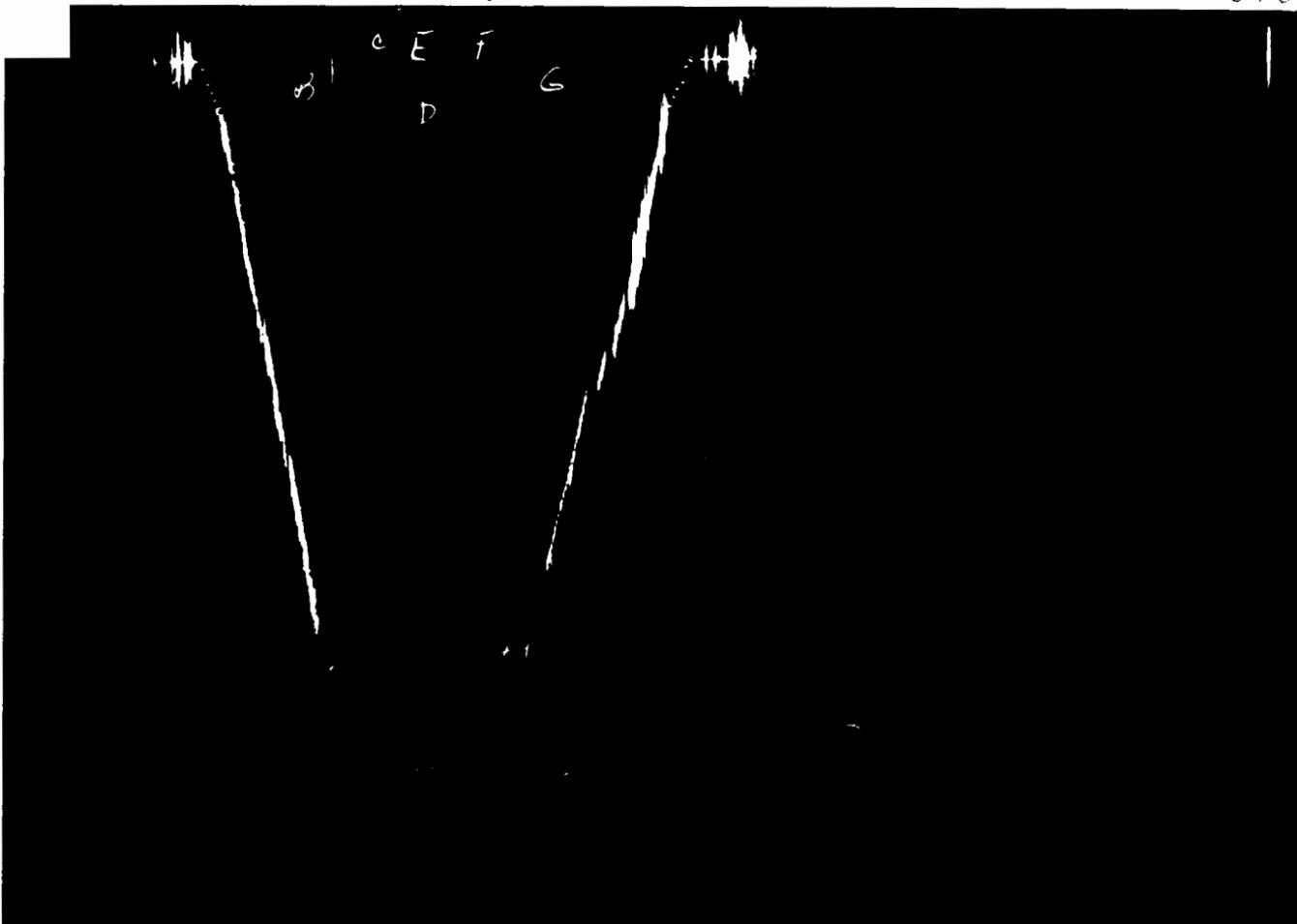


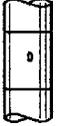
GAUGE NO: 228 DEPTH: 4054.0 BLANKED OFF: NQ HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	2063	2060.5			
B	INITIAL FIRST FLOW	10	8.8	30.0	30.0	F
C	FINAL FIRST FLOW	10	9.5			
C	INITIAL FIRST CLOSED-IN	10	9.5	30.0	30.0	C
D	FINAL FIRST CLOSED-IN	60	59.2			
E	INITIAL SECOND FLOW	20	22.1	30.0	30.0	F
F	FINAL SECOND FLOW	20	23.1			
F	INITIAL SECOND CLOSED-IN	20	23.1	30.0	30.0	C
G	FINAL SECOND CLOSED-IN	40	37.3			
H	FINAL HYDROSTATIC	2063	2059.3			



GAUGE NO: 7873 DEPTH: 4109.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		2092.5			
B	INITIAL FIRST FLOW		41.4			
C	FINAL FIRST FLOW		42.0	30.0	30.0	F
C	INITIAL FIRST CLOSED-IN		42.0			
D	FINAL FIRST CLOSED-IN		92.5	30.0	30.0	C
E	INITIAL SECOND FLOW		53.2			
F	FINAL SECOND FLOW		54.7	30.0	30.0	F
F	INITIAL SECOND CLOSED-IN		54.7			
G	FINAL SECOND CLOSED-IN		70.6	30.0	30.0	C
H	FINAL HYDROSTATIC		2085.9			

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	3711.0	
3		DRILL COLLARS.....	6.250	2.250	210.0	
50		IMPACT REVERSING SUB.....	5.000	2.250	1.0	3921.0
3		DRILL COLLARS.....	6.250	2.250	120.0	
12		DUAL CIP VALVE.....	5.000	0.870	6.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	4052.0
80		AP RUNNING CASE.....	5.000	2.250	4.0	4054.0
16		VR SAFETY JOINT.....	5.000	1.000	3.0	
70		OPEN HOLE PACKER.....	6.750	1.530	6.0	4064.0
70		OPEN HOLE PACKER.....	6.750	1.530	6.0	4070.0
20		FLUSH JOINT ANCHOR.....	5.000	2.370	35.0	
83		HT-500 TEMPERATURE CASE.....	5.000		1.0	4107.0
81		BLANKED-OFF RUNNING CASE.....	5.000		4.0	4109.0
TOTAL DEPTH					4112.0	

EQUIPMENT DATA

TEMPERATURE RECORDER CHART

APPROX 110°

098428

10° each circle

EQUATIONS FOR DST GAS WELL ANALYSIS

Indicated Flow Capacity $kh = \frac{1637 Q_g T}{m}$ md-ft

Average Effective Permeability $k = \frac{kh}{h}$ md

Skin Factor $S = 1.151 \left[\frac{m(P^*) - m(P_f)}{m} - \text{LOG} \left(\frac{k(t/60)}{\phi \mu c_f r_w^2} \right) + 3.23 \right]$ —

Damage Ratio $DR = \frac{m(P^*) - m(P_f)}{m(P^*) - m(P_f) - 0.87 mS}$ —

Indicated Flow Rate (Maximum) $AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_f)}$ MCFD

Indicated Flow Rate (Minimum) $AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_f)}}$ MCFD

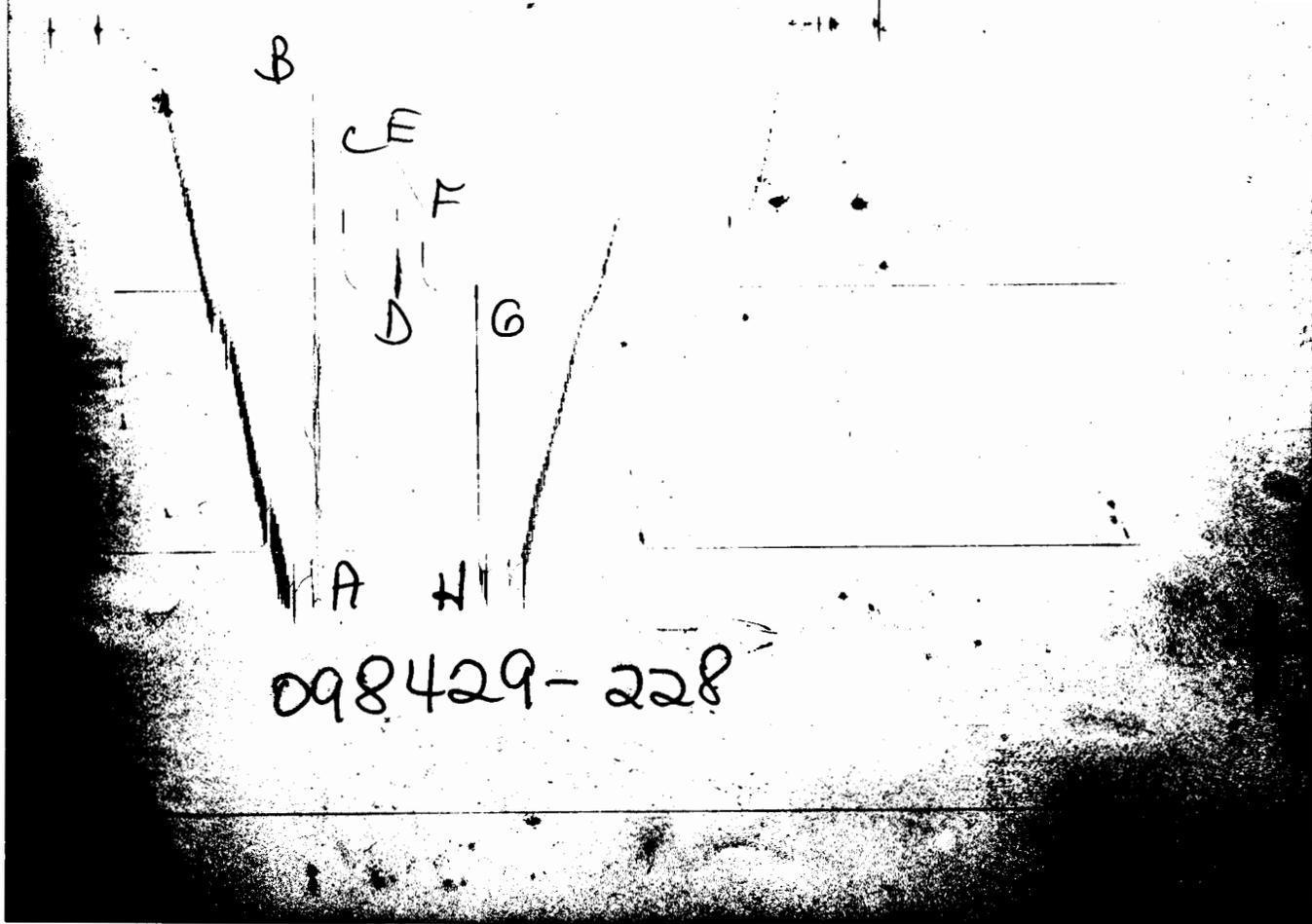
Approx. Radius of Investigation $r_i = 0.032 \sqrt{\frac{k(t/60)}{\phi \mu c_f}}$ ft



TICKET NO. 09842900
 28-MAY-85
 NESS CITY

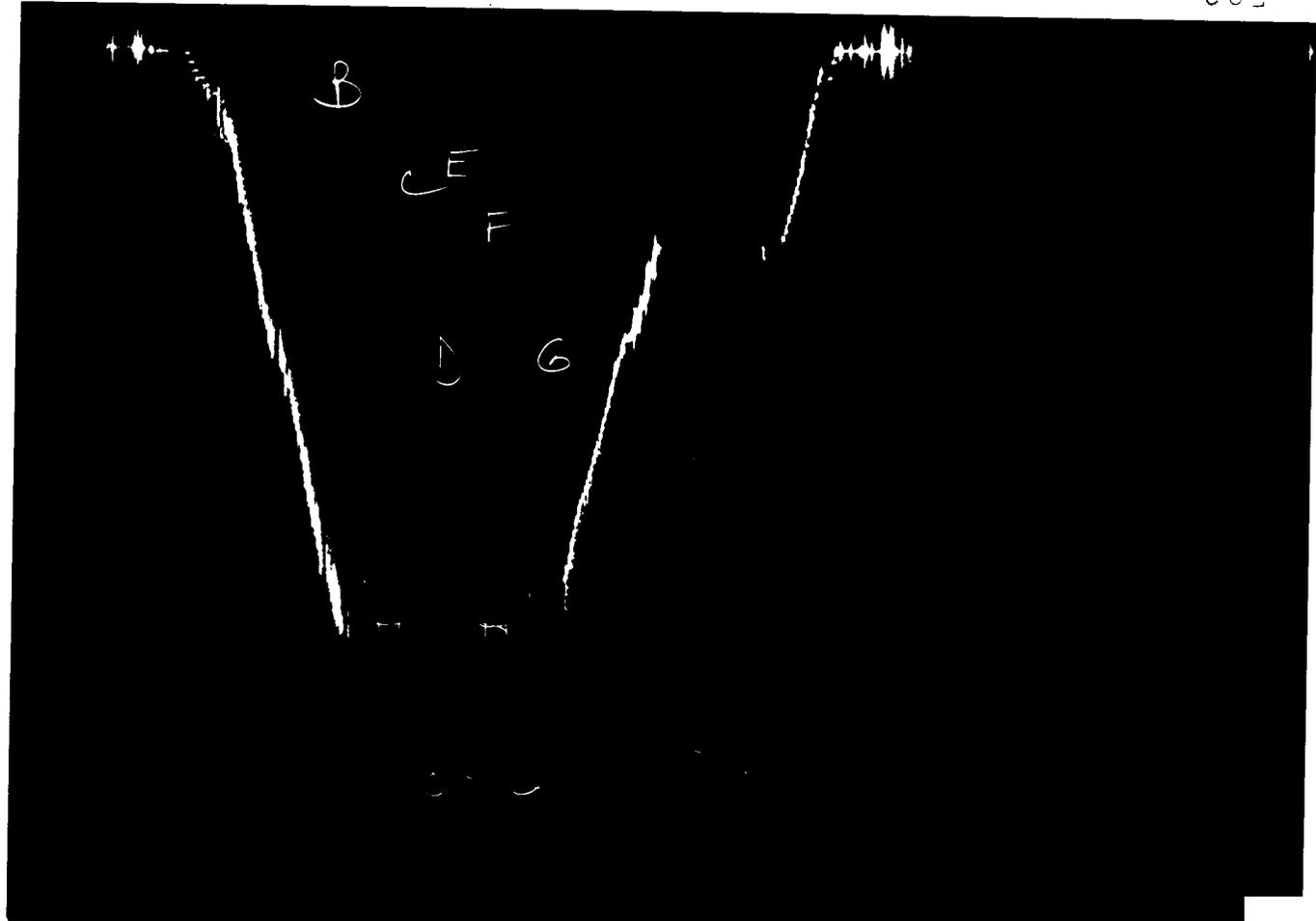
FORMATION TESTING SERVICE REPORT

LEASE NAME	BARNES	WELL NO.	1	TEST NO.	2	TEST INTERVAL	4096.0 - 4125.0	LEASE OWNER/COMPANY NAME	SUNBURST EXPLORATION COMPANY, INC
LEGAL LOCATION	26 - 16 SOUTH - 21 WEST	FIELD AREA		COUNTY	NESS	STATE	KANSAS		PK



GAUGE NO: 228 DEPTH: 4080.0 BLANKED OFF: NO HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	2083	2091.0			
B	INITIAL FIRST FLOW	101	98.3			
C	FINAL FIRST FLOW	485	483.9	15.0	16.5	F
C	INITIAL FIRST CLOSED-IN	485	483.9			
D	FINAL FIRST CLOSED-IN	1025	1028.9	30.0	29.9	C
E	INITIAL SECOND FLOW	506	514.8			
F	FINAL SECOND FLOW	665	684.5	15.0	14.1	F
F	INITIAL SECOND CLOSED-IN	665	684.5			
G	FINAL SECOND CLOSED-IN	1025	1029.0	30.0	29.5	C
H	FINAL HYDROSTATIC	2063	2071.6			



GAUGE NO: 7873 DEPTH: 4122.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		2117.0			
B	INITIAL FIRST FLOW		134.4			
C	FINAL FIRST FLOW		517.9	15.0	16.5	F
C	INITIAL FIRST CLOSED-IN		517.9			
D	FINAL FIRST CLOSED-IN		1059.2	30.0	29.9	C
E	INITIAL SECOND FLOW		544.6			
F	FINAL SECOND FLOW		716.0	15.0	14.1	F
F	INITIAL SECOND CLOSED-IN		716.0			
G	FINAL SECOND CLOSED-IN		1058.0	30.0	29.5	C
H	FINAL HYDROSTATIC		2094.6			

EQUIPMENT & HOLE DATA

FORMATION TESTED: CHEROKEE
 NET PAY (ft): 7.0
 GROSS TESTED FOOTAGE: 29.0
 ALL DEPTHS MEASURED FROM: KB
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.875
 ELEVATION (ft): 2220.0 KELLY BUSHING
 TOTAL DEPTH (ft): 4125.0
 PACKER DEPTH(S) (ft): 4090, 4096
 FINAL SURFACE CHOKE (in): _____
 BOTTOM HOLE CHOKE (in): 0.750
 MUD WEIGHT (lb/gal): 9.70
 MUD VISCOSITY (sec): 45
 ESTIMATED HOLE TEMP. (°F): _____
 ACTUAL HOLE TEMP. (°F): 120 @ 4120.0 ft

TICKET NUMBER: 09842900
 DATE: 5-22-85 TEST NO: 2
 TYPE DST: OPEN HOLE
 HALLIBURTON CAMP: _____
NESS CITY
 TESTER: B. CROSSWHITE
S. NUTTING
 WITNESS: B. MATHEISON
 DRILLING CONTRACTOR: _____
WHITE & ELLIS #2

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES	
_____	_____ @ _____ °F	_____	ppm
_____	_____ @ _____ °F	_____	ppm
_____	_____ @ _____ °F	_____	ppm
_____	_____ @ _____ °F	_____	ppm
_____	_____ @ _____ °F	_____	ppm
_____	_____ @ _____ °F	_____	ppm

SAMPLER DATA

Pstg AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ @ _____ °F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____

RECOVERED:

1488 FEET OF SALTWATER - NO SHOW OF OIL

MEASURED FROM TESTER VALVE

REMARKS:

TICKET NO: 09842900
 CLOCK NO: 27315 HOUR: 12



GAUGE NO: 228
 DEPTH: 4080.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B	1	0.0	98.3		
	2	3.0	205.0	106.8	
	3	6.0	276.3	71.3	
	4	9.0	342.5	66.1	
	5	12.0	405.2	62.7	
	6	15.0	461.5	56.3	
C	7	16.5	483.9	22.4	
FIRST CLOSED-IN					
C	1	0.0	483.9		
	2	2.0	957.6	473.8	1.8 0.969
	3	4.0	978.2	494.3	3.2 0.712
	4	6.0	991.7	507.8	4.4 0.575
	5	8.0	1000.4	516.5	5.4 0.486
	6	10.0	1006.3	522.4	6.2 0.423
	7	12.0	1011.6	527.8	7.0 0.375
	8	14.0	1014.9	531.1	7.6 0.338
	9	16.0	1018.3	534.5	8.1 0.308
	10	18.0	1020.4	536.6	8.6 0.282
	11	20.0	1022.7	538.9	9.0 0.261
	12	22.0	1024.5	540.7	9.4 0.243
	13	24.0	1025.9	542.0	9.8 0.227
	14	26.0	1026.8	542.9	10.1 0.213
	15	28.0	1027.9	544.0	10.4 0.201
D	16	29.9	1028.9	545.0	10.6 0.191
SECOND FLOW					
E	1	0.0	514.8		
	2	2.0	525.1	10.3	
	3	4.0	554.0	28.8	
	4	6.0	584.6	30.6	
	5	8.0	610.5	25.9	
	6	10.0	638.0	27.4	
	7	12.0	661.8	23.8	
F	8	14.1	684.5	22.6	
SECOND CLOSED-IN					
F	1	0.0	684.5		
	2	2.0	980.2	295.7	1.9 1.209
	3	4.0	993.5	309.0	3.5 0.935
	4	6.0	1002.3	317.9	5.0 0.784
	5	8.0	1007.1	322.7	6.3 0.684
	6	10.0	1012.6	328.1	7.5 0.608
	7	12.0	1015.6	331.1	8.6 0.549
	8	14.0	1018.9	334.5	9.6 0.503
	9	16.0	1020.9	336.5	10.5 0.464

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
	10	18.0	1023.1	338.7	11.3 0.431
	11	20.0	1024.2	339.8	12.1 0.402
	12	22.0	1025.2	340.8	12.8 0.378
	13	24.0	1026.2	341.8	13.4 0.357
	14	26.0	1027.8	343.3	14.1 0.337
	15	28.0	1028.5	344.0	14.6 0.320
G	16	29.5	1029.0	344.5	15.0 0.309

REMARKS:

TICKET NO: 09842900
 CLOCK NO: 14248 HOUR: 12



GAUGE NO: 7873
 DEPTH: 4122.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B	1	0.0	134.4		
	2	3.0	238.4	103.9	
	3	6.0	314.1	75.8	
	4	9.0	378.7	64.6	
	5	12.0	439.9	61.2	
	6	15.0	494.7	54.8	
C	7	16.5	517.9	23.2	
FIRST CLOSED-IN					
C	1	0.0	517.9		
	2	2.0	991.5	473.6	1.8 0.964
	3	4.0	1011.6	493.7	3.2 0.708
	4	6.0	1022.8	504.9	4.4 0.573
	5	8.0	1031.3	513.4	5.4 0.485
	6	10.0	1037.6	519.7	6.2 0.422
	7	12.0	1041.5	523.6	6.9 0.375
	8	14.0	1045.5	527.6	7.6 0.338
	9	16.0	1048.7	530.8	8.1 0.307
	10	18.0	1050.5	532.6	8.6 0.282
	11	20.0	1052.0	534.1	9.0 0.261
	12	22.0	1054.1	536.2	9.4 0.243
	13	24.0	1055.6	537.7	9.8 0.227
	14	26.0	1057.6	539.7	10.1 0.213
	15	28.0	1058.6	540.7	10.4 0.201
D	16	29.9	1059.2	541.3	10.6 0.191
SECOND FLOW					
E	1	0.0	544.6		
	2	2.0	557.1	12.6	
	3	4.0	588.5	31.4	
	4	6.0	617.0	28.5	
	5	8.0	644.5	27.4	
	6	10.0	670.3	25.8	
	7	12.0	692.5	22.2	
F	8	14.1	716.0	23.5	
SECOND CLOSED-IN					
F	1	0.0	716.0		
	2	2.0	1012.1	296.1	1.9 1.216
	3	4.0	1025.8	309.7	3.5 0.937
	4	6.0	1034.0	318.0	5.0 0.787
	5	8.0	1040.0	324.0	6.4 0.682
	6	10.0	1043.1	327.1	7.5 0.609
	7	12.0	1046.6	330.6	8.6 0.550
	8	14.0	1049.1	333.1	9.6 0.503
	9	16.0	1050.7	334.6	10.5 0.463

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
	10	18.0	1052.7	336.6	11.3 0.432
	11	20.0	1054.1	338.0	12.1 0.403
	12	22.0	1055.2	339.1	12.8 0.378
	13	24.0	1056.2	340.1	13.4 0.356
	14	26.0	1057.0	340.9	14.0 0.338
	15	28.0	1057.6	341.5	14.6 0.320
G	16	29.5	1058.0	341.9	15.0 0.309

REMARKS:

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	3736.0	
3		DRILL COLLARS.....	6.250	2.250	210.0	
50		IMPACT REVERSING SUB.....	5.000	2.750	1.0	3946.0
3		DRILL COLLARS.....	6.250	2.250	120.0	
5		CROSSOVER.....	5.000	2.750	1.0	
12		DUAL CIP VALVE.....	5.000	0.870	6.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	4078.0
80		AP RUNNING CASE.....	5.000	2.250	4.0	4080.0
16		VR SAFETY JOINT.....	5.000	1.000	3.0	
70		OPEN HOLE PACKER.....	6.750	1.530	6.0	4090.0
70		OPEN HOLE PACKER.....	6.750	1.530	6.0	4096.0
20		FLUSH JOINT ANCHOR.....	5.000	2.370	22.0	
83		HT-500 TEMPERATURE CASE.....	5.000		1.0	4120.0
81		BLANKED-OFF RUNNING CASE.....	5.000		4.0	4122.0
TOTAL DEPTH					4125.0	

EQUIPMENT DATA

TEMPERATURE RECORDER CHART

120°

098429

10° each circle

FORMULAS FOR GAS WELL ANALYSIS

Indicated Flow Capacity $kh = \frac{1637 Q_g T}{m}$ md-ft

Average Effective Permeability $k = \frac{kh}{h}$ md

Skin Factor $S = 1.151 \left[\frac{m(P^*) - m(P_f)}{m} - \text{LOG} \left(\frac{k(t/60)}{\phi \mu c_t r_w^2} \right) + 3.23 \right]$ —

Damage Ratio $DR = \frac{m(P^*) - m(P_f)}{m(P^*) - m(P_f) - 0.87 mS}$ —

Indicated Flow Rate (Maximum) $AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_f)}$ MCFD

Indicated Flow Rate (Minimum) $AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_f)}}$ MCFD

Approx. Radius of Investigation $r_i = 0.032 \sqrt{\frac{k(t/60)}{\phi \mu c_t}}$ ft