

# OILFIELD RESEARCH LABORATORIES

536 NORTH HIGHLAND - CHANUTE, KANSAS 66720 - PHONE (316) 431-2650

June 25, 1981

James E. Russell Petroleum, Inc.  
P. O. Box 2618  
Abilene, Texas 79604

Gentlemen:

Enclosed herewith is the report of the analysis of the rotary core taken from the Unit 2, Robbins (Martin Glover) Lease, Well No. R-29, located in Anderson County, Kansas and submitted to our laboratory on June 15, 1981.

Your business is greatly appreciated.

Very truly yours,

OILFIELD RESEARCH LABORATORIES

Sanford A. Michel

SAM/kas

3 c to Abilene, Texas  
2 c to Chanute, Kansas

# Oilfield Research Laboratories

## GENERAL INFORMATION & SUMMARY

Unit 2, Robbins

Company James E. Russell Petroleum, Inc. Lease (Martin Glover) Well No. R-29

Location 330' SNL & 2370' EWL, NE $\frac{1}{4}$

Section 32 Twp. 22S Rge. 19E County Anderson State Kansas

Elevation, Feet Datum: Mean Sea Level (Ground Level) 1081.9

Name of Sand Squirrel

Top of Core 766.0

Bottom of Core 784.7

Top of Sand 766.0

Bottom of Sand (Tested) 783.0

Total Feet of Permeable Sand 12.1

Total Feet of Floodable Sand 5.1

| Distribution of Permeable Sand:<br>Permeability Range<br>Millidarcys | Feet | Cum. Ft. |
|----------------------------------------------------------------------|------|----------|
| 0 - 5                                                                | 7.0  | 7.0      |
| 12 - 30                                                              | 1.1  | 8.1      |
| 40 - 70                                                              | 2.0  | 10.1     |
| 110 - 155                                                            | 2.0  | 12.1     |

Average Permeability Millidarcys 34.5

Average Percent Porosity 17.3

Average Percent Oil Saturation 34.3

Average Percent Water Saturation 44.1

Average Oil Content, Bbls./A. Ft. 466.

Total Oil Content, Bbls./Acre 6,764.

Average Percent Oil Recovery by Laboratory Flooding Tests 6.4

Average Oil Recovery by Laboratory Flooding Tests, Bbls./A. Ft. 100.

Total Oil Recovery by Laboratory Flooding Tests, Bbls./Acre 509.

Total Calculated Oil Recovery, Bbls./Acre See "Calculated Recovery" Section

The core was sampled by a representative of Oilfield Research Laboratories. Fresh water mud was used as a drilling fluid. The core was reported to be from a non-virgin area.

#### FORMATION CORED

The detailed log of the formation cored is as follows:

| <u>Depth Interval,<br/>Feet</u> | <u>Description</u>                             |
|---------------------------------|------------------------------------------------|
| 766.0 - 767.4                   | Sandstone, light brown, shaly.                 |
| 767.4 - 768.0                   | Shale, gray, sandy.                            |
| 768.0 - 769.8                   | Sandstone, light brown, shaly.                 |
| 769.8 - 770.9                   | Shale, gray, sandy.                            |
| 770.9 - 772.6                   | Sandstone, brown.                              |
| 772.6 - 773.1                   | Sandstone and shale, brown and gray laminated. |
| 773.1 - 776.1                   | Sandstone, brown.                              |
| 776.1 - 776.4                   | Shale, gray, sandy.                            |
| 776.4 - 776.8                   | Sandstone, brown.                              |
| 776.8 - 784.1                   | Sandstone and shale, brown and gray laminated. |
| 784.1 - 784.7                   | Shale, gray, sandy.                            |

#### LABORATORY FLOODING TESTS

The sand in this core responded to laboratory flooding tests, as a total recovery of 509 barrels of oil per acre was obtained from 5.1 feet of sand. The weighted average percent oil saturation was reduced from 37.3 to 30.9, or represents an average recovery of 6.4 percent. The weighted average effective permeability of the samples is 14.47 millidarcys, while the average initial fluid production pressure is 23.3 pounds per square inch (See Table V).

By observing the data given in Table IV, you will note that of the 15 samples tested, 6 produced water and oil, and 1 produced water only. This indicates that approximately 40 percent of the sand represented by these samples is floodable pay sand.

#### CALCULATED RECOVERY

It would appear from a study of the core data, that efficient primary and waterflood operations in the vicinity of this well should recover approximately 1,840 barrels of oil per acre. This is an average recovery of 361 barrels per acre foot from 5.1 feet of floodable sand analyzed in this core.

These recovery values were calculated using the following data and assumptions:

|                                                |      |
|------------------------------------------------|------|
| Original formation volume factor, estimated    | 1.05 |
| Reservoir water saturation, percent, estimated | 25.0 |
| Average porosity, percent                      | 20.9 |
| Oil saturation after flooding, percent         | 30.9 |
| Performance factor, percent, estimated         | 55.0 |
| Net floodable sand, feet                       | 5.1  |

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## RESULTS OF SATURATION & PERMEABILITY TESTS

TABLE 1-B

Company James E. Russell Petroleum, Inc. Lease Unit 2, Robbins (Martin Glover) Well No. R-29

| Sample No. | Depth, Feet | Effective Porosity Percent | Percent Saturation |       |       | Oil Content Bbls. / A Ft. | Perm., Mill. | Feet of Sand |          | Total Oil Content | Perm. Capacity Ft. X md. |
|------------|-------------|----------------------------|--------------------|-------|-------|---------------------------|--------------|--------------|----------|-------------------|--------------------------|
|            |             |                            | Oil                | Water | Total |                           |              | Ft.          | Cum. Ft. |                   |                          |
| 1          | 766.5       | 12.1                       | 25                 | 50    | 75    | 235                       | Imp.         | 1.4          | 1.4      | 329               | 0.00                     |
| 2          | 768.5       | 12.4                       | 45                 | 48    | 93    | 436                       | 3.1          | 0.8          | 2.2      | 349               | 2.48                     |
| 3          | 769.4       | 15.0                       | 7                  | 70    | 77    | 82                        | Imp.         | 1.0          | 3.2      | 82                | 0.00                     |
| 4          | 771.5       | 21.4                       | 37                 | 32    | 69    | 614                       | 44.          | 1.0          | 4.2      | 614               | 44.00                    |
| 5          | 772.5       | 15.6                       | 43                 | 37    | 80    | 520                       | 13.          | 0.7          | 4.9      | 364               | 9.10                     |
| 6          | 773.5       | 21.4                       | 39                 | 39    | 78    | 647                       | 153.         | 1.0          | 5.9      | 647               | 153.00                   |
| 7          | 774.4       | 21.5                       | 45                 | 29    | 74    | 751                       | 65.          | 1.0          | 6.9      | 751               | 65.00                    |
| 8          | 775.5       | 24.1                       | 25                 | 38    | 63    | 467                       | 113.         | 1.0          | 7.9      | 467               | 113.00                   |
| 9          | 776.5       | 17.9                       | 35                 | 46    | 81    | 486                       | 27.          | 0.4          | 8.3      | 194               | 10.80                    |
| 10         | 777.8       | 15.9                       | 27                 | 53    | 80    | 333                       | 3.9          | 1.2          | 9.5      | 400               | 4.68                     |
| 11         | 778.5       | 17.7                       | 44                 | 29    | 73    | 604                       | 1.3          | 1.0          | 10.5     | 604               | 1.30                     |
| 12         | 779.6       | 15.5                       | 44                 | 37    | 81    | 529                       | 2.6          | 1.0          | 11.5     | 529               | 2.60                     |
| 13         | 780.5       | 18.3                       | 38                 | 42    | 80    | 540                       | 4.2          | 1.0          | 12.5     | 540               | 4.20                     |
| 14         | 781.5       | 15.3                       | 38                 | 55    | 93    | 451                       | 4.5          | 1.0          | 13.5     | 451               | 4.50                     |
| 15         | 782.5       | 17.3                       | 33                 | 52    | 85    | 443                       | 2.4          | 1.0          | 14.5     | 443               | 2.40                     |

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## SUMMARY OF PERMEABILITY & SATURATION TESTS

TABLE III

| Company              |                      | James E. Russell Petroleum, Inc. | Lease                             | Unit 2, Robbins (Martin Glover)  | Well No.                        | R-29                         |
|----------------------|----------------------|----------------------------------|-----------------------------------|----------------------------------|---------------------------------|------------------------------|
| Depth Interval, Feet | Depth Interval, Feet | Feet of Core Analyzed            | Average Permeability, Millidarcys | Permeability Capacity, Ft. x Md. | Average Oil Content Bbl./A. Ft. | Total Oil Content Bbls./Acre |
| 766.0 - 769.8        | 766.0 - 769.8        | 0.8                              | 3.1                               | 2.48                             | 238                             | 760                          |
| 770.9 - 776.8        | 770.9 - 776.8        | 5.1                              | 77.4                              | 394.90                           | 595                             | 3,037                        |
| 776.8 - 783.0        | 776.8 - 783.0        | 6.2                              | 3.2                               | 19.68                            | 479                             | 2,967                        |
| 766.0 - 783.0        | 766.0 - 783.0        | 12.1                             | 34.5                              | 417.06                           | 466                             | 6,764                        |

| Depth Interval, Feet | Feet of Core Analyzed | Average Percent Porosity | Average Percent Oil Saturation | Average Percent Water Saturation | Average Oil Content Bbl./A. Ft. | Total Oil Content Bbls./Acre |
|----------------------|-----------------------|--------------------------|--------------------------------|----------------------------------|---------------------------------|------------------------------|
| 766.0 - 769.8        | 3.2                   | 13.1                     | 24.4                           | 55.8                             | 238                             | 760                          |
| 770.9 - 776.8        | 5.1                   | 20.9                     | 37.3                           | 35.7                             | 595                             | 3,037                        |
| 776.8 - 783.0        | 6.2                   | 16.6                     | 37.0                           | 44.9                             | 479                             | 2,967                        |
| 766.0 - 783.0        | 14.5                  | 17.3                     | 34.3                           | 44.1                             | 466                             | 6,764                        |

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## RESULTS OF LABORATORY FLOODING TESTS

TABLE IV

Unit 2, Robbins  
(Martin Glover)

Well No. R-29

James E. Russell Petroleum, Inc.

Company

| Sample No. | Depth, Feet | Effective Porosity Percent | Original Oil Saturation |              | Oil Recovery |              | Residual Saturation |         |              | Volume of Water Recovered cc* | Effective Permeability Millidarcys** | Initial Fluid Production Pressure Lbs./Sq./In. |
|------------|-------------|----------------------------|-------------------------|--------------|--------------|--------------|---------------------|---------|--------------|-------------------------------|--------------------------------------|------------------------------------------------|
|            |             |                            | %                       | Bbls./A. Ft. | %            | Bbls./A. Ft. | % Oil               | % Water | Bbls./A. Ft. |                               |                                      |                                                |
| 1          | 766.5       | 12.2                       | 25                      | 237          | 0            | 0            | 25                  | 51      | 237          | 0                             | Imp.                                 | -                                              |
| 2          | 768.5       | 12.5                       | 45                      | 436          | 0            | 0            | 45                  | 40      | 436          | 0                             | Imp.                                 | -                                              |
| 3          | 769.4       | 15.1                       | 7                       | 82           | 0            | 0            | 7                   | 78      | 82           | 0                             | Imp.                                 | -                                              |
| 4          | 771.5       | 21.5                       | 37                      | 617          | 8            | 133          | 29                  | 66      | 484          | 362                           | 16.83                                | 20                                             |
| 5          | 772.5       | 15.7                       | 43                      | 524          | 11           | 134          | 32                  | 59      | 390          | 216                           | 3.60                                 | 25                                             |
| 6          | 773.5       | 21.5                       | 39                      | 651          | 3            | 50           | 36                  | 57      | 601          | 422                           | 17.49                                | 20                                             |
| 7          | 774.4       | 21.6                       | 45                      | 754          | 11           | 184          | 34                  | 52      | 570          | 458                           | 19.16                                | 15                                             |
| 8          | 775.5       | 24.1                       | 25                      | 467          | 2            | 37           | 23                  | 72      | 430          | 380                           | 17.49                                | 10                                             |
| 9          | 776.5       | 17.8                       | 35                      | 483          | 2            | 28           | 33                  | 50      | 455          | 20                            | 0.75                                 | 50                                             |
| 10         | 777.8       | 16.0                       | 27                      | 335          | 0            | 0            | 27                  | 54      | 335          | 0                             | Imp.                                 | -                                              |
| 11         | 778.5       | 18.0                       | 43                      | 600          | 0            | 0            | 43                  | 31      | 600          | 0                             | Imp.                                 | -                                              |
| 12         | 779.6       | 15.6                       | 44                      | 533          | 0            | 0            | 44                  | 43      | 533          | 0                             | Imp.                                 | -                                              |
| 13         | 780.5       | 18.0                       | 39                      | 545          | 0            | 0            | 39                  | 42      | 545          | 0                             | Imp.                                 | 50                                             |
| 14         | 781.5       | 15.4                       | 38                      | 454          | 0            | 0            | 48                  | 56      | 454          | 12                            | 0.90                                 | -                                              |
| 15         | 782.5       | 17.4                       | 33                      | 445          | 0            | 0            | 33                  | 53      | 445          | 0                             | Imp.                                 | -                                              |

Notes: cc—cubic centimeter.

\*—Volume of water recovered at the time of maximum oil recovery.

\*\*—Determined by passing water through sample which still contains residual oil.

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## SUMMARY OF LABORATORY FLOODING TESTS

TABLE V

Unit 2, Robbins  
(Martin Glover)

Well No. R-29

Company James E. Russell Petroleum, Inc.

766.0 - 783.0

Depth Interval, Feet

5.1

Feet of Core Analyzed

20.9

Average Percent Porosity

37.3

Average Percent Original Oil Saturation

6.4

Average Percent Oil Recovery

30.9

Average Percent Residual Oil Saturation

60.5

Average Percent Residual Water Saturation

91.4

Average Percent Total Residual Fluid Saturation

598.

Average Original Oil Content, Bbls./A. Ft.

100.

Average Oil Recovery, Bbls./A. Ft.

498.

Average Residual Oil Content, Bbls./A. Ft.

3,049.

Total Original Oil Content, Bbls./Acre

509.

Total Oil Recovery, Bbls./Acre

2,540.

Total Residual Oil Content, Bbls./Acre

14.47

Average Effective Permeability, Millidarcys

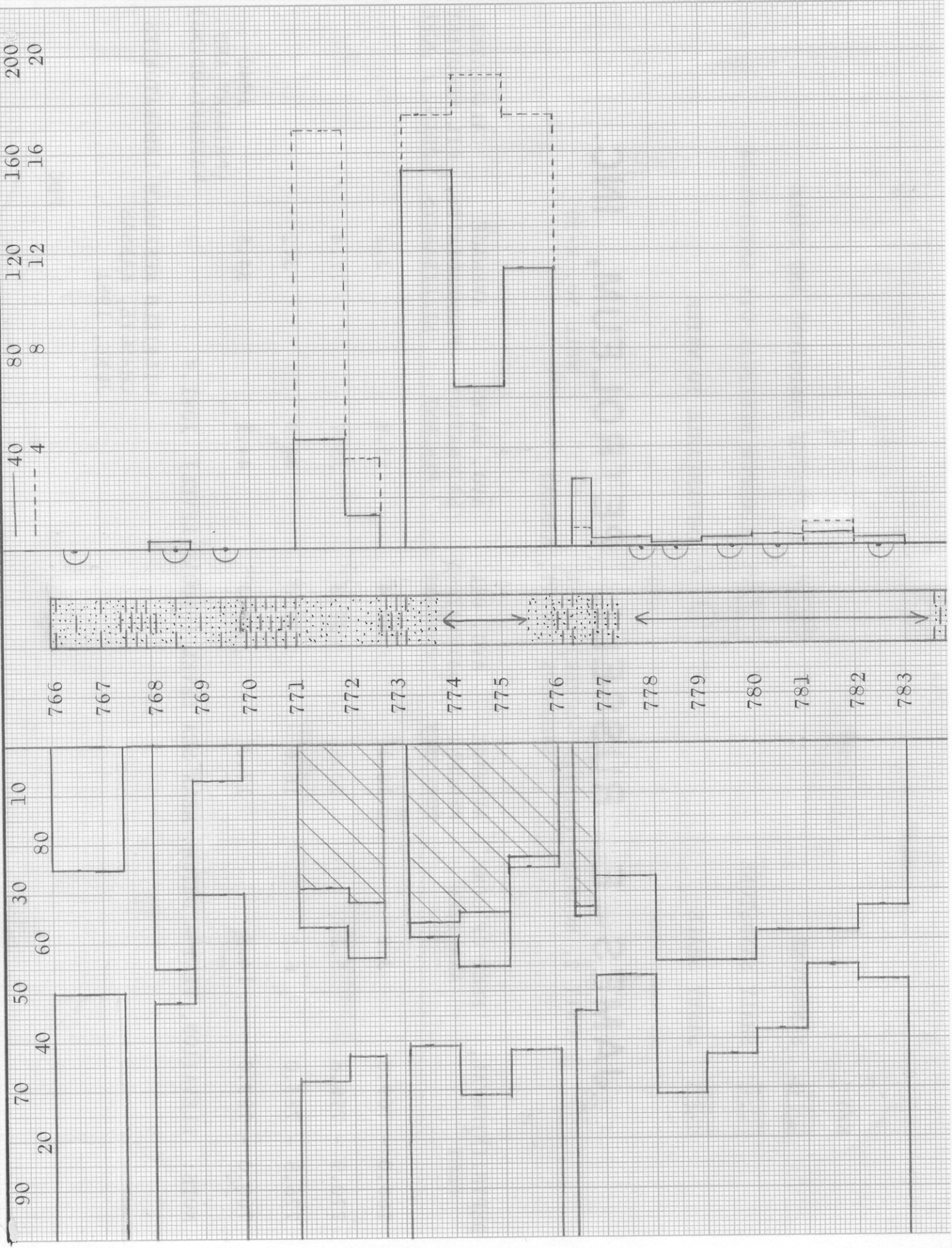
23.3

Average Initial Fluid Production Pressure, p.s.i.

NOTE: Only those samples which recovered oil were used in calculating the above averages.

WATER SAT., PERCENT → ← OIL SAT., PERCENT

PERMEABILITY, IN MILLIDARCS  
EFFECTIVE PERMEABILITY TO WATER, IN MILLIDARCS



KEY:

|                                                                                     |                 |                                                                                    |                                  |
|-------------------------------------------------------------------------------------|-----------------|------------------------------------------------------------------------------------|----------------------------------|
|  | SANDSTONE       |  | LAMINATED SANDSTONE AND SHALE    |
|  | SHALY SANDSTONE |  | FLOODPOT RESIDUAL OIL SATURATION |
|  | SANDY SHALE     |  | IMPERMEABLE TO WATER             |

# JAMES E. RUSSELL PETROLEUM, INC.

UNIT 2, ROBBINS (MARTIN GLOVER) LEASE  
ANDERSON COUNTY, KANSAS  
WELL NO. R-29

| DEPTH INTERVAL,<br>FEET | FEET OF CORE<br>ANALYZED | AVERAGE<br>POROSITY<br>PERCENT | AVG. OIL<br>SATURATION<br>PERCENT | AVG. WATER<br>SATURATION<br>PERCENT | AVERAGE<br>PERMEABILITY,<br>MILLIDARCS | CALCULATED<br>OIL RECOVERY<br>BBLs. / ACRE |
|-------------------------|--------------------------|--------------------------------|-----------------------------------|-------------------------------------|----------------------------------------|--------------------------------------------|
|-------------------------|--------------------------|--------------------------------|-----------------------------------|-------------------------------------|----------------------------------------|--------------------------------------------|

|               |      |      |      |      |      |      |
|---------------|------|------|------|------|------|------|
| 766.0 - 769.8 | 3.2  | 13.1 | 24.4 | 55.8 | 3.1  |      |
| 770.9 - 776.8 | 5.1  | 20.9 | 37.3 | 35.7 | 77.4 |      |
| 776.8 - 783.0 | 6.2  | 16.6 | 37.0 | 44.9 | 3.2  |      |
| 766.0 - 783.0 | 14.5 | 17.3 | 34.3 | 44.1 | 34.5 | 1840 |

NOTE: ELEVATION, FEET - DATUM: MEAN SEA LEVEL (GROUND LEVEL) 1081.9  
(PRIMARY AND WATERFLOODING)

OILFIELD RESEARCH LABORATORIES  
CHANUTE, KANSAS  
JUNE, 1981