



# OILFIELD RESEARCH LABORATORIES

536 NORTH HIGHLAND - CHANUTE, KANSAS - PHONE HE1-2650

May 26, 1967

CRA, Incorporated  
P.O. Box 98  
Wellington, Kansas

Gentlemen:

Enclosed herewith is the report of the analysis of the Rotary core taken from the Humphrey Lease, Well No. 12, Bourbon County, Kansas and submitted to our laboratory on May 20, 1967.

Your business is greatly appreciated.

Very truly yours,

OILFIELD RESEARCH LABORATORIES

*Benjamin R. Pearman*  
Benjamin R. Pearman

BRP:rf

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**Oilfield Research Laboratories**

**GENERAL INFORMATION & SUMMARY**

|  |  |                       |                 |                 |                     |
|--|--|-----------------------|-----------------|-----------------|---------------------|
| <b>Company</b>   | <b>CRA, Incorporated</b>                                   | <b>Lease</b>          | <b>Humphrey</b> | <b>Well No.</b> | <b>12</b>           |
| <b>Location</b>  | <b>540' EWL &amp; 990' NSL, NE<math>\frac{1}{4}</math></b> |                       |                 |                 |                     |
| <b>Section</b>   | <b>36</b>  | <b>Twp.</b>           | <b>24S</b>      | <b>Rge.</b>     | <b>21E</b>          |
|  |  |                       |                 | <b>County</b>   | <b>Bourbon</b>      |
|  |  |                       |                 | <b>State</b>    | <b>Kansas</b>       |
| <b>Name of Sand</b>  | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>Bartlesville</b> |
| <b>Top of Core</b>   | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>607.0</b>        |
| <b>Bottom of Core</b>  | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>658.0</b>        |
| <b>Top of Sand</b>   | - - - - -  | (Analyzed)            | - - - - -       | - - - - -       | <b>607.0</b>        |
| <b>Bottom of Sand</b>  | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>651.0</b>        |
| <b>Total Feet of Permeable Sand</b>                                    | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>38.2</b>         |
| <b>Total Feet of Floodable Sand</b>                                    | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>18.8</b>         |
| <b>Distribution of Permeable Sand:</b>                                 |  |                       |                 |                 |                     |
| <b>Permeability Range</b>  |  | <b>Feet</b>           |                 | <b>Cum. Ft.</b> |                     |
| <b>Millidarcys</b>   |  |                       |                 |                 |                     |
| 0 - 5  |  | 9.5                   |                 | 9.5             |                     |
| 5 - 10   |  | 12.1                  |                 | 21.6            |                     |
| 10 - 20  |  | 5.3                   |                 | 26.9            |                     |
| 20 - 50  |  | 10.3                  |                 | 37.2            |                     |
| 50 & above   |  | 1.0                   |                 | 38.2            |                     |
| <b>Average Permeability Millidarcys</b>                                | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>16.7</b>         |
| <b>Average Percent Porosity</b>  | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>18.9</b>         |
| <b>Average Percent Oil Saturation</b>                                  | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>41.7</b>         |
| <b>Average Percent Water Saturation</b>                                | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>39.7</b>         |
| <b>Average Oil Content, Bbls./A. Ft.</b>                               | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>620.</b>         |
| <b>Total Oil Content, Bbls./Acre</b>                                   | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>24,319.</b>      |
| <b>Average Percent Oil Recovery by Laboratory Flooding Tests</b>       | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>13.7</b>         |
| <b>Average Oil Recovery by Laboratory Flooding Tests, Bbls./A. Ft.</b> | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>212.</b>         |
| <b>Total Oil Recovery by Laboratory Flooding Tests, Bbls./Acre</b>     | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>3,990.</b>       |
| <b>Total Calculated Oil Recovery, Bbls./Acre</b>                       | -  | (Primary & Secondary) | -               | -               | <b>6,960.</b>       |
| <b>Packer Setting, Feet</b>  | - - - - -  | - - - - -             | - - - - -       | - - - - -       |                     |
| <b>Viscosity, Centipoises @</b>  | - - - - -  | - - - - -             | - - - - -       | - - - - -       |                     |
| <b>A. P. I. Gravity, degrees @ 60 °F</b>                               | - - - - -  | - - - - -             | - - - - -       | - - - - -       |                     |
| <b>Elevation, Feet</b>   | - - - - -  | - - - - -             | - - - - -       | - - - - -       | <b>1014.9</b>       |

Fresh water mud was used as the circulating fluid while taking this core. The core was sampled and the samples sealed in cans and plastic bags by a representative of Oilfield Research Laboratories. The well was drilled in virgin territory.

FORMATION CORED

The detailed log of the formation cored is as follows:

Depth Interval, Description  
Feet \_\_\_\_\_

607.0 - 607.4 - Grayish light brown, laminated, shaly sandstone.  
607.4 - 608.3 - Brown, slightly shaly sandstone.  
608.3 - 609.0 - Grayish light brown, laminated, shaly sandstone.  
609.0 - 609.3 - Gray sandy shale.  
609.3 - 610.2 - Brown sandstone.  
610.2 - 610.4 - Gray shale.  
610.4 - 610.7 - Grayish light brown, laminated, shaly sandstone.  
610.7 - 611.1 - Gray, laminated, sandy shale.  
611.1 - 612.0 - Brown sandstone.  
612.0 - 612.8 - Brown, laminated, shaly sandstone.  
612.8 - 613.9 - Gray shale.  
613.9 - 614.9 - Grayish light brown, shaly sandstone.  
614.9 - 615.2 - Sandy conglomerate.  
615.2 - 616.0 - Brown shaly sandstone.  
616.0 - 617.7 - Gray shale.  
617.7 - 619.8 - Brown sandstone.  
619.8 - 620.6 - Grayish brown, laminated, shaly sandstone.  
620.6 - 623.5 - Brown shaly sandstone.  
623.5 - 626.0 - Light brown, laminated, shaly sandstone.

626.0 - 629.3 - Brown sandstone.  
629.3 - 630.1 - Gray, laminated, sandy shale.  
630.1 - 631.5 - Brown, slightly shaly sandstone.  
631.5 - 632.5 - Gray and light brown, laminated, shaly sandstone.  
632.5 - 634.8 - Brown, laminated, slightly shaly sandstone.  
634.8 - 635.3 - Grayish brown, laminated, shaly sandstone.  
635.3 - 635.5 - Gray shale.  
635.5 - 637.9 - Brown sandstone.  
637.9 - 638.9 - Brown, laminated, slightly shaly sandstone.  
638.9 - 640.4 - Dark carbonaceous sandstone.  
640.4 - 640.8 - Light brown, laminated, slightly carbonaceous, shaly sandstone.  
640.8 - 651.0 - Dark carbonaceous sandstone.  
651.0 - 652.0 - Dark carbonaceous conglomerate.  
652.0 - 653.3 - Gray, shaly conglomerate.  
653.3 - 654.3 - Coal.  
654.3 - 658.0 - Black shale.

Coring was started at a depth of 607.0 feet in sandstone and completed at 658.0 feet in shale. This core shows a total of 39.2 feet of sandstone. For the most part, the pay is made up of brown, more or less, shaly sandstone.

#### PERMEABILITY

For the sake of distribution, the core was divided into three sections. The weighted average permeability of the upper, middle and lower sections is 16.2, 21.6 and 10.0 millidarcys respectively; the overall average being 16.7 (See Table III). By observing the data given on the coregraph, it is noticeable that the sand has a rather

irregular permeability profile. The permeability of the sand varies from impermeable to a maximum of 54. millidarcys.

#### PERCENT SATURATION & OIL CONTENT

The sand in this core shows a good weighted average percent oil saturation, namely, 41.7. The weighted average percent oil saturation of the upper, middle and lower sections is 32.8, 41.9 and 45.5 respectively. The weighted average percent water saturation of the upper, middle and lower sections is 50.1, 40.0 and 34.5 respectively; the overall average being 39.7 (See Table III). This gives an overall weighted average total fluid saturation of 81.4 percent.

The weighted average oil content of the upper, middle and lower sections is 460, 629 and 681 barrels per acre foot respectively; the overall average being 620. The total oil content, as shown by this core, is 24,319 barrels per acre (See Table III).

#### LABORATORY FLOODING TESTS

The sand in this core responded to laboratory flooding tests, as a total recovery of 3,990 barrels of oil per acre was obtained from 18.8 feet of sand. The weighted average percent oil saturation was reduced from 42.5 to 28.8, or represents an average recovery of 13.7 percent. The weighted average effective permeability of the samples is 1.13 millidarcys, while the average initial fluid production pressure is 27.6 pounds per square inch (See Table V).

By observing the data given in Table IV, you will note that of the 42 samples tested, 22 produced water and 19 oil. This indicates that approximately 45 percent of the sand represented by these samples is floodable pay sand. The tests also show that the sand has a wide

variation in effective permeability to water.

### CONCLUSION

The results of the laboratory tests indicate that efficient primary operations in the vicinity of this well should recover approximately 2,270 barrels of oil per acre or an average of 65 barrels per acre foot from 35.0 feet of pay sand. An additional 4,690 barrels of oil per acre or an average of 249 barrels per acre foot can be recovered by efficient waterflooding operations. These recovery values were calculated using the following data and assumptions:

|   |             |
|---|-------------|
| Original formation volume factor                                  | 1.06        |
| Reservoir water saturation, percent                               | 30.0        |
| Expected primary recovery, estimated, percent<br>(607.0 - 638.9 ) | 6.0         |
| Expected primary recovery, estimated, percent<br>(638.9 - 651.0)  | 2.0         |
| Average porosity, percent   | 18.8 - 19.4 |
| Oil saturation after flooding, percent                            | 28.8        |
| Performance factor, percent                                       | 50.0        |
| Net floodable pay sand, feet                                      | 18.8        |

This core shows a pay sand section (616.0 - 638.9) having a good oil saturation, a moderate water saturation and a wide variation in effective permeability to water. The lower zone (638.9 - 651.0) is carbonaceous sand that will probably respond to primary efforts, but will not respond to water-flooding.

**Oilfield Research Laboratories**

**RESULTS OF SATURATION & PERMEABILITY TESTS**

**TABLE 1-B**

CRA, Incorporated  
Company

Lease  
Humphrey

Well No. — 12

| Sample No. | Depth, Feet | Effective Porosity Percent | Percent Saturation |       |       | Oil Content Bbls./A Ft. | Penn., Mill. | Feet of Sand | Cum. Ft. | Total Oil Content | Perm. Capacity Ft. X md. |
|------------|-------------|----------------------------|--------------------|-------|-------|-------------------------|--------------|--------------|----------|-------------------|--------------------------|
|            |             |                            | Oil                | Water | Total |                         |              |              |          |                   |                          |
| 1          | 607.1       | 15.8                       | 29                 | 56    | 85    | 355                     | 3.7          | 0.4          | 0.4      | 142               | 1.48                     |
| 2          | 608.1       | 20.4                       | 37                 | 42    | 79    | 586                     | 6.4          | 0.9          | 1.3      | 529               | 5.76                     |
| 3          | 609.4       | 18.2                       | 42                 | 43    | 85    | 593                     | 50.          | 0.9          | 2.2      | 534               | 45.00                    |
| 4          | 610.5       | 13.6                       | 22                 | 72    | 94    | 232                     | 3.9          | 0.3          | 2.5      | 70                | 1.17                     |
| 5          | 611.4       | 19.3                       | 38                 | 49    | 87    | 569                     | 23.          | 0.9          | 3.4      | 511               | 20.70                    |
| 6          | 612.1       | 17.9                       | 30                 | 52    | 82    | 417                     | 6.2          | 0.8          | 4.2      | 334               | 4.96                     |
| 7          | 614.1       | 17.8                       | 23                 | 51    | 74    | 318                     | 9.7          | 1.0          | 5.2      | 318               | 9.70                     |
| 8          | 615.3       | 16.2                       | 32                 | 54    | 86    | 402                     | 10.          | 0.8          | 6.0      | 322               | 8.00                     |
| 9          | 618.1       | 20.6                       | 48                 | 31    | 79    | 767                     | 46.          | 0.9          | 6.9      | 690               | 41.40                    |
| 10         | 619.1       | 20.3                       | 53                 | 30    | 83    | 835                     | 33.          | 1.2          | 8.1      | 1,008             | 39.60                    |
| 11         | 620.1       | 16.2                       | 29                 | 52    | 81    | 364                     | 7.6          | 0.8          | 8.9      | 292               | 6.08                     |
| 12         | 621.1       | 21.4                       | 55                 | 27    | 82    | 913                     | 27.          | 1.0          | 9.9      | 913               | 27.00                    |
| 13         | 622.1       | 18.5                       | 36                 | 43    | 79    | 517                     | 5.8          | 1.0          | 10.9     | 517               | 5.80                     |
| 14         | 623.1       | 15.9                       | 44                 | 44    | 88    | 543                     | 15.          | 0.9          | 11.8     | 489               | 13.50                    |
| 15         | 624.1       | 18.5                       | 36                 | 43    | 79    | 517                     | 4.0          | 1.1          | 12.9     | 569               | 4.40                     |
| 16         | 625.1       | 17.6                       | 38                 | 45    | 83    | 519                     | 4.3          | 1.4          | 14.3     | 726               | 6.02                     |
| 17         | 626.1       | 20.5                       | 51                 | 40    | 91    | 811                     | 15.          | 0.6          | 14.9     | 486               | 9.00                     |
| 18         | 627.1       | 21.3                       | 49                 | 28    | 77    | 810                     | 54.          | 1.0          | 15.9     | 810               | 54.00                    |
| 19         | 628.1       | 19.9                       | 49                 | 36    | 85    | 757                     | 46.          | 1.7          | 17.6     | 1,288             | 78.20                    |
| 20         | 630.2       | 19.4                       | 34                 | 43    | 77    | 512                     | 19.          | 0.4          | 18.0     | 205               | 7.60                     |
| 21         | 631.1       | 19.5                       | 38                 | 39    | 77    | 575                     | 7.0          | 1.0          | 19.0     | 575               | 7.00                     |
| 22         | 632.1       | 15.3                       | 29                 | 55    | 84    | 344                     | Imp.         | 1.0          | 20.0     | 344               | 0.00                     |
| 23         | 633.1       | 16.0                       | 31                 | 53    | 84    | 385                     | 4.5          | 1.1          | 21.1     | 424               | 4.95                     |
| 24         | 634.1       | 17.0                       | 36                 | 51    | 87    | 474                     | 4.7          | 1.2          | 22.3     | 569               | 5.64                     |

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**RESULTS OF SATURATION & PERMEABILITY TESTS**

**TABLE 1-B**

| Company | CRA, Inc. | Lease | Humphrey | Well No. | 12         |             |                            |                    |       |       |                           |              |              |                   |                          |
|---------|-----------|-------|----------|----------|------------|-------------|----------------------------|--------------------|-------|-------|---------------------------|--------------|--------------|-------------------|--------------------------|
|         |           |       |          |          | Sample No. | Depth, Feet | Effective Porosity Percent | Percent Saturation |       |       | Oil Content Bbls. / A Ft. | Perm., Mill. | Feet of Sand | Total Oil Content | Perm. Capacity Ft. X md. |
|         |           |       |          |          |            |             |                            | Oil                | Water | Total |                           |              | Ft.          | Cum. Ft.          |                          |
| 25      | 635.1     | 18.0  | 45       | 42       | 87         | 628         |                            | 1.2                | 0.5   | 22.8  | 314                       | 0.60         |              |                   |                          |
| 26      | 636.1     | 21.1  | 42       | 40       | 82         | 687         |                            | 41.                | 1.0   | 23.8  | 687                       | 41.00        |              |                   |                          |
| 27      | 637.1     | 21.4  | 49       | 32       | 81         | 812         |                            | 41.                | 1.3   | 25.1  | 1,058                     | 53.30        |              |                   |                          |
| 28      | 638.1     | 21.1  | 40       | 33       | 73         | 654         |                            | 7.6                | 1.0   | 26.1  | 654                       | 7.60         |              |                   |                          |
| 29      | 639.1     | 20.5  | 48       | 27       | 75         | 762         |                            | 12.                | 0.7   | 26.8  | 534                       | 8.40         |              |                   |                          |
| 30      | 640.1     | 20.8  | 49       | 31       | 80         | 790         |                            | 8.3                | 0.8   | 27.6  | 632                       | 6.64         |              |                   |                          |
| 31      | 641.1     | 21.8  | 48       | 24       | 72         | 811         |                            | 15.                | 0.7   | 28.3  | 569                       | 10.50        |              |                   |                          |
| 32      | 642.1     | 20.1  | 42       | 32       | 74         | 654         |                            | 8.2                | 1.0   | 29.3  | 654                       | 8.20         |              |                   |                          |
| 33      | 643.1     | 19.0  | 45       | 34       | 79         | 663         |                            | 4.4                | 1.0   | 30.3  | 663                       | 4.40         |              |                   |                          |
| 34      | 644.1     | 18.6  | 42       | 37       | 79         | 605         |                            | 5.1                | 1.0   | 31.3  | 605                       | 5.10         |              |                   |                          |
| 35      | 645.1     | 19.3  | 41       | 34       | 75         | 613         |                            | 7.4                | 1.0   | 32.3  | 613                       | 7.40         |              |                   |                          |
| 36      | 646.1     | 20.3  | 46       | 33       | 79         | 724         |                            | 6.1                | 1.0   | 33.3  | 724                       | 6.10         |              |                   |                          |
| 37      | 647.1     | 17.7  | 45       | 37       | 82         | 617         |                            | 0.95               | 1.0   | 34.3  | 617                       | 0.95         |              |                   |                          |
| 38      | 648.1     | 20.1  | 50       | 31       | 81         | 779         |                            | 11.                | 1.0   | 35.3  | 779                       | 11.00        |              |                   |                          |
| 39      | 649.1     | 20.1  | 52       | 33       | 85         | 810         |                            | 15.                | 1.0   | 36.3  | 810                       | 15.00        |              |                   |                          |
| 40      | 650.1     | 20.0  | 41       | 32       | 73         | 636         |                            | 31.                | 1.4   | 37.7  | 890                       | 43.40        |              |                   |                          |
| 41      | 651.1     | 16.6  | 63       | 34       | 97         | 809         |                            | 3.0                | 1.0   | 38.7  | 809                       | 3.00         |              |                   |                          |
| 42      | 652.1     | 9.9   | 11       | 84       | 95         | 84          |                            | 0.78               | 0.5   | 39.2  | 42                        | 0.39         |              |                   |                          |
|         |           |       |          |          |            |             |                            |                    |       |       | Total                     | -24,319      |              |                   |                          |

**Oilfield Research Laboratories**

**SUMMARY OF PERMEABILITY & SATURATION TESTS**

**TABLE III**

| Company                 | CRA, Inc. | Lease                    |                          | Humphrey                                |                                       | Well No. 12                           |        |
|-------------------------|-----------|--------------------------|--------------------------|---|---------------------------------------|---------------------------------------|--------|
|                         |           | Depth Interval,<br>Feet  | Feet of Core<br>Analyzed | Average<br>Permeability,<br>Millidarcys | Permeability<br>Capacity<br>Ft. x Md. |                                       |        |
|                         |           | 607.0 - 616.0            | 6.0                      | 16.2                                    | 96.77                                 |                                       |        |
|                         |           | 617.7 - 638.9            | 19.1                     | 21.6                                    | 412.69                                |                                       |        |
|                         |           | 638.9 - 652.5            | 13.1                     | 10.0                                    | 130.48                                |                                       |        |
|                         |           | 607.0 - 652.5            | 38.2                     | 16.7                                    | 639.94                                |                                       |        |
| Depth Interval,<br>Feet |           | Feet of Core<br>Analyzed |                          | Average<br>Percent<br>Porosity          | Average<br>Percent Oil<br>Saturation  | Average<br>Oil Content<br>Bbl./A. Ft. |        |
|                         |           |                          |                          |   |                                       | Total Oil<br>Content<br>Bbls./Acre    |        |
|                         |           | 607.0 - 616.0            | 6.0                      | 17.9                                    | 32.8                                  | 460                                   | 2,760  |
|                         |           | 617.7 - 638.9            | 20.1                     | 19.1                                    | 41.9                                  | 629                                   | 12,618 |
|                         |           | 638.9 - 652.5            | 13.1                     | 19.2                                    | 45.5                                  | 681                                   | 8,941  |
|                         |           | 607.0 - 652.5            | 39.2                     | 18.9                                    | 41.7                                  | 39.7                                  | 24,319 |

**Oilfield Research Laboratories**

**RESULTS OF LABORATORY FLOODING TESTS**

**TABLE IV**

| Company | CRA, Inc. | Lease      |             | Humphrey                  |                           | Well No. 12           |                               |                                      |  |     |       |       |    |
|---------|-----------|------------|-------------|---------------------------|---------------------------|-----------------------|-------------------------------|--------------------------------------|--|-----|-------|-------|----|
|         |           | Sample No. | Depth, Feet | Original Oil Saturation % | Oil Recovery Bbls./A. Ft. | Residual Saturation % | Volume of Water Recovered cc* | Effective Permeability Millidarcys** | Initial Fluid Production Pressure Lbs./Sq. In. |     |       |       |    |
|         | 1         | 607.1      | 16.2        | 30                        | 377                       | 0                     | 30                            | 64                                   | 377  | 8   | 0.300 | 40    |    |
|         | 2         | 608.1      | 20.0        | 37                        | 573                       | 7                     | 108                           | 59                                   | 465  | 42  | 1.10  | 25    |    |
|         | 3         | 609.4      | 18.7        | 42                        | 609                       | 13                    | 188                           | 29                                   | 421  | 112 | 3.70  | 20    |    |
|         | 4         | 610.5      | 14.0        | 26                        | 282                       | 0                     | 0                             | 26                                   | 73   | 282 | 5     | 0.200 | 45 |
|         | 5         | 611.4      | 19.0        | 38                        | 559                       | 2                     | 30                            | 36                                   | 53   | 529 | 28    | 0.800 | 25 |
|         | 6         | 612.1      | 17.5        | 30                        | 406                       | 0                     | 0                             | 30                                   | 68   | 406 | 24    | 0.800 | 30 |
|         | 7         | 614.1      | 18.1        | 23                        | 322                       | 0                     | 0                             | 23                                   | 66   | 322 | 4     | 0.200 | 45 |
|         | 8         | 615.3      | 16.0        | 33                        | 409                       | 0                     | 0                             | 33                                   | 55   | 409 | 0     | Imp.  | -  |
|         | 9         | 618.1      | 21.0        | 48                        | 781                       | 24                    | 391                           | 24                                   | 60   | 390 | 87    | 2.70  | 20 |
|         | 10        | 619.1      | 20.0        | 53                        | 821                       | 27                    | 418                           | 26                                   | 73   | 403 | 37    | 1.50  | 25 |
|         | 11        | 620.1      | 16.5        | 29                        | 371                       | 3                     | 38                            | 26                                   | 73   | 333 | 4     | 0.200 | 35 |
|         | 12        | 621.1      | 21.7        | 55                        | 924                       | 24                    | 403                           | 31                                   | 68   | 521 | 48    | 1.80  | 20 |
|         | 13        | 622.1      | 18.0        | 36                        | 502                       | 12                    | 168                           | 24                                   | 67   | 334 | 10    | 0.400 | 30 |
|         | 14        | 623.1      | 16.4        | 44                        | 560                       | 16                    | 204                           | 28                                   | 69   | 356 | 31    | 0.900 | 20 |
|         | 15        | 624.1      | 18.7        | 36                        | 521                       | 0                     | 0                             | 36                                   | 45   | 521 | 0     | Imp.  | -  |
|         | 16        | 625.1      | 17.5        | 36                        | 488                       | 0                     | 0                             | 36                                   | 46   | 488 | 0     | Imp.  | -  |
|         | 17        | 626.1      | 20.6        | 51                        | 814                       | 16                    | 256                           | 35                                   | 64   | 558 | 10    | 0.400 | 25 |
|         | 18        | 627.1      | 20.9        | 49                        | 794                       | 21                    | 340                           | 28                                   | 71   | 454 | 52    | 1.60  | 20 |
|         | 19        | 628.1      | 19.7        | 49                        | 749                       | 24                    | 367                           | 25                                   | 74   | 382 | 61    | 2.10  | 20 |
|         | 20        | 630.2      | 19.3        | 34                        | 509                       | 7                     | 105                           | 27                                   | 71   | 404 | 8     | 0.334 | 25 |
|         | 21        | 631.1      | 19.7        | 38                        | 581                       | 5                     | 76                            | 33                                   | 64   | 505 | 4     | 0.200 | 40 |
|         | 22        | 632.1      | 15.1        | 29                        | 690                       | 0                     | 0                             | 29                                   | 56   | 690 | 0     | Imp.  | -  |
|         | 23        | 633.1      | 16.4        | 31                        | 394                       | 3                     | 38                            | 28                                   | 67   | 356 | 2     | 0.100 | 45 |
|         | 24        | 634.1      | 17.3        | 36                        | 483                       | 5                     | 67                            | 31                                   | 59   | 416 | 0     | 0.025 | 35 |

Notes: cc—cubic centimeter.

\*—Volume of water recovered at the time of maximum oil recovery.

\*\*—Determined by passing water through sample which still contains residual oil.

**Oilfield Research Laboratories**

**RESULTS OF LABORATORY FLOODING TESTS**

**TABLE IV**

| Company | CRA, Inc. |             |                            |                           |              |                |              |                       |       |                               |                                      |
|---------|-----------|-------------|----------------------------|---------------------------|--------------|----------------|--------------|-----------------------|-------|-------------------------------|--------------------------------------|
|         |           | Depth, Feet | Effective Porosity Percent | Original Oil Saturation % | Bbls./A. Ft. | Oil Recovery % | Bbls./A. Ft. | Residual Saturation % | Water | Volume of Water Recovered cc* | Effective Permeability Millidarcys** |
| 25      | 635.1     | 17.7        | 4.6                        | 631                       | 0            | 46             | 4.3          | 631                   | 0     | Imp.                          | 1.20                                 |
| 26      | 636.1     | 21.2        | 4.2                        | 691                       | 14           | 230            | 28           | 62                    | 461   | 48                            | 30                                   |
| 27      | 637.1     | 20.9        | 4.9                        | 794                       | 15           | 243            | 34           | 57                    | 551   | 34                            | 30                                   |
| 28      | 638.1     | 20.8        | 4.0                        | 645                       | 9            | 145            | 31           | 65                    | 500   | 10                            | 0.334                                |
| 29      | 639.1     | 20.8        | 5.0                        | 806                       | 0            | 0              | 50           | 26                    | 806   | 0                             | 35                                   |
| 30      | 640.1     | 20.8        | 4.9                        | 789                       | 0            | 0              | 49           | 32                    | 789   | 0                             | —                                    |
| 31      | 641.1     | 21.5        | 4.8                        | 800                       | 0            | 0              | 48           | 27                    | 800   | 0                             | —                                    |
| 32      | 642.1     | 20.3        | 4.4                        | 691                       | 0            | 0              | 44           | 31                    | 691   | 0                             | —                                    |
| 33      | 643.1     | 18.7        | 4.5                        | 651                       | 0            | 0              | 45           | 37                    | 651   | 0                             | —                                    |
| 34      | 644.1     | 18.7        | 4.1                        | 594                       | 0            | 0              | 41           | 39                    | 594   | 0                             | —                                    |
| 35      | 645.1     | 19.0        | 4.2                        | 619                       | 0            | 0              | 42           | 35                    | 619   | 0                             | —                                    |
| 36      | 646.1     | 20.3        | 4.7                        | 739                       | 0            | 0              | 47           | 36                    | 739   | 0                             | —                                    |
| 37      | 647.1     | 17.4        | 4.5                        | 606                       | 0            | 0              | 45           | 36                    | 606   | 0                             | —                                    |
| 38      | 648.1     | 20.1        | 5.0                        | 779                       | 0            | 0              | 50           | 33                    | 779   | 0                             | —                                    |
| 39      | 649.1     | 20.0        | 5.1                        | 790                       | 0            | 0              | 51           | 33                    | 790   | 0                             | —                                    |
| 40      | 650.1     | 20.0        | 4.3                        | 666                       | 0            | 0              | 43           | 33                    | 666   | 0                             | —                                    |
| 41      | 651.1     | 16.6        | 6.1                        | 786                       | 0            | 0              | 61           | 37                    | 786   | 0                             | —                                    |
| 42      | 652.1     | 10.1        | 12                         | 94                        | 0            | 0              | 12           | 85                    | 94    | 0                             | —                                    |

Notes: cc—cubic centimeter.

\*—Volume of water recovered at the time of maximum oil recovery.

\*\*—Determined by passing water through sample which still contains residual oil.

**Oilfield Research Laboratories**

**SUMMARY OF LABORATORY FLOODING TESTS**

**TABLE V**

| Company   | CRA, Inc.     | Lease         | Humphrey      | Well No. |
|---|---------------|---------------|---------------|----------|
| Depth Interval, Feet                              | 607.0 - 616.0 | 617.7 - 638.9 | 607.0 - 638.9 |          |
| Feet of Core Analyzed                             | 2.7           | 16.1          |               | 18.8     |
| Average Percent Porosity                          | 19.2          | 19.4          |               | 19.4     |
| Average Percent Original Oil Saturation           | 38.9          | 43.1          |               | 42.5     |
| Average Percent Oil Recovery                      | 7.3           | 14.7          |               | 13.7     |
| Average Percent Residual Oil Saturation           | 31.6          | 28.4          |               | 28.8     |
| Average Percent Residual Water Saturation         | 59.4          | 59.5          |               | 59.4     |
| Average Percent Total Residual Fluid Saturation   | 91.0          | 87.9          |               | 88.2     |
| Average Original Oil Content, Bbls./A. Ft.        | 581.          | 661.          |               | 649.     |
| Average Oil Recovery, Bbls./A. Ft.                | 109.          | 230.          |               | 212.     |
| Average Residual Oil Content, Bbls./A. Ft.        | 472.          | 431.          |               | 437.     |
| Total Original Oil Content, Bbls./Acre            | 1,567.        | 10,646.       |               | 12,213.  |
| Total Oil Recovery, Bbls./Acre                    | 293.          | 3,697.        |               | 3,990.   |
| Total Residual Oil Content, Bbls./Acre            | 1,274.        | 6,949.        |               | 8,223.   |
| Average Effective Permeability, Millidarcys       | 1.87          | 1.01          |               | 1.13     |
| Average Initial Fluid Production Pressure, p.s.i. | 23.3          | 28.4          |               | 27.6     |

NOTE: Only those samples which recovered oil were used in calculating  
the above averages.