CORE LABORATORIES, INC.

Petroleum Reservoir Engineering
DALLAS 1, TEXAS

September 13, 1961

REPLY TO 4010 N. YOUNGS BLVD. P. O. BOX 7128 OKLAHOMA CITY, OKLA.

Home-Stake Production Company Philtower Building Tulsa, Oklahoma

Attention: Mr. Dave Davies

Subject: Core Analysis

Kipfer "A" No. 0-3 Well

Harris Pool Field

Greenwood County, Kansas CLI File No. CP-10-718-FC

Gentlemen:

Coarse grained Bartlesville sand analyzed from 2140 to 2168 feet exhibits residual fluid saturations indicative of oil production. The interval has an average porosity of 20.6 percent and an average permeability of 48 md. The productive capacity of 1047 md./ft. appears adequate to support satisfactory rates of withdrawal without benefit of a treatment. Higher than normal total water saturations are believed due to the presence of chert and weathered chert nodules found in the analyzed interval.

A summary of the average core analysis values on those samples which measured in excess of 2.0 md. permeability has been presented on page one of this report along with estimates of the recoverable oil.

Thank you for the opportunity of serving you.

Yours very truly,

Core Laboratories, Inc.

J. G. Evertson, Jr.

District Manager

JGE:db

7 cc: Addressee

CORE LABORATORIES, INC.

Petroleum Reservoir Engineering
- DALLAS, TEXAS

Page 1 of 1 File CP-10-718-FC Well Kipter "A" No. 0-3

CORE SUMMARY AND CALCULATED RECOVERABLE DIL

FORMATION NAME AND DEPTH INTER	/AL: Bar	tlesville 2140 - 2168				
FEET OF CORE RECOVERED FROM ABOVE INTERVAL	28	AVERAGE TOTAL WATER SATURATION: PER CENT OF PORE SPACE				
FEET OF CORE INCLUDED IN AVERAGES	22	AVERAGE CONNATE WATER SATURATION: PER CENT OF PORE SPACE	(e)	45		
AVERAGE PERMEABILITY: MILLIDARCYS	48	DIL GRAVITY: *API	(e)	38		
PRODUCTIVE CAPACITY: MILLIDARCY-FEET	1047	ORIGINAL SOLUTION GAS-OIL RATIO: CUBIC FEET PER BARREL	(e)	140/1		
AVERAGE POROSITY: PER CENT	20.6	ORIGINAL FORMATION VOLUME FACTOR: BARRELS BATURATED OIL PER BARREL STOCK-TANK OIL	(e)	1.13		
AVERAGE RESIDUAL DIL SATURATION: PER CENT OF PORE SPACE	20.0	CALCULATED ORIGINAL STOCK-TANK OIL IN PLACE: BARRELS PER ACRE-FOOT		745		

Calculated maximum solution gas drive recovery is 176 barrels per acre-foot, assuming production could be continued until reservoir pressure declined to zero psig. Calculated maximum water drive recovery is 425 barrels per acre-foot, assuming full maintenance of original reservoir pressure, 100% areal and vertical coverage, and continuation of production to 100% water cut. (Please refer to footnotes for further discussion of recovery estimates.)

FORMATION NAME AND DEPTH INTERVAL:

FEET OF CORE RECOVERED FROM	AVERAGE TOTAL WATER SATURATION:
ABOVE INTERVAL	PER CENT OF PORE SPACE
FEET OF CORE	AVERAGE CONNATE WATER SATURATION:
INCLUDED IN AVERAGES	PER CENT OF PORE SPACE
AVERAGE PERMEASILITY: MILLIDARCYS	OIL GRAVITY: *API
PRODUCTIVE CAPACITY:	ORIGINAL SOLUTION GAS-DIL RATIO:
MILLIDARCY-FEET	CUBIC FEET PER BARREL
AVERAGE POROSITY: PER CENT	ORIGINAL FORMATION VOLUME FACTOR: BARRELS SATURATED OIL PER BARREL STOCK-TANK OIL
AVERAGE RESIDUAL DIL SATURATION:	CALCULATED ORIGINAL STOCK-TANK OIL IN PLACE:
PER CENT OF PORE SPACE	BARRELS PER ACRE-FOOT

Calculated maximum solution gas drive recovery is barrels per acre-foot, assuming production could be continued until reservoir pressure declined to zero psig. Calculated maximum water drive recovery is barrels per acre-foot, assuming full maintenance of original reservoir pressure, 100% areal and vertical coverage, and continuation of production to 100% water cut. (Please refer to footnotes for further discussion of recovery estimates.)

These recovery estimates represent theoretical maximum values for solution gas and water drive. They assume that production is started at original reservoir pressure; i.e., no account is taken of production to date or of prior drainage to other areas. The effects of factors tending to reduce actual ultimate recovery, such as economic limits on oil production rates, gas-oil ratios, or water-oil ratios, have not been taken into account. Neither have factors been considered which may result in actual recovery intermediate between solution gas and complete water drive recoveries, such as gas cap expansion, gravity drainage, or partial water drive. Detailed predictions of ultimate oil recovery to specific abandonment conditions may be made in an engineering study in which consideration is given to overall reservoir characteristics and economic factors.

These analyses, opinions or interpretations are based on observations and materials supplied by the client to whom, and for whose exclusive and confidential use, this report is made. The interpretations or opinions expressed represent the best judgment of Core Laboratories, Inc., (all errors and omissions excepted); but Core Laboratories, Inc., and its officers and employees assume no responsibility and make no warranty or representation as to the productivity, proper operation, or profitableness of any oil, gas or other mineral well or sand in connection with which such report is used or relied upon.

⁽c) Calculated (e) Estimated (m) Measured (*) Refer to attached letter.



COMPANY_	HOME-STAKE PROD	UCTION COMPANY	DATE ON	9-3-61	FILE NO.	CP10-718-FC
WELL	KIPPER "A" NO.	0-3	DATE OFF_	9-3-61	ENGRS	BOYLE
FIELD	HARRIS POOL		FORMATION	BARTLESVILLE	ELEV	-
COUNTY	GREENWOOD	STATE KANSAS	DRLG. FLD.	WATER BASE MUD	CORES	DIAMOND
		3-225-10E				
		LIMESTONE CO	NGLOMERATE	<i>၀</i> ္မီး <u>ဇီ</u> ရီ сн	ERT C	
	SHALE	DOLOMITE 7	Γ]

COMPLETION COREGRAPH

						COMPLETION CORLORATION								
						PERMEABILITY O-O				TOTAL WATER O-O PERCENT PORE SPACE				
	TABU	LAR DA	TA an	id IN	TERPRETATION	1,00	80	6ρ	40 20	φ.	80		0 20	q
U X d B X X ✓ ⊃ FEET MD.		YT180%	SATU	IDUAL RATION E SPACE	PROD.	PO	ROSITY	OSITY xx		OIL SATURATION XX			-X	
	MD.	PORO	OIL	TOTAL WATER	PROD.	40 30 20 10 0				0 20 40 60 80 .				
1	2140-41	61	21.4	25.2	52.3	m	Ш	HATT.		2140		HIAH	ПП	Ш
2	41-42	127			53.0	H				0.00		4		1111
3	42-43	205			42.3	1	1111		i i			H	††† † †	††† †
4	43-44	17			46.7			††††	9	· · · · ·		1	††† † †	
5	111-15	21			19.2					1				$\dagger \dagger \dagger \dagger$
6	45-46	5.1			58.2					2115		1	††† † †	
7	46-47	29			50.4					.o. 9			11111	
8	47-48	10			49.5				1	i .o			††† † †	
9	48-49	89	21.5	21.8	47.0		+					 		
10	49-50	ليل			45.3				d.	2150		8		††† 1
11	50-51	201	23.2	23.7	47.0	H				5120		l 8		
12	51-52	31	18.6	22.6	45.2				40	$\prod \cdots $		1 8		
13	52-53	14	17.9									 		
11	53-54	30	19.5	20.5	53.8					0 0		1		
15	54-55	15	19.2	17.7	52.1					ام مرده		 	 	
16	55-56	15	20.3	16.7	57.1				3 6	2177		3		
17	56-57	18	22.3	17.5	60.5							4		
18	57-58	15	17.2	17.5	53.5					• • •				
19	58-59	12	20.9	16.3	50.6				4	. o. o.				
20	59-60	5.2	18.9	12.2	56.0				M E	2160		4		
21	60-61	0.4	16.6	11.5	53.0				3			B		
22	61-62	1.3	17.7	15.3	19.7		11111		.					
23	62-63	3.3						1		• • • •				
24	63-64	72	23.0			1111:	0 **							1
25	64-65	0.1					11111			12165		190		\coprod
26	65-66	1.6	19.6	11.7	52.5		11111			9.0			441144	\coprod
27	66-67	0.4	16.0	11.9	65.6	-	11111	11111	*	1.4.0.				
28	67-68	50.1	14.8	0.0	85.7		11111	+						$\downarrow \downarrow$
-20		The second second second					1111	4444						+
1					19	α osl \oplus	111	لللت		2169				