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Geological Wellsite Report

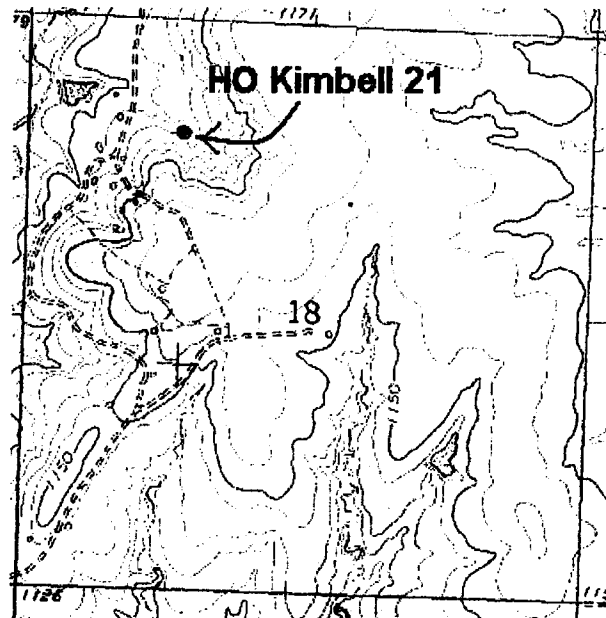
October 8, 2007

15-207-27254

Haas Petroleum, LLC
800 W. 47th St, Suite 409
Kansas City, MO 64112
Attn: Mark Haas

EnerJex Resources, Inc.
Commerce Plaza
7300 W. 110th St., 7th Floor
Overland Park, KS 66210
Attn: Brad Kramer

RE: Geological Wellsite Report
HO Kimbell No. 21, Producer Well
SW SW NE NW4
Section 18, T24S - R14E
Woodson County, Kansas



The following report on the subject well includes detailed information and geological data based on microscopic examination of rotary drill cuttings and drill bit rate of penetration from 1250' to a total depth of 1703' below the kelly bushing. A detailed log that plots drilling time, sample cuttings description and the geological tops is included. Subsea corrected geological tops were based on a relative surveyed ground level elevation of 1115.9' and the sample datum kelly bushing elevation of 1120.4'. The kelly bushing elevation is approximately 4.5' above the ground level.

Daily Progress

September 7, 2007; Rig # 2, Spud and set 41' of 8 5/8" surface casing, drill from 41' to 90',

September 8, 2007; Drill from 90' to 1090',

September 9, 2007, Drill from 1090' to TD at 1703',

September 10, 2007; Open-Hole Logged by Osage Wireline, Inc.

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Well Information

Well Name: HO Kimbell No. 21 **Elev.:** Rel. Survey GL 1115.9', KB 1120.4'

Location: SW SW NE NW4
Section 18, T 24S—R 14E
Woodson County, Kansas

GPS lat long Coord: N37.96415, W-95.91705

API No.: 15-207-27254-0000 **Field:** Winterscheid

Operator: Haas Petroleum, LLC

Contact Person: Mark Haas

Drilling Co.: Skyy Drilling, Rig # 2
Yates Center, Kansas, 66865
KS Operator License No.: 33557

Drilling Co. Owner: Mark Haas **Tool Pusher:** Ben Harrell

Cement Co.: Consolidated Oil Well Service Co.
KS Operator License No.: 04996

Status: Pending Open-Hole Completion **Spud Date:** Sept. 7, 2007

Rotary Total Depth: 1703' KB **Date Reached TD:** Sept. 9, 2007

Surface Casing: Hole drilled with 12 ¼" bit, 41' of 8 5/8" casing,
Cemented with approximately 30 sacks of class "A" cement with 2% gel
and 3% CaCl₂.

Drilling Notes: 5-blade (Ultrerra) PDC 6 3/4-inch Bit from 41' to 1703'
Drilling time provided from 1250' to TD at 1703'
Sample travel time to surface (lag), approx. 1 min. per 150 feet

Mud Program: Native fresh water mud to 1100', fresh water gel mud from 1100' to TD
Fudd Mud, Inc. provided occasional monitoring of chemical drilling mud,
Preferred properties; 33 to 36 vis, 8.9 to 9.4 wt.

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Geological Supervision:

David Griffin, RG, provided wellsite supervision on Sept. 9 and Sept. 10, 2007 for depths from 1250' to 1703' TD. Samples microscopically examined for the entire interval.

Logs and Cores: This well is a set-thru producer completion. An open-hole log was obtained by Osage Wireline, Inc. and a cased-hole log by Midwest Survey. The LAS log files were received from Osage Wireline on October 1, 2007. No cores were gathered for this well.

Drill Stem Testing: No drill stem tests were performed.

Geological Datums:

<i>HO Kimbell No. 21, Geological Tops</i>					HO Kimb 22	HO Kimb 19
SW SW NE NW4	KB Sample Depth		KB Open-Hole Log Depth		E2 NE NW NW4	W2 NE NW NW4, 636' W
Relative Survey KB Elev. 1120	Depth	Subsea	Depth	Subsea	Rel. Surv. KB Elev. 1125 Sample Log Subsea	Rel. Surv. KB Elev. 1110 Sample Log Subsea
Cherokee Group	1283	-163	1282	-161	-158	-171
U. Squirrel SS	1293	-173	1291	-170		
Ardmore LS	1395	-275	1394	-273	-268	-271
Cattleman SS						-285
Bartlesville Zone Marker	1504	-384	1503	-382	-380	-384
Bartlesville SS						
Chat Conglomerate	1614	-494	1614	-493	-488	-496
Mississippian LS	1627	-507	1628	-507	-505	-512
Miss. Dol, Pay Zone	1639	-519	1643	-522	-521	-518
Total Depth	1703	-583	1707	-586	-533	-580

Structural Comparisons:

Structural comparison of subsea corrected geological log tops for HO Kimbell No. 21 indicates that the top of the dolomite pay zone was 1' lower than in HO Kimbell No. 22, a new producing well lying 680' to the north.

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Pay Zone Description

Mississippian; Dolomite:

Pay Zone, 1643' to 1665', KB, Open-Hole Log;

Dolomite, calcareous, tan to tannish gray to brown, very fine to fine crystalline, fair to very good crystalline porosity and fair to very good vugular porosity, 5% to 30% chert, nodular, white, tan, or gray, good to strong oil odor, excellent show of free oil washing from sample, abundant oil bleeding from samples and collecting on the surface of the sample wash water, noticeable oil scum on the drilling mud pit, 30% to 80% bright green sample fluorescence. This zone looks excellent with abundant free oil bleeding from samples. Limestone interbeds with little oil showing occur from approximately 1650' to 1653', O-Hole Log.

Pay Zone Saltwater Calculations:

Open-Hole Log responses indicate the best potential pay zone lies from 1643' to 1650' and from 1653' to 1665' KB. The average of the density and neutron porosity measurements range from 14.8% to 31.5% and the deep induction resistivity measurement range from 3.94 to 10.4 ohms. Using a formation water resistivity (R_w) value of 0.11 and a cementation (m) value of 2, the S_w calculations range from 36.9% to 79.4% using the Archie Equation. The Archie Equation calculations on half foot interval log data are presented on the attached sheet for reference.

Sample Observations of Other Zones of Interest

Pennsylvanian, Bartlesville Zone, Shale and Coal

1504' to 1515', KB, Open-Hole Log;

Shale, dark gray to black and coaly, good odor in samples that quickly dissipates, high resistivity indicate a probable gas zone.

Pennsylvanian, Sandy Siltstone, Conglomerate?:

1614' to 1628', KB, Open-Hole Log;

Sandy siltstone, to silty sandstone, possible conglomerate, light grayish- tan, sandy, predominately very fine grained with minor fine and medium quartz grains, also contains coal, shale, light gray silty to very dark gray, some clay streaks, trace chert throughout, translucent gray, poor to good porosity, no odor, no show of oil or fluorescence.

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Mississippian Limestone:

1628' to 1642', KB, Open-Hole Log;

Limestone, cream to very light gray, medium to coarse crystalline, grainstone, 10% silty sandstone interbeds, very minor glauconitic, mostly very fine grained with minor fine and medium grained, poor to fair crystalline porosity, poor to fair vugular porosity, slight odor, slight show of oil bleeding from sample in bottom part of zone, 3% bright green fluorescence.

Summary:

Approximately 19' of cherty dolomitic pay zone was penetrated from 1643' to 1650' and from 1653' to 1665' KB, Open-Hole Log, for a subsea top of -522, which is 1' structurally lower than HO Kimbell No. 22, a new open-hole producer well lying 680' to the north. The pay zone is structurally high and with fair to very good crystalline and vugular porosity development. The pay zone contained a strong odor and an excellent showing of free oil that readily washes from the samples indicative of high oil saturations. Analysis of the saltwater saturations from the open-hole log indicates that this well probably has the lowest log inferred saltwater percentages for the pay zone to date. With the excellent showing of oil, the operator set and cemented 4½-inch casing through the pay zone for completion as a set-thru producer.

Recommendations:

Based on the sample observations, structural position of the pay zone and open-hole log responses, the best zone to perforate appears to be from 1638' to 1656', GL, (-526' datum). At the time of the writing of this report, the well had already perforated from 1638' to 1648' and 1650' to 1656'. The zone was treated with mud acid and then treated with an unknown quantity of 15% acid and is currently thought to be producing from 10 to 15 BOPD.

Respectfully Submitted,



David B. Griffin, RG
Consulting Geologist

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Attachments: Drilling Time, Sample Description and Geological Tops Log, and Archie Equation Saltwater Calculations

HO Kimbell No. 21												
Mississippian Dolomite												
Model = Archie												
PARAMETERS	ZN	DEPTH	THK	RT	PHI	RWA	RO	MA	SW	BVW	VSH	PAY
X		1	1640	0.5	49.5	0.42	12.87	2.57	51.0%	0.047	0.168	0
Y		2	1640.5	0.5	42.9	0.48	9.78	2.66	47.8%	0.051	0.175	0
A		3	1641	0.5	34	0.41	9.21	2.59	52.0%	0.057	0.201	0
M		4	1641.5	0.5	25.5	0.31	8.98	2.47	58.3%	0.066	0.250	0
N		5	1642	0.5	19	0.26	8.04	2.40	65.0%	0.076	0.268	0
RW	0.11	6	1642.5	0.5	14.5	0.24	6.58	2.39	67.2%	0.087	0.284	0
CTHK	40.5	7	1643	0.5	11.7	0.26	5.04	2.44	65.6%	0.097	0.301	0
AVPHI	0.19	8	1643.5	0.5	10.4	18.3%	4.12	2.51	63.1%	0.103	0.364	0
FTOIL	1.68	9	1644	0.5	9.66	17.5%	3.58	2.57	60.9%	0.107	0.370	0
PAYFEET	18	10	1644.5	0.5	9.15	19.0%	3.06	2.66	57.8%	0.110	0.318	0
P		11	1645	0.5	8.48	20.5%	2.61	2.74	55.5%	0.114	0.241	0.05
Q		12	1645.5	0.5	7.86	21.1%	2.47	2.75	56.0%	0.118	0.208	0.05
R		13	1646	0.5	7.69	20.5%	2.61	2.68	58.3%	0.120	0.200	0.04
DMIN	1640	14	1646.5	0.5	8.08	19.6%	2.86	2.64	56.4%	0.117	0.166	0.04
DMAX	1680	15	1647	0.5	8.68	18.9%	3.09	2.62	59.7%	0.113	0.167	0.04
KB	1121	16	1647.5	0.5	8.97	18.7%	3.16	2.62	56.4%	0.111	0.169	0.04
TD	1703	17	1648	0.5	8.54	18.6%	3.17	2.59	60.9%	0.113	0.147	0.04
BHT	94	18	1648.5	0.5	7.53	18.6%	3.17	2.51	64.9%	0.121	0.145	0.03
ST	75	19	1649	0.5	6.43	18.6%	3.18	2.42	70.3%	0.131	0.157	0.03
RMF	1.4	20	1649.5	0.5	5.51	18.6%	3.17	2.33	75.8%	0.141	0.152	0.02
RMFT	75	21	1650	0.5	4.79	19.0%	3.06	2.27	78.9%		0.146	0
		22	1650.5	0.5	4.27	19.8%	2.81	2.26			0.139	0
		23	1651	0.5	3.94	20.6%	2.60	2.28			0.124	0
		24	1651.5	0.5	3.76	21.4%	2.41	2.29			0.140	0
		25	1652	0.5	3.71	21.6%	2.36	2.30	79.7%		0.162	0
		26	1652.5	0.5	3.78	21.3%	2.42	2.29			0.175	0
		27	1653	0.5	3.94	21.0%	2.49	2.30	79.4%		0.185	0
		28	1653.5	0.5	4.23	20.3%	2.66	2.29	79.3%		0.201	0
Colors:	ON	29	1654	0.5	4.7	19.4%	2.92	2.29	78.7%		0.213	0
		30	1654.5	0.5	5.39	19.0%	3.05	2.34	75.2%	0.143	0.227	0.02
RSH		31	1655	0.5	6.33	18.5%	3.23	2.40	71.4%	0.132	0.242	0.03
PHISH		32	1655.5	0.5	7.46	18.1%	3.36	2.47	67.1%	0.121	0.257	0.03
		33	1656	0.5	8.49	19.2%	3.68	2.64	59.2%	0.114	0.248	0.04
		34	1656.5	0.5	9.15	21.7%	4.34	2.89	50.6%	0.110	0.241	0.05
		35	1657	0.5	9.53	23.9%	5.55	3.12	44.8%	0.107	0.219	0.07
		36	1657.5	0.5	9.66	24.9%	6.60	3.22	42.8%	0.107	0.190	0.07
		37	1658	0.5	9.76	25.8%	6.85	3.31	41.2%	0.106	0.176	0.08
		38	1658.5	0.5	9.74	27.8%	7.75	3.50	38.3%	0.106	0.148	0.09
		39	1659	0.5	9.39	29.5%	8.82	3.64	36.7%	0.108	0.133	0.09
		40	1659.5	0.5	8.85	30.2%	8.81	3.67	36.9%	0.111	0.138	0.10
		41	1660	0.5	8.36	31.0%	8.80	3.69	37.1%	0.115	0.160	0.10
		42	1660.5	0.5	7.93	31.5%	7.79	3.71	37.4%	0.118	0.197	0.10
		43	1661	0.5	7.57	31.0%	7.73	3.81	38.9%	0.121	0.239	0.09
		44	1661.5	0.5	7.25	29.5%	6.83	3.43	41.7%	0.123	0.254	0.09
		45	1662	0.5	6.82	26.8%	5.50	3.14	47.1%	0.126	0.195	0.07
		46	1662.5	0.5	6.68	23.5%	4.37	2.84	54.5%	0.128	0.141	0.05
		47	1663	0.5	6.55	20.8%	3.28	2.55	62.4%	0.130	0.141	0.04
		48	1663.5	0.5	6.42	18.4%	2.22	3.24	71.0%	0.131	0.161	0.03
		49	1664	0.5	6.26	17.6%	1.19	3.56	75.4%	0.133	0.193	0.02
		50	1664.5	0.5	6.08	18.0%	0.20	3.39	74.7%	0.135	0.187	0.02
		51	1665	0.5	5.76	18.0%	0.19	3.40	76.9%	0.138	0.156	0.02
		52	1665.5	0.5	5.46	17.4%	0.16	3.64	72.3%	0.142	0.145	0
		53	1666	0.5	5.28	16.4%	0.14	4.09	71.4%	0.144	0.163	0
		54	1666.5	0.5	5.22	16.0%	0.13	4.29	71.1%	0.145	0.157	0
		55	1667	0.5	5.14	16.9%	0.15	3.83	71.7%	0.146	0.144	0
		56	1667.5	0.5	4.98	18.2%	0.16	3.32	72.4%	0.149	0.171	0
		57	1668	0.5	4.74	19.0%	0.17	3.08	72.8%		0.173	0
		58	1668.5	0.5	4.51	18.9%	0.16	3.09	72.3%		0.158	0
		59	1669	0.5	4.36	18.3%	0.15	3.28	71.7%		0.197	0
		60	1669.5	0.5	4.3	17.7%	0.14	3.50	71.2%		0.258	0
		61	1670	0.5	4.27	17.8%	0.13	3.49	71.2%		0.267	0
		62	1670.5	0.5	4.25	18.5%	0.15	3.21	71.7%		0.253	0
		63	1671	0.5	4.32	19.0%	0.16	3.04	72.1%		0.264	0
		64	1671.5	0.5	4.45	18.9%	0.16	3.07	72.2%		0.296	0
		65	1672	0.5	4.58	18.7%	0.16	3.13	72.3%		0.300	0
		66	1672.5	0.5	4.74	18.6%	0.16	3.17	72.4%		0.258	0
CROSS SECTION		67	1673	0.5	4.88	18.2%	0.16	3.32	72.3%		0.224	0
DATUM 1		68	1673.5	0.5	4.98	17.8%	0.16	3.47	72.1%	0.149	0.223	0
DATUM 2		69	1674	0.5	4.99	17.6%	0.15	3.56	71.9%	0.148	0.236	0
No. of Pft		70	1674.5	0.5	4.85	17.4%	0.15	3.62	71.8%	0.149	0.240	0
		71	1675	0.5	4.89	16.6%	0.14	3.98	71.2%		0.215	0
		72	1675.5	0.5	4.69	15.8%	0.12	4.41	70.6%	0.150	0.198	0
		73	1676	0.5	4.96	16.0%	0.13	4.31	70.8%	0.149	0.233	0
		74	1676.5	0.5	5.04	16.7%	0.14	3.92	71.4%	0.148	0.273	0
		75	1677	0.5	5.12	17.4%	0.16	3.62	72.0%	0.147	0.318	0
		76	1677.5	0.5	5.23	17.5%	0.16	3.60	72.1%	0.145	0.447	0
		77	1678	0.5	5.42	16.6%	0.15	3.97	71.7%	0.142	0.760	0
		78	1678.5	0.5	5.77	15.0%	0.13	4.87	70.9%	0.138	1.263	0
		79	1679	0.5	6.16	15.7%	0.12	5.88	70.2%	0.134	1.493	0
		80	1679.5	0.5	6.44	15.0%	0.13	5.62	70.7%	0.131	1.161	0
		81	1680	0.5	6.52	15.2%	0.15	4.75	71.7%	0.130	0.679	0

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