sandstone.

639.18 - 639.60 - Laminated sandy shale.

639.60 - 640.15 - Brown fine grained micaceous sandstone.

640.15 - 640.30 - Oray shale.

640.30 - 641.35 - Brown fine grained micaceous sandstone.

641.35 - 641.50 - Laminated shaley sandstone.

641.50 - 641.70 - Laminated sandy shale.

641.70 - 642.15 - Finely laminated shaley sandstone.

642.15 - 642.30 - Laminated sandy shale.

642.30 - 643.00 - Gray shale.

643.00 - 643.60 - Brown fine grained micaceous sandstone.

643.60 - 643.77 - Laminated sandy shale.

643.77 - 643.95 - Finely laminated shaley sandstone.

643.95 - 644.50 - Dark brown fine grained micaceous candstone.

644.50 - 645.05 - Laminated gandy shale.

645.05 - 645.60 - Brown fine grained laminated micaceous shaley sandstone.

645.60 - 645.75 - Laminated sandy shale.

645.75 - 645.89 - Brown fine grained micaceous candstone.

645.89 - 646.00 - Oray shale.

646.00 - 646.50 - Brown fine grained finely laminated micaceous shaley sandstone.

646.30 - 646.82 - Oray shale.

646.82 - 647.00 - Finely laminated shaley sandstone.

647.00 - 647.25 - Brown fine grained micaceous sandstone.

647.25 - 647.50 - Finely laminated shaley sandstone.

647.50 - 647.88 - Laminated gandstone and shale.

647.88 - 648.90 - Loss.

648.90 - 649.00 - Laminated sandstone and shale.

649.00 - 649.60 - Dark brown fine grained micaceous sandstone.

649.60 - 649.70 - Laminated sandstone and shale.

649.70 - 649.80 - Brown fine grained micaceous shaley sandstone.

649.80 - 649.90 - Laminated sandstone and shale.

649.90 - 653.60 - Dark brown fine grained micaceous sandstone.

650.60 - 651.20 - loss.

651.20 - 651.70 - Dark brown fine grained micaceous candstone.

651.70 - 651.90 - Laminated sandy shale.

651.90 - 652.38 - Dark brown fine grained micaceous sandstone.

652.38 - 653.63 - Gray shale.

653.63 - 653.96 - Discarded at well.

Coring was started at a depth of 616.83 feet in gray shale and completed at 653.96 feet, probably in shale. The bottom 0.33 feet of core was discarded at well. This core shows a total of 18.20 feet of sandstone. The cored section is badly broken by layers of shale and laminated sandstone and shale. For the most part, the clean sand is made up of fine grained micaceous to shaley sandstone.

#### PERMEABILITY

For the sake of distribution, the core was divided into three sections. The weighted average permeability of the upper, middle and lower sections are 2.28, 9.06 and 30.95 millidarcys respectively; while that of the pay sand, or that part of the cored section extending from the packer setting to the bottom of the sand, is 11.96. (See Table II). By observing the data given on the coregraph, it is noticeable that the sand has a very irregular permeability profile.

## PERCENT SATURATION & OIL CONTENT

The pay sand in this core shows a very good weighted average percent oil saturaeil saturation, namely, 54.12. The weighted average percent oil saturation of the upper, middle and lower sections are 43.24, 53.10 and 63.17
respectively. The weighted average percent water saturation of the upper,
middle and lower sections are 53.00, 32.20 and 23.80 respectively; while
that of the pay sand is 31.34 (See Table IV). This gives an overall
weighted average total fluid saturation of 85.46 percent.

In an effort to get some idea of the degree of flushing of the sand during coring, all of the saturation samples were analyzed for chloride content. The results of these tests are given in Tables VII and VIII.

Apparently salt water was used as a circulating fluid as the chloride content of the samples do not give the results that would be expected

if fresh water was used.

The weighted average oil content of the upper, middle and lower sections are 530, 771 and 932 barrels per acre foot respectively; while that of the pay sand is 787 barrels. The total oil content, as shown by this core, is 13,223 barrels per acre of which 12,322 barrels are in the pay eand section (See Table IV).

#### LABORATORY FLOODING TESTS

The eard in this core responded very well to laboratory flooding tests, as a total recovery of 6,093 barrels per sore was obtained from 13.11 feet of sand. The weighted average percent oil saturation was reduced from 57.08 to 26.55, or represents an average recovery of 30.53 percent. The weighted average effective permeability of the samples is 1.41 millidarcys, while the average initial fluid production pressure is 14.2 pounds per square inch (See Table VI).

By observing the data given in Table V, you will note that of the 27 samples tested, 20 produced water and oil. This indicates that most of the sand represented by these samples is floodable. The results also show that the sand has a wide variation in effective permeability.

## \*\*) (\*\*)

From a study of the above data, we believe that an efficient water flood within the vicinity of this well will recover approximately 3,850 barrels of oil per acre. In calculating this recovery, no allowance was made for oil lost during coring. From the data given above and on the coregraph, it is evident that the eand within the vicinity of this well is pressured up, or that the well was drilled in semi-virgin territory. By using the primary production factor we ordinarily use in this area,

the calculated recovery is lower than that calculated directly from the core analysis data. The reason why the calculated recovery is considerable lower than the flood pot recovery is the fact that there is a wide variation in perseability.

The principle drawback of this core is the fact that the sand is badly broken and has a wide variation in permeability.

#### SHOT RECOMMENDATION

Company Bean Ro	ok 011 Corpor	Maion Lease Ross	116	Well No.
Depth Interval, Feet	Feet of Sand	Size of Shell Inches	Qts./Ft.	Total Quarts
630.5 - 650.5	20.0	3.5	2.0	40.0

Recommended Packer Setting 625.5 feet

# Oil Field Research Laboratories RESULTS OF PERMEABILITY TESTS TABLE I

Company Deep Rock Oil Corporation Lease Roselle

Well No. RC-39

Sample Depth, No. Feet	Depth,	Permeability	Feet	of Core	Permeability
	Millidarcys	Ft.	Cum. Ft.	Capacity Ft. x Md.	
1	619.33	Imp.	0.30	0.70	0.00
9	620.67			0.30	0.00
2	621.25	Imp.	0.35	0.65	0.00
1	621.75	Imp.	0.40	1.05	0.00
5	622.07	3.8 Tmm	0.35	1.40	1.33
6	622.70	Imp.	0.25	1.65	0.00
1 2 3 4 5 6 7	625.45	1.4	0.60	2.25	0.84
4A	625.67	Imp.	0.23	2.48	0.00
8	626.12	2.2	0.50	2.98	1.10
9	626.35	Imp.	0.19	3.17	0.00
10		2.2	0.46	3.63	1.01
	626.97	13.	0.40	4.03	5.20
11	627.23	13.	0.70	4.73	9.10
12	627.90	Imp.	0.20	4.93	0.00
13	628.13	Imp.	0.20	5.13	0.00
17A	628.37	0.66	0.55	5.68	0.36
14	630.62	14.	0.52	6.20	7.28
15	631.33	24.	0.35	6.55	8.40
16	631.53	23.	0.45	7.00	10.35
17	632.20	24.	0.40	7.40	9.60
18	632.48	Imp.	0.40	7.80	0.00
19	632.88	1.6	0.78	8.58	1.25
20	633.58	6.3	0.10	8.68	0.63
21	633.88	8.7	0.25	8.93	2.18
11A	634.10	7.5	0.55	9.48	4.13
22	634.55	1.6	0.10	9.58	0.16
23	634.78	12.	0.15	9.73	1.80
12A	635.00	2.8	0.55	10.28	1.54
24	635.50	24.	0.15	10.43	3.60
25	635.63	8.5	0.10	10.53	0.85
13A	635.90	7.7	0.65	11.18	5.01
26	636.37	3.6	0.16	11.34	0.58
27	636.55	6.4	0.54	11.88	3.46
28	637.30	16.	0.40	12.28	6.40
15A	637.60	6.3	0.65	12.93	4.10
29	638.13	0,86	0.25	13.18	0.22
30	638.43	1.8	0.40	13.58	0.72
31	639.12	2.5	0.48	14.06	1.20
32	639.50	· qmI	0.42	14.48	0.00
17A	639.72	12.	0.55	15.03	6.60
33	640.47	22.	0.60	15.63	13.20

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# Oil Field Research Laboratories RESULTS OF PERMEABILITY TESTS TABLE I

Company Deep Rock Oil Corporation Lease Roselle

Well No. RC-39

Sample	Depth,	Permeability	Feet	of Core	Permeability
No.	Feet	Millidarcys	Ft.	Cum. Ft.	Capacity Ft. x Md.
34 35 19 A 36 20 A 37 38 21 A 40 41 A 42 A 43 44 45 46 47 48 49	641.20 641.43 641.82 642.20 643.15 643.68 643.90 644.10 644.82 645.20 645.75 645.84 646.12 646.93 647.12 647.70 648.95 649.55 649.96 650.50 651.40 651.80 652.32	15. 2.7 0.81 Imp. 5.1 1.1 3.9 34. 1.8 1.1 1.2 3.3 4.9 4.0 1.3 2.7 14. 53. 43. 32. 27. 0.91 14.	0.45 0.15 0.45 0.15 0.60 0.17 0.18 0.55 0.55 0.15 0.14 0.50 0.18 0.50 0.38 0.10 0.60 0.35 0.35 0.20 0.48	16.08 16.23 16.68 16.83 17.43 17.60 17.78 18.33 18.88 19.43 19.58 19.72 20.22 20.40 20.90 21.28 21.38 21.38 22.68 23.18 23.38 23.86	6.75 0.41 0.36 0.00 3.06 0.18 0.70 18.70 0.99 0.61 0.18 0.46 2.45 7.20 0.65 1.03 1.40 31.80 15.05 11.20 13.50 0.18 6.72

#### SUMMARY OF PERMEABILITY TESTS

#### TABLE II

Company Been Rock O	11 Corporation	Lease Roselle	Well No. RG-39
Depth Interval, Feet	Feet of Core Analyzed	Average Permeability, Millidarcys	Permeability Capacity, Ft. x Md.
618,60 - 622,75	0.95	2,28	2,17
625.55 - 647.50	16.86	9.06	152.73
649.00 - 652.38	2.58	30,95	79.85
625.50 - 652.38	19.44	21.96	232,58

2 5 3 5 1 6

Oil Field Research Laboratories
RESULTS OF SATURATION TESTS

#### TABLE III

Company Deep Rock Oil Corporation

Lease Roselle

Well No. RC-39

Sat.	Sat. Depth,	Effective Percent Saturation			Oil Content	Feet o	f Core	Total Oil	
No.	Feet	Porosity Percent	Oil	Water	Total	Bbls./A. Ft.	Ft.	Cum. Ft.	Content Bbls./Acre
F-234567891121314151617	618.75 620.85 621.05 622.26 625.67 626.52 627.43 628.37 630.85 631.72 633.12 634.10 635.00 635.90 636.72 637.60 638.62 639.72	14.1 13.7 14.8 17.5 19.2 18.3 18.2 14.3 20.0 19.9 17.4 19.1 16.9 19.6 18.8 19.0 21.3	940290215127678004 55.9021559.7678004 57.59.57.57.57.57.57.57.57.57.57.57.57.57.57.	63.3 59.6 38.8 30.4 27.3 26.3 31.4 26.6 32.6 32.6 32.6 32.6 32.6 32.6 32.6	97.0 97.0 986.4542802486.0 986.4542802486.0 882.5428084.86888888888888888888888888888888888	371 354 817 817 866 837 866 875 886 875 887 887 887 887 887 887 887 887 887	0.70 0.20 0.60 0.50 0.75 0.75 0.75 0.75 0.75 0.75 0.7	0.70 0.90 1.10 1.70 2.20 3.06 3.76 4.31 5.03 6.81 7.36 7.91 8.56 9.50 10.15 11.03 11.58	260 71 80 490 417 5851 5851 618 415 7852 648 415 7852 6521

#### RESULTS OF SATURATION TESTS

#### TABLE III

Company Deep Rock Oil Corporation Lease Roselle Well No. RC-39

Sat.	Depth,	Effective	Per	Percent Saturation		Oil Content	Feet o	of Core	Total Oil
No.	Feet	Porosity Percent	Oil	Water	Total	Bbls./A. Ft.	Ft.	Cum. Ft.	Content Bbls./Acre
18 19 20 21 22 23 24 F-24 25 26 27	640.70 641.82 643.15 644.10 645.20 646.12 647.12 647.37 649.12 651.40 652.00	20.5 15.3 20.3 18.7 15.9 16.0 17.7 15.0 20.4 17.5 18.8	54.7 726.7 57.2 61.6 9.4 57.2 61.9 57.2 61.8 62.4 61.9	26.7 58.2 36.4 23.8 51.8 51.8 22.4 23.2	81.4 84.9 93.6 84.1 87.9 93.8 93.0 87.6 88.2	870 317 901 886 489 521 774 362 1,027 847 902 Total	1.05 0.45 0.55 0.55 0.55 0.25 0.25 0.50 0.48	12.63 13.08 13.68 14.23 14.78 15.28 15.53 15.78 16.38 16.88 17.36	913 144 541 488 269 261 193 91 616 424 433

#### RESULTS OF LABORATORY FLOODING TESTS

TABLE V

Company Deep Rock Oil Corporation

Roselle

R0-39

Well No.

Original Oil Saturation Oil Recovery Residual Saturation Initial Fluid Sample Effective Depth. Volume of Water Effective Production Pressure Permeability, Millidarcys Porosity Recovered No. Feet Bbls./A, Ft. Percent Bbls./A. Ft. Bbls./A. Ft. % Oil % Water Percent Lbs./Sq. In. Percent 15.0 619.07 34.5 401 0.0 34.5 0 64.1 401 0 50+ Imp. 621.05 35.0 402 50+ 50 14.8 0.0 35.0 61.9 408 0 Imp. 622.53 58.7 756 16.6 6.0 77 52.7 44.5 679 0.024 0.85 625.92 19.8 56.0 860 23.4 359 38.6 56.8 501 0.108 25 844 626.75 20.0 54.4 31.2 484 23.2 73.2 360 1.05 10 56.1 627.67 18.0 783 25.8 360 423 25 50.3 64.3 0.120 628.63 14.9 42.4 490 0.0 490 48.4 50.7 50 + Imp. 631.13 20.1 55.0 857 31.4 489 366 35.6 72.3 55 54 14 29 1 19 1.75 10 631.95 19.7 57.9 885 31.1 475 26.8 70.0 410 2.09 10 553.35 10 17.8 59.6 930 22.8 512 418 86.8 70.7 0.396 634.35 15 30 15 19.6 56.4 858 30.8 469 389 25.6 70.6 0.854 12 635.25 17.2 56.7 757 20.7 276 481 0.106 86.0 68.7 13 536.15 19.8 87.0 854 31.8 478 25.2 TE.O 378 0.508 14 10 15 25 10 637.00 18.8 56.4 823 27.7 404 28.7 419 1.48 69.5 15 637.90 18.1 54.3 762 26.3 393 10 369 0.397 28.0 69.6 16 658.90 19.2 58.2 778 26.7 398 25.5 70.2 380 0.203 17 640.00 21.0 57.5 937 94 58.7 555 24.8 73.3 404 2.82 10 10 640.95 20.4 54.0 855 472 29.3 24.2 71.1 383 1.66 19 548.05 15.7 26.2 319 0.0 25.2 69.3 319 0 Imp. 20 648.45 19.8 58.3 894 35.3 541 383 36 15 23.0 75.9 0.999 21 644.35 19.0 62.2 917 36.3 535 362 10 25.9 158 72.6 4.98 22 645.46 15.4 37.1 443 0.0 0 37.1 57.8 443 50+ Imp. 23 546.37 25.5 586 40.8 0.0 0 40.8 51.3 536 50+ Imp. 24 647.37 15.0 31.1 362 0.0 0 31.1 66.5 362 0 50 + Imp. 25 649.35 20.4 64.0 1,015 40.4 639 374 23.6 71.5 222 5.43 26 651.60 19.0 874 68 59.3 504 84.8 370 25.1 66.4 1.70 10 27 658.17 519 18.9 64.8 950 85.4 29.4 67.7 431 32 0.713 oubic contineter Rotes: Volume of water recovered at the time of meximum oil recovery. \*\* Determined by passing water through sample which still contains residual oil.

#### SUMMARY OF LABORATORY FLOODING TESTS

#### TABLE VI

Company Deep Rock Oil Corporat	ion Lease	Rossile	Well No.
Depth, Interval, Feet	625,55 - 644,50	649.00 - 652.38	625,55 - 652,38
Feet of Core Analyzed	11.53	1.58	13.11
Average Percent Porosity	19.27	19,49	19,29
Average Percent Original Oil Saturation	86.30	62,72	57.08
Average Percent Oil Recovery	29.65	36,90	20,53
Average Percent Residual Oil Saturation	26.65	25.82	26,53
Average Percent Residual Water Saturation	70.00	60.73	69.85
Average Percent Total Residual Fluid Saturation	96,65	94.55	96,40
Average Original Oil Content, Bbls./A. Ft.	851.	950.	863,
Average Oil Recovery, Bbls./A. Ft.	452.	560.	465.
Average Residual Oil Content, Bbls./A. Ft.	399.	390.	398.
Total Original Oil Content, Bbls./Acre	9,814.	1,500.	11,314.
Total Oil Recovery, Bbls./Acre	5,809.	884.	6,093.
Total Residual Oil Content, Bbls./Acre	4,605.	6 16.	5,221.
Average Effective Permeability, Millidarcys	1.81	2.82	1.41
Average Initial Fluid Production Pressure, p.s.i.	15.6	6.7	14.2

NOTE: Only those samples which recovered oil were used in calculating the above averages.

# Oil Field Research Laboratories RESULTS OF WATER DIFFERENTATION TESTS TABLE VII

Company Deen Rock Gil Corporation Lease Roselle

\_ Well No. 10-39

Sample No.	Depth, Feet	Chloride Content of Brine in Sand ppm	Percent Water Saturation Connate Drilling & Total Foreign
12745678501211111111111111111111111111111111111	616.75 620.85 622.26 625.67 636.52 627.43 628.37 630.85 631.72 634.10 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00 635.00	16,400 16,200 17,400 19,700 18,506 20,600 21,500 21,600 21,600 21,600 21,600 21,600 21,600 21,600 21,600 21,700 20,600 21,700 20,600 21,700 20,600 21,700 20,600 21,700	
		Hote; pps - par	e per million

#### SUMMARY OF WATER DIFFERENTATION TESTS

#### TABLE VIII

ompany Deep Book	Oll Corporation	Lease	Well No.
Depth Interval, Feet	Chloride Content of Brine in Sand, ppm	Average Percent Connate Water	Average Percent Drilling & Foreign Water
618.60 - 622.75	16,793		
625.55 - 647.50	19,826		
649.00 - 652.38	22,639		
625.50 - 652.38	20,114		
Hotes	ppm - parts pe	e million	