

# OILFIELD RESEARCH LABORATORIES

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- REGISTERED ENGINEERS -

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August 11, 1960

Schermerhorn Oil Corporation  
P.O. Box 287  
Tulsa, Oklahoma

Gentlemen:

Enclosed herewith is the report of the analysis of the 2 $\frac{1}{2}$ " Rotary core taken from the Pavilcek-Perry Lease, Well No. W-10, Allen County, Kansas, and submitted to our laboratory on August 5, 1960.

Your business is greatly appreciated.

Very truly yours,

OILFIELD RESEARCH LABORATORIES

*Carl L. McElrea*  
Carl L. McElrea

CLM:cw

1 c. - Schermerhorn Oil Corporation  
Route #1  
Earlton, Kansas

well 7 ✓

L - 1.2

F - 2

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## GENERAL INFORMATION & SUMMARY

Company Schermerhorn Oil Corporation Lease Pavilcek-Perry Well No. W-10

Location 330' East of Center

Section 34 Twp. 25S Rge. 21E County Allen State Kansas

|                              |              |
|------------------------------|--------------|
| Name of Sand                 | Bartlesville |
| Top of Core                  | 640.5        |
| Bottom of Core               | 669.5        |
| Pay                          |              |
| Top of/Sand                  | 652.2        |
| Pay                          |              |
| Bottom of/Sand               | 661.0        |
| Total Feet of Permeable Sand | 12.8         |
| Good                         |              |
| Total Feet of Floodable Sand | 8.8          |

**Distribution of Permeable Sand:**  
Permeability Range  
Millidarcys

|             | Feet | Cum. Ft. |
|-------------|------|----------|
| 0 - 25      | 3.2  | 3.2      |
| 25 - 50     | 2.3  | 5.5      |
| 50 - 75     | 2.3  | 7.8      |
| 75 - 100    | 1.5  | 9.3      |
| 100 & above | 3.5  | 12.8     |

|   |         |
|---|---------|
| Average Permeability Millidarcys                                | 58.9    |
| Average Percent Porosity  | 18.7    |
| Average Percent Oil Saturation                                  | 46.7    |
| Average Percent Water Saturation                                | 41.6    |
| Average Oil Content, Bbls./A. Ft.                               | 698.    |
| Total Oil Content, Bbls./Acre                                   | 10,112. |
| Average Percent Oil Recovery by Laboratory Flooding Tests       | 29.3    |
| Average Oil Recovery by Laboratory Flooding Tests, Bbls./A. Ft. | 465.    |
| Total Oil Recovery by Laboratory Flooding Tests, Bbls./Acre     | 4,555   |
| Total Calculated Oil Recovery, Bbls./Acre                       | 2,430.  |
| Packer Setting, Feet  |         |
| Viscosity, Centipoises @  |         |
| A.P.G. Gravity, degrees @ 60 °F                                 |         |
| Elevation, Feet   |         |

A fresh water mud was used as the circulating fluid during the coring of the sand.

This core was sampled and the samples were sealed in cans by a representative of Oilfield Research Laboratories.

### FORMATION CORED

The detailed log of the formation cored is as follows:

| Depth Interval,<br>Feet | Description |
|-------------------------|-------------|
|-------------------------|-------------|

|               |                                       |
|---------------|---------------------------------------|
| 640.5 - 646.7 | Light brown shaley sandstone.         |
| 646.7 - 647.5 | Laminated sandy shale.                |
| 647.5 - 650.5 | Light brown shaley sandstone.         |
| 650.5 - 652.2 | Laminated sandstone and shale.        |
| 652.2 - 661.0 | Dark brown sandstone.                 |
| 661.0 - 662.0 | Brown to dark carbonaceous sandstone. |
| 662.0 - 669.5 | Shale.                                |

Coring was started at a depth of 640.5 feet in light brown shaley sandstone and completed at 669.5 feet in shale. This core shows a total of 19.0 feet of sandstone. For the most part, the pay is made up of dark brown sandstone.

### PERMEABILITY

For the sake of distribution, the core was divided into two sections. The weighted average permeability of the upper and lower sections is 21.4 and 70.3 millidarcys respectively; the overall average being 58.9 (See Table III). By observing the data given on the coregraph, it is noticeable that the sand has an irregular permeability profile. The permeability of the sand varies from 2.1 to a maximum of 127 millidarcys.

### PERCENT SATURATION & OIL CONTENT

The sand in this core shows a very good weighted average percent

oil saturation, namely, 46.7. The weighted average percent oil saturation of the upper and lower sections is 28.9 and 55.4 respectively. The weighted average percent water saturation of the upper and lower sections is 64.2 and 32.2 respectively; the overall average being 41.6 (See Table III). This gives an overall weighted average total fluid saturation of 88.3 percent.

The weighted average oil content of the upper and lower sections is 372 and 854 barrels per acre foot respectively; the overall average being 698. The total oil content, as shown by this core, is 10,112 barrels per acre of which 8,364 barrels are in the lower section (See Table III).

#### LABORATORY FLOODING TESTS

The sand in this core responded very well to laboratory flooding tests, as a total recovery of 4,555 barrels of oil per acre was obtained from 9.8 feet of sand. The weighted average percent oil saturation was reduced from 56.4 to 27.1, or represents an average recovery of 29.3 percent. The weighted average effective permeability of the samples is 6.74 millidarcys, while the average initial fluid production pressure is 8.3 pounds per square inch (See Table V).

By observing the data given in Table IV, you will note that of the 14 samples tested, 13 produced water and 9 oil. This indicates that approximately 64 percent of the sand represented by these samples is floodable pay sand. The tests also show that the floodable sand has a comparatively uniform effective permeability.

#### CONCLUSION

It is evident from the enclosed data that an efficient water-flood will recover approximately 2,430 barrels of oil per acre from the area of which this core is representative. This represents an average recovery of 276 barrels of oil per acre foot from the 8.8 feet of good

floodable pay sand analysed. The following factors were used in calculating this recovery:

|  |      |
|--|------|
| Original formation volume factor           | 1.06 |
| Present formation volume factor            | 1.01 |
| True water saturation, percent             | 32.0 |
| Primary oil recovery, percent              | 4.0  |
| Calculated present oil saturation, percent | 60.8 |
| Porosity, percent                          | 20.7 |
| Oil saturation at abandonment, percent     | 26.0 |
| Performance factor                         | 50.0 |

The analysis results show 8.8 feet of good floodable pay sand in the interval extending from the depth of 652.2 to 661.0 feet. The floodable sand has very good oil and normal water saturations and good effective permeability.

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**RESULTS OF PERMEABILITY TESTS**  
**TABLE I**

Company Schermerhorn Oil Corporation Lease Pavilcek-Perry Well No. W-10

| Sample No. | Depth Feet | Permeability Millidarcy | Feet of Core |          | Permeability Capacity Ft. x Md. |
|------------|------------|-------------------------|--------------|----------|---------------------------------|
|            |            |                         | Ft.          | Cum. Ft. |                                 |
| 1          | 647.9      | 15.                     | 0.6          | 0.6      | 9.00                            |
| 2          | 648.4      | 9.1                     | 0.6          | 1.2      | 5.46                            |
| 3          | 648.9      | 5.7                     | 0.5          | 1.7      | 2.85                            |
| 4          | 649.4      | 45.                     | 0.5          | 2.2      | 22.50                           |
| 5          | 649.9      | 29.                     | 0.5          | 2.7      | 14.50                           |
| 6          | 650.4      | 33.                     | 0.3          | 3.0      | 9.90                            |
| 7          | 650.9      | Imp.                    | 0.7          | 3.7      | 0.00                            |
| 8          | 651.4      | Imp.                    | 0.5          | 4.2      | 0.00                            |
| 9          | 651.9      | Imp.                    | 0.5          | 4.7      | 0.00                            |
| 10         | 652.4      | 16.                     | 0.5          | 5.2      | 8.00                            |
| 11         | 652.9      | 30.                     | 0.5          | 5.7      | 15.00                           |
| 12         | 653.4      | 55.                     | 0.5          | 6.2      | 27.50                           |
| 13         | 653.9      | 85.                     | 0.5          | 6.7      | 42.50                           |
| 14         | 654.4      | 124.                    | 0.5          | 7.2      | 62.00                           |
| 15         | 654.9      | 114.                    | 0.5          | 7.7      | 57.00                           |
| 16         | 655.4      | 102.                    | 0.5          | 8.2      | 51.00                           |
| 17         | 655.9      | 127.                    | 0.5          | 8.7      | 63.50                           |
| 18         | 656.4      | 31.                     | 0.5          | 9.2      | 15.50                           |
| 19         | 656.9      | 53.                     | 0.5          | 9.7      | 26.50                           |
| 20         | 657.4      | 121.                    | 0.5          | 10.2     | 60.50                           |
| 21         | 657.9      | 42.                     | 0.5          | 10.7     | 21.00                           |
| 22         | 658.4      | 101.                    | 0.5          | 11.2     | 50.50                           |
| 23         | 658.9      | 72.                     | 0.5          | 11.7     | 36.00                           |
| 24         | 659.4      | 76.                     | 0.5          | 12.2     | 38.00                           |
| 25         | 659.9      | 111.                    | 0.5          | 12.7     | 55.50                           |
| 26         | 660.4      | 75.                     | 0.5          | 13.2     | 37.50                           |
| 27         | 660.9      | 66.                     | 0.3          | 13.5     | 19.80                           |
| 28         | 661.4      | 2.1                     | 1.0          | 14.5     | 2.10                            |

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RESULTS OF SATURATION TESTS

TABLE II

Company Schermerhorn Oil Corporation Lease Pavilcek-Perry Well No. W-10

| Sat. No. | Depth, Feet | Effective Porosity Percent | Percent Saturation |       |       | Oil Content Hbl./A. Ft. | Feet of Core |           | Total Oil Content Hbl./Acres |
|----------|-------------|----------------------------|--------------------|-------|-------|-------------------------|--------------|-----------|------------------------------|
|          |             |                            | Oil                | Water | Total |                         | Ft.          | Cum. Ft.  |                              |
| F-1      | 648.0       | 19.0                       | 27                 | -     | -     | 398                     | 0.6          | 0.6       | 229                          |
| 1        | 648.2       | 15.1                       | 30                 | 66    | 96    | 352                     | 0.5          | 1.1       | 176                          |
| 2        | 649.1       | 15.9                       | 27                 | 66    | 93    | 333                     | 1.0          | 2.1       | 333                          |
| 3        | 650.1       | 20.1                       | 29                 | 62    | 91    | 452                     | 0.9          | 3.0       | 407                          |
| 4        | 651.1       | 16.5                       | 25                 | 69    | 94    | 320                     | 1.1          | 4.1       | 352                          |
| 5        | 652.1       | 13.5                       | 40                 | 54    | 94    | 419                     | 0.6          | 4.7       | 251                          |
| 6        | 653.1       | 20.3                       | 49                 | 31    | 80    | 777                     | 1.4          | 6.1       | 1,082                        |
| 7        | 654.1       | 20.5                       | 55                 | 31    | 86    | 874                     | 1.0          | 7.1       | 874                          |
| 8        | 655.1       | 20.6                       | 67                 | 28    | 95    | 1,071                   | 1.0          | 8.1       | 1,071                        |
| 9        | 656.1       | 20.2                       | 65                 | 31    | 96    | 1,020                   | 1.0          | 9.1       | 1,020                        |
| 10       | 657.1       | 23.1                       | 69                 | 26    | 95    | 1,238                   | 1.0          | 10.1      | 1,238                        |
| 11       | 658.1       | 21.0                       | 53                 | 35    | 88    | 863                     | 1.0          | 11.1      | 863                          |
| 12       | 659.1       | 21.5                       | 54                 | 40    | 94    | 900                     | 1.0          | 12.1      | 900                          |
| 13       | 660.1       | 18.8                       | 46                 | 34    | 80    | 671                     | 1.4          | 13.5      | 940                          |
| 14       | 661.1       | 10.3                       | 47                 | 33    | 80    | 376                     | 1.0          | 14.5      | 376                          |
|          |             |                            |                    |       |       |                         | Total-       | - - - - - | -10,112                      |

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**SUMMARY OF PERMEABILITY & SATURATION TESTS**

**TABLE III**

Company Schermerhorn Oil Corporation Lease Pavilcek-Perry Well No. W-10

| Depth Interval,<br>Feet | Feet of Core<br>Analyzed | Average<br>Permeability,<br>Millidarcys | Permeability<br>Capacity<br>Ft. x Md. |
|-------------------------|--------------------------|---|---------------------------------------|
| 647.5 - 650.5           | 3.0                      | 21.4                                    | 64.21                                 |
| 652.2 - 662.0           | 9.8                      | 70.3                                    | 689.40                                |
| 647.5 - 662.0           | 12.8                     | 58.9                                    | 753.61                                |

| Depth Interval,<br>Feet | Feet of Core<br>Analyzed | Average<br>Percent<br>Porosity | Average<br>Percent Oil<br>Saturation | Average<br>Percent Water<br>Saturation | Average<br>Oil Content<br>Bbl./A. Ft. | Total Oil<br>Content<br>Bbl./Acre |
|-------------------------|--------------------------|--------------------------------|--------------------------------------|--|---------------------------------------|-----------------------------------|
| 647.5 - 652.2           | 4.7                      | 16.9                           | 28.9                                 | 64.2                                   | 372                                   | 1,748                             |
| 652.2 - 662.0           | 9.8                      | 19.6                           | 55.4                                 | 32.2                                   | 854                                   | 8,364                             |
| 647.5 - 662.0           | 14.5                     | 18.7                           | 46.7                                 | 41.6                                   | 698                                   | 10,112                            |

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RESULTS OF LABORATORY FLOODING TESTS

TABLE IV

Company Schermerhorn Oil Corporation Lease Pavilcek-Perry Well No. W-10

| Sample No. | Depth, Feet | Effective Porosity Percent | Original Oil Saturation |              | Oil Recovery |              | Residual Saturation |         |              | Volume of Water Recovered cc* | Effective Permeability mD/cm <sup>2</sup> ** | Initial Fluid Production Pressure Lbs./Sq./In. |
|------------|-------------|----------------------------|-------------------------|--------------|--------------|--------------|---------------------|---------|--------------|-------------------------------|--|--|
|            |             |                            | %                       | Ekib./A. Ft. | %            | Ekib./A. Ft. | % Oil               | % Water | Ekib./A. Ft. |                               |  |  |
| 1          | 648.0       | 19.0                       | 27                      | 398          | 0            | 0            | 27                  | 69      | 398          | 33                            | 0.537  | 30   |
| 2          | 649.1       | 16.0                       | 24                      | 298          | 0            | 0            | 24                  | 75      | 298          | 2                             | 0.090  | 40   |
| 3          | 650.1       | 20.6                       | 31                      | 496          | 0            | 0            | 31                  | 68      | 496          | 50                            | 1.02   | 25   |
| 4          | 651.1       | 16.8                       | 24                      | 313          | 0            | 0            | 24                  | 72      | 313          | 16                            | 0.375  | 35   |
| 5          | 652.1       | 13.0                       | 37                      | 374          | 0            | 0            | 37                  | 53      | 374          | 0                             | Imp.   | 50+  |
| 6          | 653.1       | 20.8                       | 49                      | 792          | 25           | 404          | 24                  | 69      | 388          | 110                           | 6.56   | 5  |
| 7          | 654.1       | 20.7                       | 55                      | 883          | 29           | 466          | 26                  | 71      | 417          | 172                           | 10.39  | 5  |
| 8          | 655.1       | 20.8                       | 67                      | 1,081        | 41           | 661          | 26                  | 69      | 420          | 209                           | 9.06   | 5  |
| 9          | 656.1       | 20.5                       | 65                      | 1,034        | 44           | 700          | 21                  | 68      | 334          | 103                           | 7.62   | 5  |
| 10         | 657.1       | 22.8                       | 69                      | 1,221        | 44           | 779          | 25                  | 65      | 442          | 88                            | 6.81   | 5  |
| 11         | 658.1       | 21.3                       | 53                      | 875          | 27           | 446          | 26                  | 69      | 429          | 143                           | 8.46   | 5  |
| 12         | 659.1       | 21.8                       | 54                      | 914          | 25           | 423          | 29                  | 65      | 491          | 175                           | 6.04   | 5  |
| 13         | 660.1       | 18.3                       | 46                      | 653          | 20           | 284          | 26                  | 62      | 369          | 163                           | 5.96   | 5  |
| 14         | 661.1       | 10.8                       | 47                      | 394          | 14           | 117          | 33                  | 57      | 277          | 2                             | 0.170  | 35   |

Notes: cc—cubic centimeter.

\*—Volume of water recovered at the time of maximum oil recovery.

\*\*—Determined by passing water through sample which still contains residual oil.

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SUMMARY OF LABORATORY FLOODING TESTS

TABLE V

|   |                              |       |                |          |      |
|---|------------------------------|-------|----------------|----------|------|
| Company   | Schermerhorn Oil Corporation | Lease | Pavilcek-Perry | Well No. | W-10 |
| Depth Interval, Feet                              | 652.2 - 662.0                |       |                |          |      |
| Feet of Core Analyzed                             | 9.8                          |       |                |          |      |
| Average Percent Porosity                          | 19.7                         |       |                |          |      |
| Average Percent Original Oil Saturation           | 56.4                         |       |                |          |      |
| Average Percent Oil Recovery                      | 29.3                         |       |                |          |      |
| Average Percent Residual Oil Saturation           | 27.1                         |       |                |          |      |
| Average Percent Residual Water Saturation         | 66.0                         |       |                |          |      |
| Average Percent Total Residual Fluid Saturation   | 93.1                         |       |                |          |      |
| Average Original Oil Content, Bbls./A. Ft.        | 860.                         |       |                |          |      |
| Average Oil Recovery, Bbls./A. Ft.                | 465.                         |       |                |          |      |
| Average Residual Oil Content, Bbls./A. Ft.        | 395.                         |       |                |          |      |
| Total Original Oil Content, Bbls./Acre            | 8,425.                       |       |                |          |      |
| Total Oil Recovery, Bbls./Acre                    | 4,555.                       |       |                |          |      |
| Total Residual Oil Content, Bbls./Acre            | 3,870.                       |       |                |          |      |
| Average Effective Permeability, Millidarcys       | 6.74                         |       |                |          |      |
| Average Initial Fluid Production Pressure, p.s.i. | 8.3                          |       |                |          |      |

NOTE: Only those samples which recovered oil were used in calculating the above averages.