

30-19-21

TORP

Memo

| | | | | | |
|-------------------|---------------------|---------|-----------------|------------|---|
| Post-It® Fax Note | 7671 | Date | 4/1/97 | # of pages | 1 |
| To | Tim Carr | From | Rodney Reynolds | | |
| Co./Dept | KGS | Co. | TORP | | |
| Phone # | cc: Paul G + Saibal | Phone # | 4-4491 | | |
| Fax # | 4-5317 | Fax # | 4-4967 | | |

To: Paul Willhite
 Don Green
 Shapour Vossoughi

From: Rodney Reynolds

CC: Tim Carr
 Paul Gerlach
 Saibal Bhattacharya

Date: April 1, 1997

Re: Wellbore flowing pressures in the Schaben Field

I am in receipt of a copy of the recent fluid level data acquired by Ritchie Exploration on the wells they operate in the Schaben Field. From my experience as a production engineer, I am familiar with how this data is acquired, the instruments used to acquire this data, the accuracy limitations associated with these instruments, and how to interpret the data. My evaluation of the data indicates that of the 23 wells on which data was received, 15 of the wells are operating in a pumped off condition. This is the general practice of the oil industry, especially when dealing with marginal production. However, occasionally situations dictate that backpressure be held against the formation in wells that have high productivity, produce excessive amounts of water, to assist in reducing lifting costs, or in some instances may assist in maintaining some percentage in oil cut. I also spoke with Danny Biggs (production superintendent) and Jack Gurley (petroleum engineer) for Pickrell Drilling Company, concerning fluid levels on their wells. They indicated that they have not recently shot fluid levels, but in general they try to pump the wells off, however they have a few large water producers they cannot pump off. They said its time to shoot fluid levels and they will supply a copy of the results to me.

I have also compared the recently acquired fluid level data to the fluid level information acquired from the historic information contained in the well files, on which TORP based the model and simulation. The recent data correlates with the data we used, with 2 exceptions. The recent data indicates the Moore B-6 is carrying approx. 200' fluid above the perforations and the well files indicated it to be pumped off and the Moore D-4 which Ritchie field personnel indicated to me had "a lot of fluid in the hole" and the recent data indicates it is pumped off.

15-135

30-19-21
25-19-22

| Name | Interval | | Vis. | Oil gr. | B= FVF | K | Phi | C | Skin | Final pr. | Temp | Water Sp gr. | Chlorides | Sulfates | Calcium | Magnesium | Kh/Vis. |
|--------------|-----------|------|----------|---------|--------|-------|------|------------------|-------|-----------|------|--------------|-----------|----------|---------|-----------|---------|
| | To | From | cp | | | md | | vol/vol/psi*10^6 | | | F | | | | | | |
| Moore B5 | 4395 | 4405 | 3 | | 1.2 | | 0.15 | 10 | 6.87 | 1375 | 118 | | | | | | |
| 15-135-30062 | 4385 | 4395 | 3 | | 1.2 | 30 | 0.15 | 10 | 5.41 | 1382 | 118 | | | | | | |
| Moore B1 | 4430 | 4440 | | | | | | | | | | 1.029 | 25800 | 2500 | 2140 | 300 | |
| 15-135-29344 | 4313 | 4325 | | 39 @ 60 | | | | | | | 119 | | | | | | |
| | 4380 | 4396 | | | | | | | | | 116 | | | | | | |
| | 4330 | 4396 | | | | | | | | | 116 | | | | | | |
| | 4396 | 4410 | 2.5 | 42.6 | 1.2 | 115 | 0.15 | 12 | -3.96 | 665 | 120 | | | | | | |
| | 4410 | 4420 | 2.5 | | 1.2 | 13.65 | 0.15 | 10 | 2.02 | 1397 | 119 | | | | | | |
| | 4420 | 4430 | 2.5 | | 1.2 | 87 | 0.15 | 12 | -2.91 | 1413 | 120 | | | | | | |
| | 4430 | 4440 | | | | | | | | | 118 | | | | | | |
| Moore B4 | 4402 | 4412 | 3 | | 1.2 | 11.45 | 0.15 | 10 | 0.353 | 1273 | 118 | | | | | | |
| 15-135 | 4412 | 4422 | 3 | | 1.2 | 216 | 0.15 | 10 | 20.8 | 1377 | 120 | | | | | | |
| 30042 | 4393 | 4402 | | | | | | | | | 118 | | | | | | |
| Moore B6 | 4415 | 4427 | | | | | | | | | 112 | | | | | | |
| 15-135 | 4427 | 4437 | | | | | | | | | 112 | | | | | | |
| 19004 | 4437 | 4447 | | 39 @ 60 | | | | | | | 118 | | | | | | |
| Moore C2 | Prod. Int | | | | 38 | | | | | | | | | | | | |
| 19013 | 4304 | 4319 | | | | | | | | | 110 | | | | | | |
| Moore C3 | DST 7 | | | | | | | | | | | | | | | | 21.75 |
| 21024 | DST 6 | | | | | 3.45 | | | | | | | | | | | 9.19 |
| Moore D1 | 4392 | | 28 @ 77F | | | | | | | | | | 25000 | | | | |
| 30047 | 4366 | 4383 | 3 | | 1.2 | 1.17 | 0.15 | 10 | 0.727 | 1405 | 100 | | | | | | |
| | 4383 | 4398 | 3 | 40.5-60 | 1.2 | 28 | 0.17 | 10 | 2.49 | 1377 | 100 | | | | | | |
| | 4398 | 4410 | 3 | | 1.2 | 13.8 | 0.13 | 10 | 3.195 | 1407 | 100 | | | | | | |
| Moore D2 | 4365 | 4386 | 2.5 | | 1.2 | | | 10 | 0.5 | 1340 | 116 | | | | | | |
| 30023 | 4386 | 4393 | | | | | | | | | 118 | | | | | | |
| Moore D3 | 4400 | 4410 | | | | | | | | | 119 | | | | | | |
| 30030 | 4381 | 4388 | | | | | | | | | 118 | | | | | | |
| | 4388 | 4400 | 3 | | 1.15 | 21.1 | 0.15 | 10 | 8.08 | 1383 | 119 | | | | | | |
| | 4400 | 4410 | 3 | | 1.15 | 100 | 0.15 | 10 | 11.65 | 1372 | 119 | | | | | | |
| Moore D4 | 4408 | 4418 | | | | | | | | | 112 | | | | | | |
| | 4418 | 4428 | | | 36 | | | | | | 112 | | | | | | |
| | 4428 | 4436 | | | 38 | | | | | | 112 | | | | | | |
| Foos A2 | 4409 | 4414 | | 36 @ 60 | | | | | | | 115 | 1.035 | 29200 | 3250 | 2000 | 250 | |
| 30025 | 4401 | 4409 | | | | | | | | | 115 | | | | | | |
| Humburg A2 | | | | | | | | | | | | 1.04 | 29201 | 5000 | 1222 | 793 | |
| 19015 | 4391 | 4401 | 3 | | 1.2 | 17.3 | 0.15 | 10 | 0.695 | 1370 | 110 | | | | | | |
| | 4401 | 4411 | 3 | | 1.2 | 20.4 | 0.15 | 10 | | 1275 | 112 | | | | | | |
| | 4295 | 4310 | | | | | | | | | 110 | | | | | | |
| Borger A1 | 4405 | 4422 | | 38 @ 60 | | | | | | | 115 | | | | | | |
| 19012 | 4308 | 4323 | | | | | | | | | 115 | | | | | | |
| Borger A2 | 4398 | 4410 | 3 | | 1.2 | | 0.15 | 10 | 0.435 | 1389 | | | | | | | |
| 30004 | 4389 | 4398 | 3 | | 1.2 | 9.6 | 0.15 | 10 | 1.7 | 1456 | 100 | | | | | | |
| | 4369 | 4378 | | | | | | | | | 100 | | | | | | |

Total diss solids

= 30740

25000

↓
Avg.
1.035

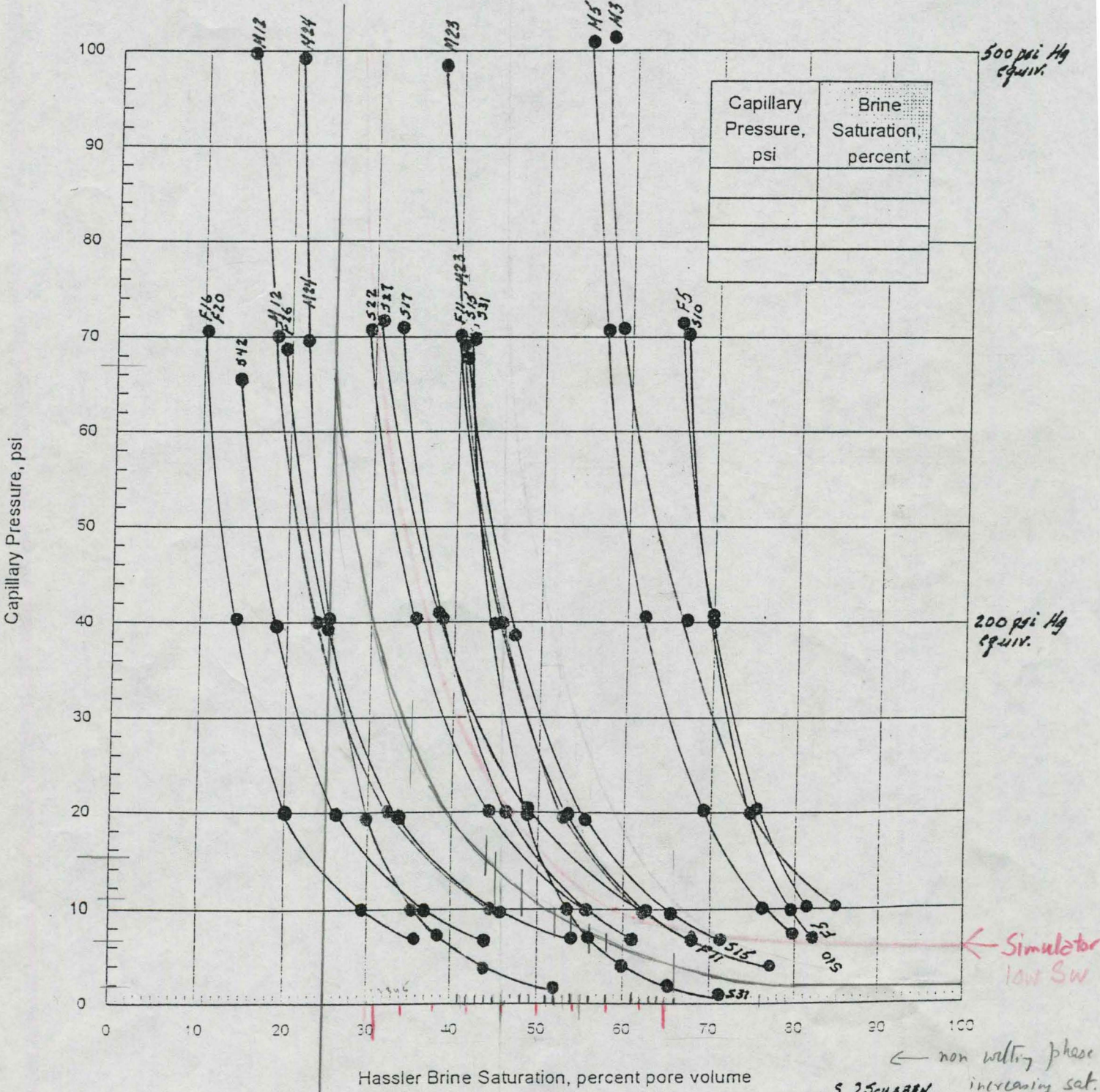
CENTRIFUGE CAPILLARY PRESSURE

Air Displacing Brine System
Ambient Conditions

Well: Ritchie
Field: Schaben
Location: Ness County, Kansas

Sample ID:
Depth, ft.:
Permeability to Air, md:
Porosity, percent:

$P_c(10) = 0.3608 P_c(100)$



← non wetting phase increasing sat.
S 2 Schaben
F 1 F003
M 4 M0026

Schaben Field

| | Cap. P | Sample ID | depth | K air | core PHI helium deter. | MRIL core PHI saturation deter. |
|---------|--------|-----------|------------|-------|------------------------------|--|
| Moore 4 | 2 | 4394.8 | 0.036 | 7.4 | 7.02 | |
| | 3 | 4399.4 | 0.144 | 12.6 | 13.97 | |
| | 5 | 4411.2 | 1.38 | 16.5 | 15.12 | |
| | 12 | 4423.5 | 8.54 | 19.8 | 21.32 | |
| | 23 | 4437.1 | 0.777 | 10.8 | 9.74 | |
| | 24 | 4437.8 | 149 | 14.7 | 11.56 | |
| Foos 1 | 5 | 4398 | 0.21 | 6 | 7.09 | |
| | 11 | 4405.7 | 13 | 18.6 | 18.65 | |
| | 16 | 4410.8 | 43 | 23.5 | 22.69 | |
| | 20 | 4416.4 | 64 | 24.5 | 23.47 | |
| | 26 | 4427.6 | 14 | 18.4 | 18.49 | |
| Lyle 2 | 10 | 4398.8 | 3.7 | 14.5 | 13.53 | |
| | 15 | 4403.8 | 7.5 | 14 | 16.25 | |
| | 17 | 4405.8 | 48 | 16.9 | 16.38 | |
| | 22 | 4411.8 | 25 | 18.4 | 18.72 | |
| | 27 | 4417.2 | 2.8 | 16.8 | 17.23 | |
| | 31 | 4421.7 | 1030(frac) | 12.9 | 12.82 | |
| | 42 | 4434.8 | 33 | 22.7 | 22.04 | |

Well: Ritchie 2 Lyle Schaben "P"

100 % Saturated Sample Data

| Sample ID | 10 | 15 | 17 | 22 | 27 | 31 | 42 |
|--------------------------------------|--------------|-------|-------|-------|-------|-------|-------|
| Regularized Fluid Filled Porosity, % | 14.61 | 16.17 | 16.49 | 18.82 | 17.27 | 12.91 | 21.95 |
| MRIL Fluid Filled Porosity, % | <u>13.53</u> | 16.25 | 16.38 | 18.72 | 17.23 | 12.82 | 22.04 |
| "Free" Water Saturation, % | 44.1 | 59.8 | 67.3 | 77.1 | 79.2 | 42.7 | 80.1 |
| "Free" Average T ₂ , ms | 220. | 180. | 237. | 113.4 | 80.16 | 717. | 114.3 |
| "Bound" Water Saturation, % | 55.9 | 40.2 | 32.7 | 22.9 | 20.8 | 57.3 | 19.9 |
| "Bound" Average T ₂ , ms | 15.33 | 17.35 | 21.24 | 13.98 | 11.72 | 25. | 14.43 |
| Calculated Permeability, md | 2.10 | 15.4 | 30.4 | 139. | 128. | 1.5 | 382. |

Desaturated Sample Data (Original) (70 psi)

| | | | | | | | |
|--------------------------------------|--------------|-------|-------|-------|-------|--------|-------|
| Regularized Fluid Filled Porosity, % | 10.54 | 8.22 | 6.77 | 7.44 | 7.41 | 5.04 | 6.23 |
| MRIL Fluid Filled Porosity, % | <u>10.38</u> | 8.41 | 6.93 | 7.60 | 6.68 | 4.98 | 6.39 |
| "Free" Water Saturation, % | 46.70 | 70.00 | 66.40 | 60.30 | 69.20 | 26.30 | 58.50 |
| "Free" Average T ₂ , ms | 58.32 | 37.81 | 49.02 | 51.04 | 39.80 | 222.67 | 29.77 |
| "Bound" Water Saturation, % | 53.30 | 30.00 | 33.60 | 39.70 | 30.80 | 73.70 | 41.50 |
| "Bound" Average T ₂ , ms | 7.23 | 7.41 | 8.30 | 8.11 | 7.58 | 12.46 | 7.05 |

Desaturated Sample Data (100 psi)

| | | | | | | | |
|--------------------------------------|-------|-------|-------|-------|-------|--------|-------|
| Regularized Fluid Filled Porosity, % | 10.62 | 8.89 | 6.27 | 6.51 | 7.40 | 4.68 | 4.73 |
| MRIL Fluid Filled Porosity, % | 10.27 | 8.99 | 6.33 | 6.52 | 7.49 | 4.19 | 4.71 |
| "Free" Water Saturation, % | 44.11 | 66.18 | 61.93 | 53.68 | 62.08 | 28.16 | 33.76 |
| "Free" Average T ₂ , ms | 63.98 | 39.88 | 41.47 | 47.62 | 41.96 | 606.17 | 31.27 |
| "Bound" Water Saturation, % | 55.89 | 33.82 | 38.07 | 46.32 | 37.92 | 71.84 | 66.24 |
| "Bound" Average T ₂ , ms | 7.41 | 7.61 | 7.71 | 7.29 | 7.31 | 14.31 | 6.27 |

Desaturated Sample Data (1000 psi)

| | | | | | | | |
|--------------------------------------|-------------|-------|-------|-------|-------|--------|---------|
| Regularized Fluid Filled Porosity, % | 6.75 | 5.46 | 3.93 | 2.68 | 3.26 | 2.76 | 2.58 |
| MRIL Fluid Filled Porosity, % | <u>6.52</u> | 5.41 | 3.89 | 2.59 | 3.18 | 2.23 | 2.03 |
| "Free" Water Saturation, % | 42.33 | 61.92 | 51.41 | 34.36 | 21.63 | 35.87 | 1.48 |
| "Free" Average T ₂ , ms | 40.08 | 32.40 | 31.06 | 31.41 | 34.18 | 449.13 | 6253.08 |
| "Bound" Water Saturation, % | 57.67 | 38.08 | 48.59 | 65.64 | 78.37 | 64.13 | 98.52 |
| "Bound" Average T ₂ , ms | 5.31 | 5.94 | 6.06 | 4.93 | 5.51 | 10.06 | 8.59 |

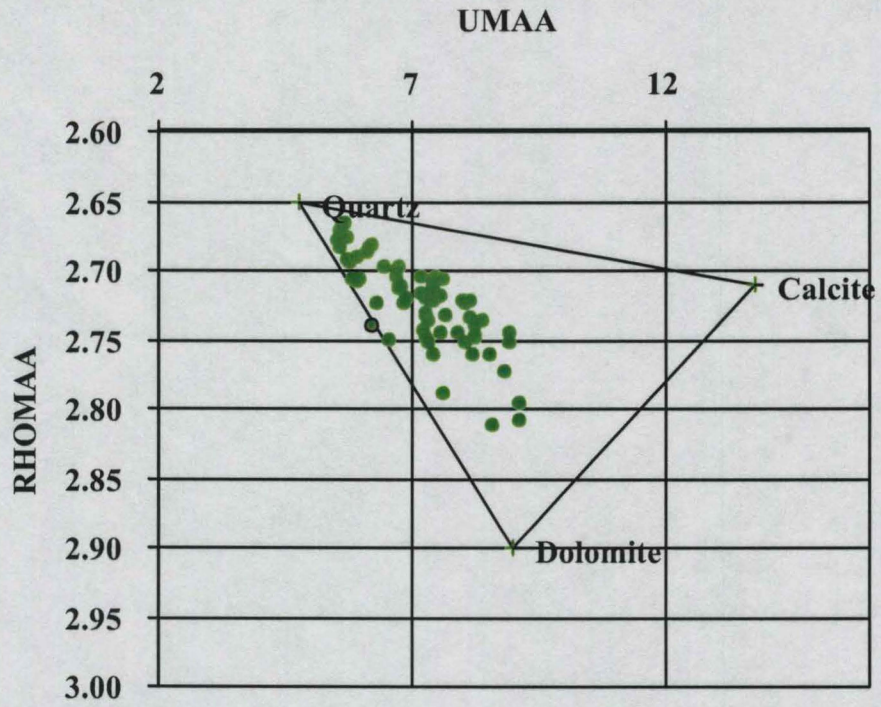


Figure --: RHOMAA-UMAA plot constructed on log data from Lyle Schaben 2P well to analyze lithologic composition of the reservoir rock.

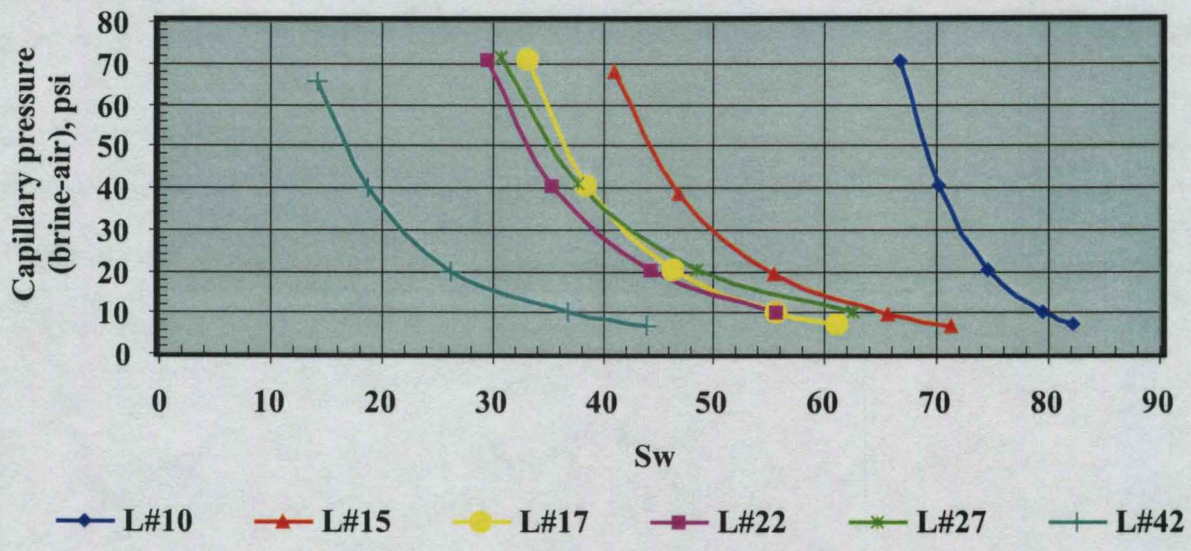
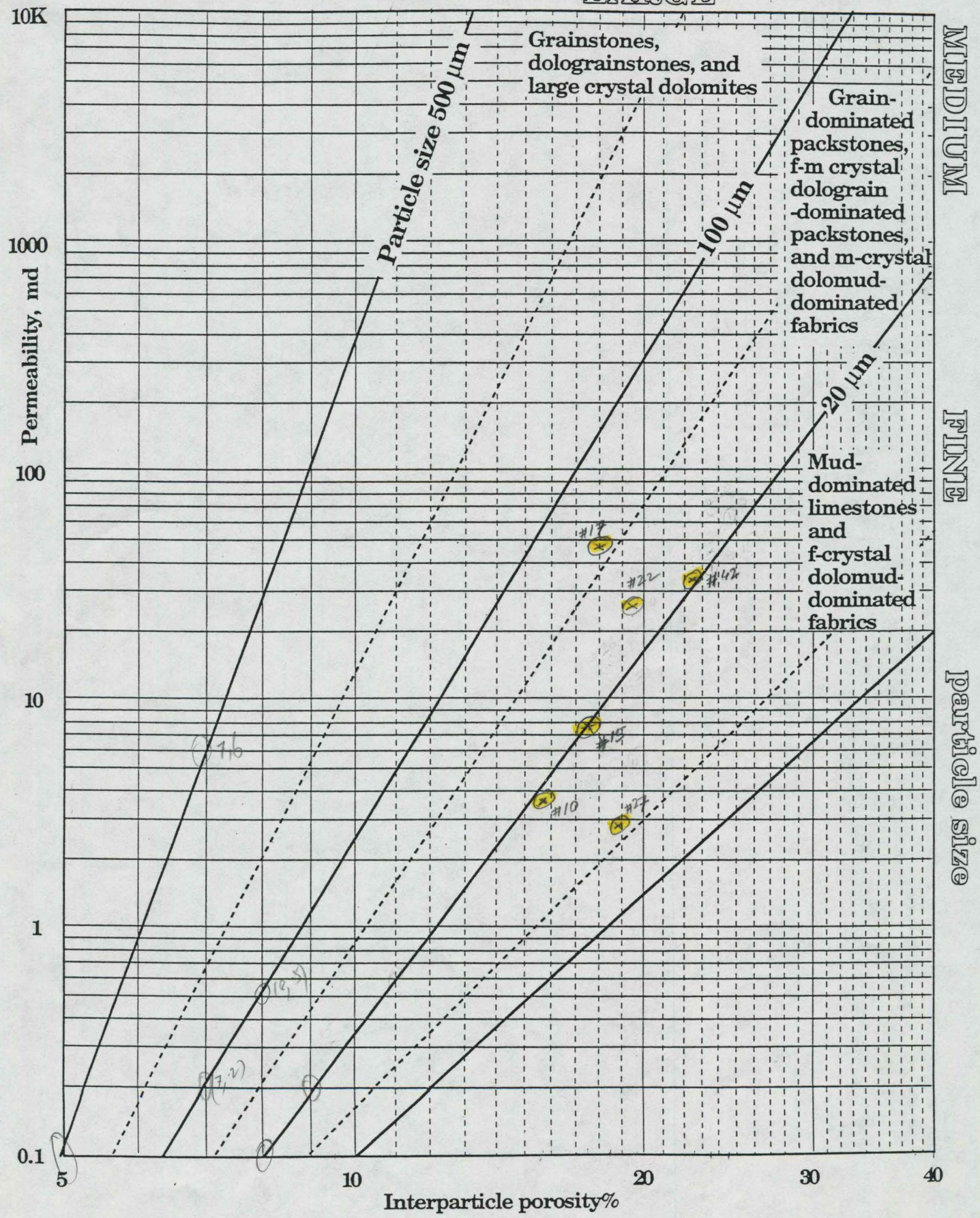


Figure --: Capillary pressure curves measured at (or near) 70 psi (brine-air) on Mississippiian plugs taken from Lyle Schaben 2P.

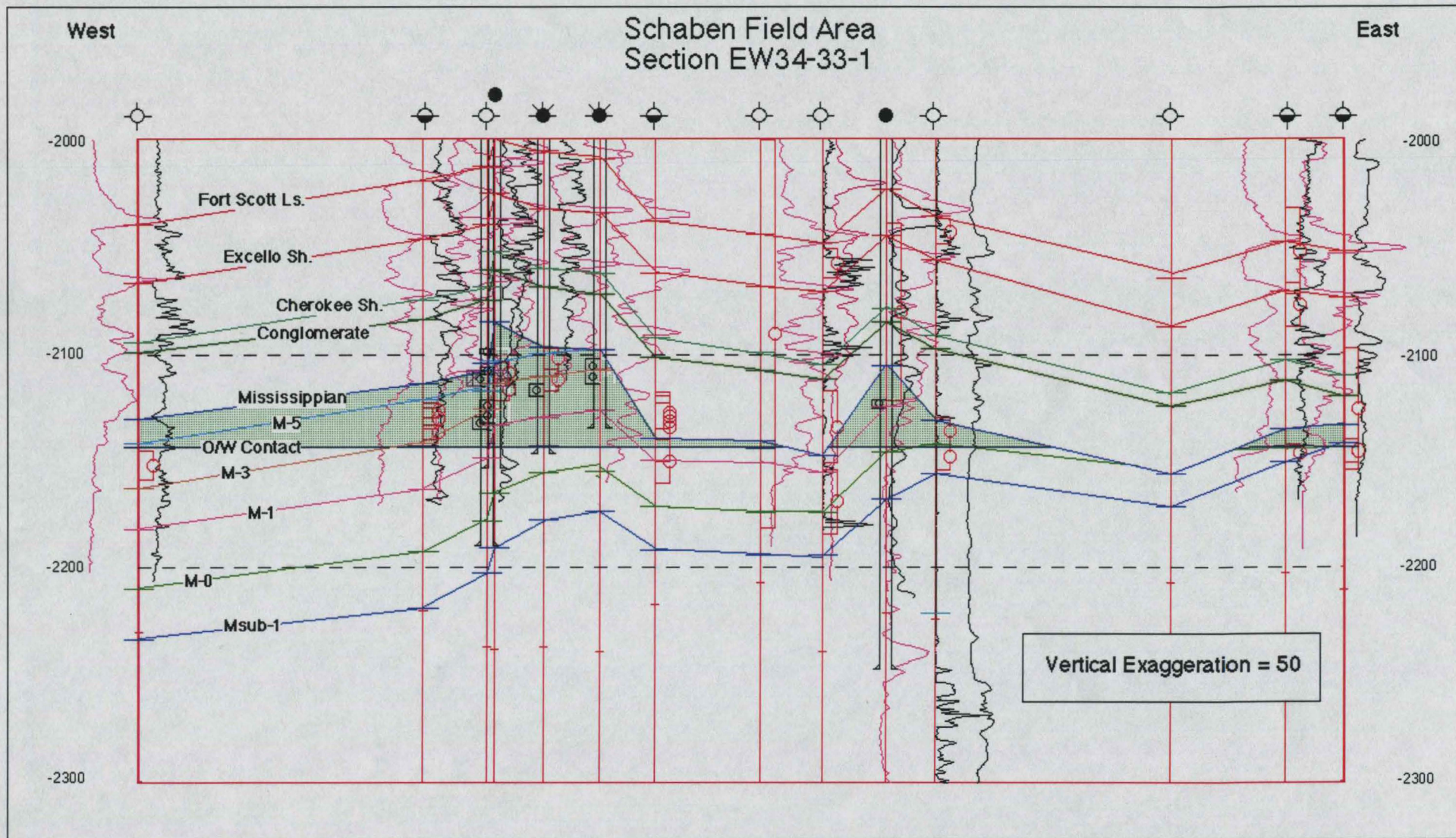
Dyke - Schaben

LARGE



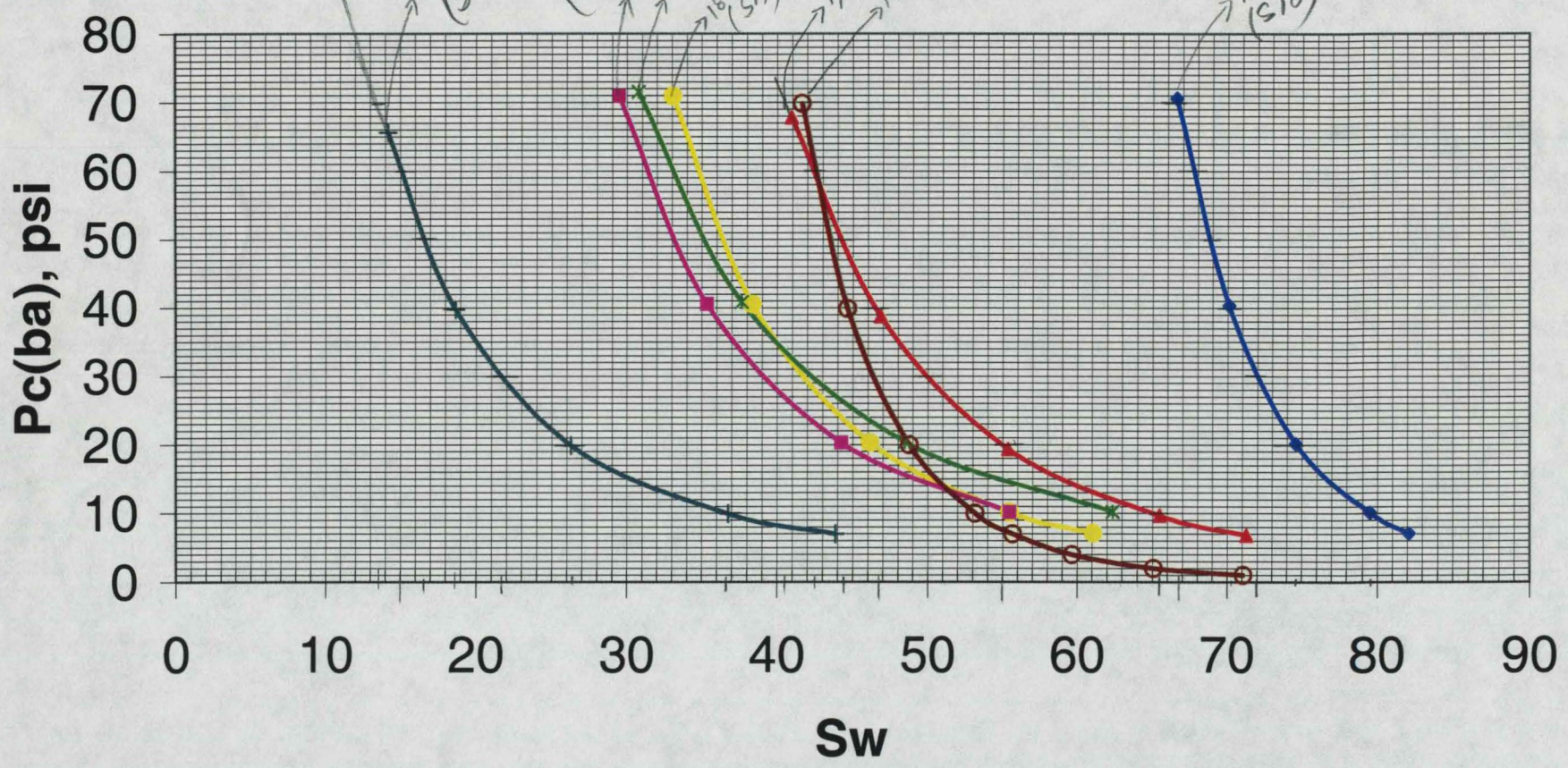
Lucia (1983, 1995) non-vuggy carbonate classification of porosity-permeability fields by particle size class. Sloping dashed lines are RMA fits for each class.

Through Lyle Schaben 2P



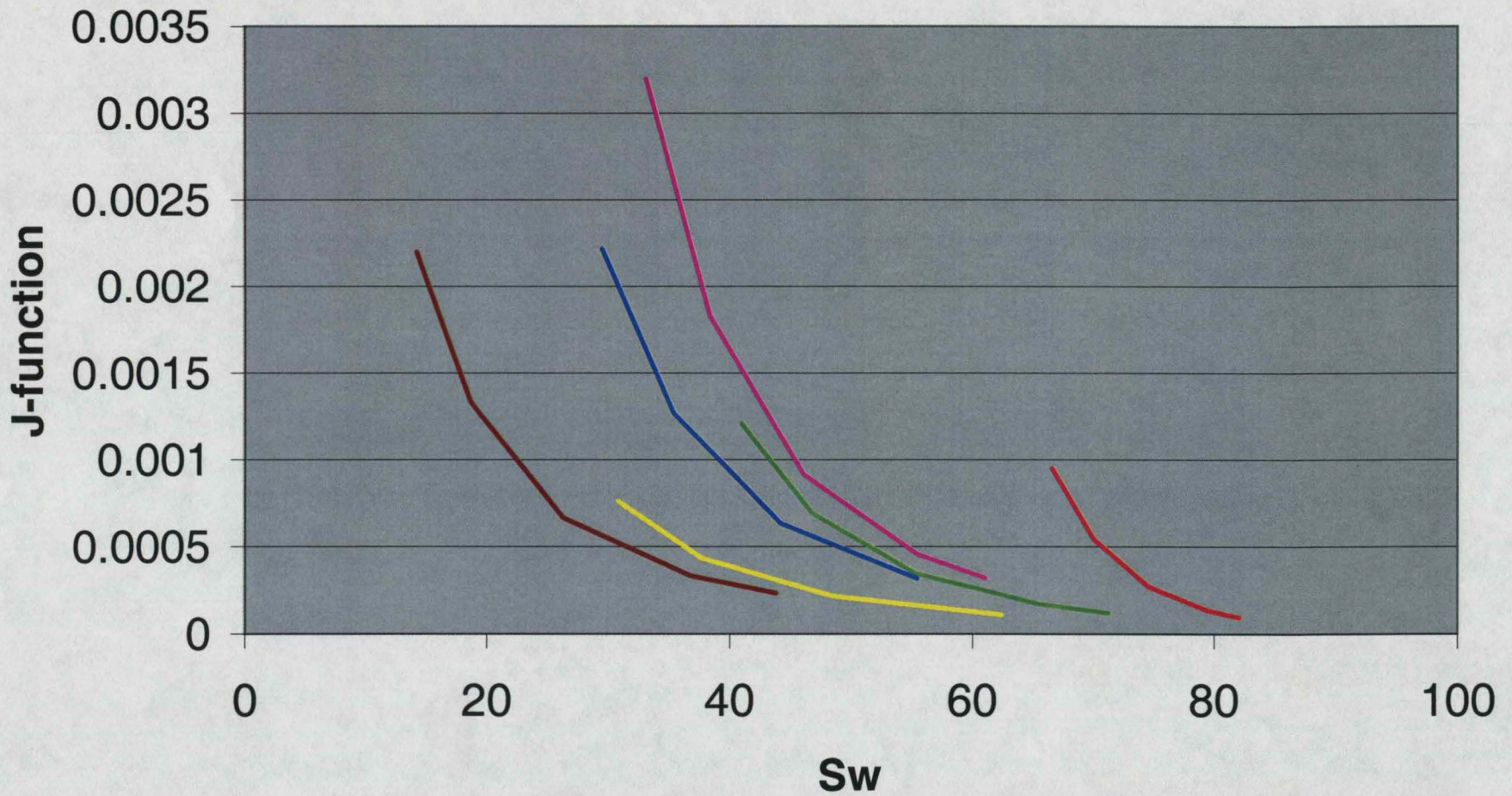
$$\frac{199 = 17.}{190 = 5.} \\ \hline 22$$

Lyle Schaben 2P - Pc @ 70 psi



- ◆ Smpl#10 ▲ Smpl#15 ● Smpl#17 ■ Smpl#22
- ✱ Smpl#27 ○ Smpl#31 + Smpl#42

Lyle Schaben 2P



— J10 — J15 — J17 — J22 — J27 — J42

J10 *J17* *J27*
J15
J22

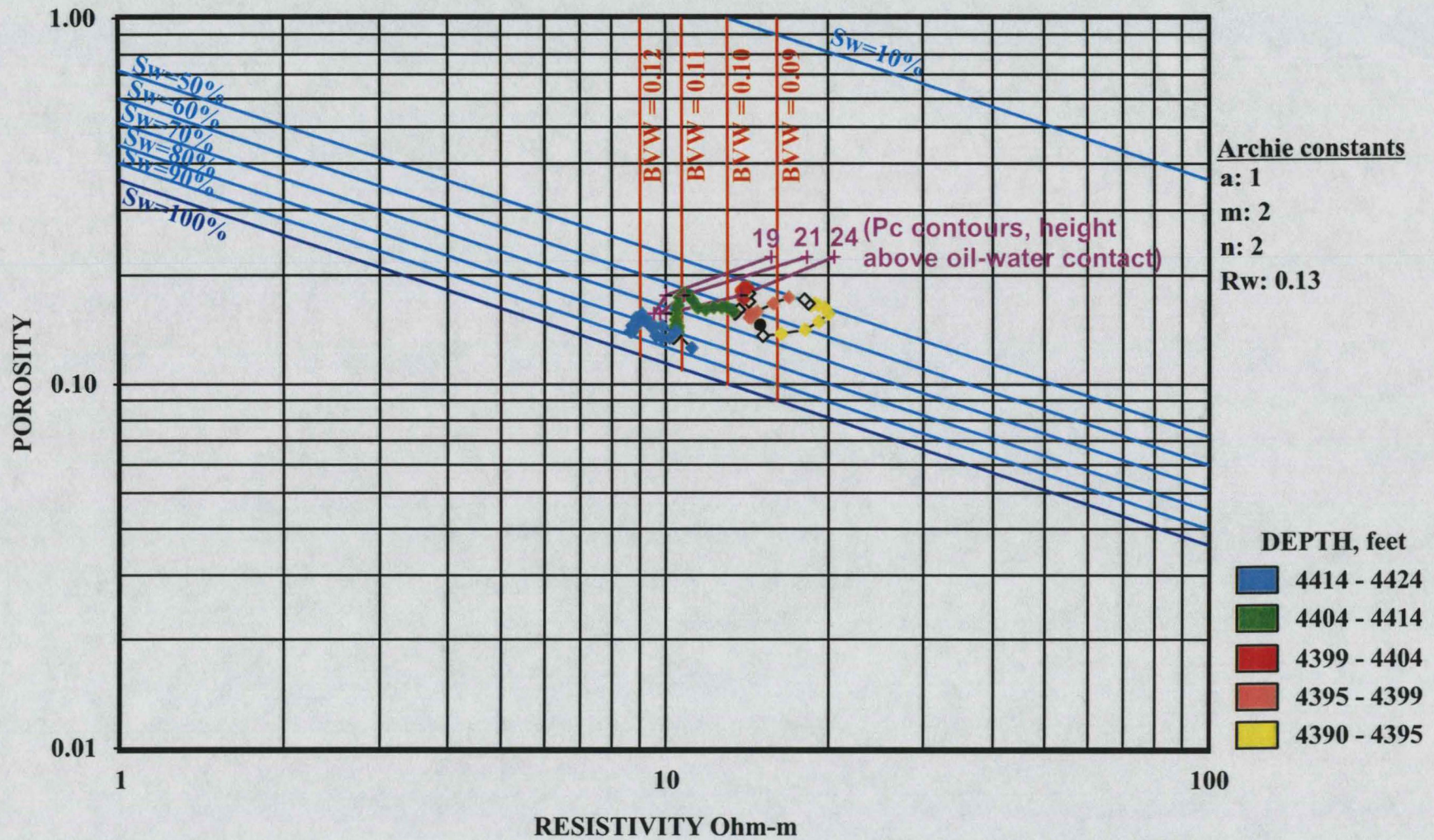


Figure --: Super Pickett plot of Lyle Schaben 2P well. Capillary pressure data from core plugs L#10, L#15, and L#42 plotted as height above oil-water contact contours. Perforated interval extends from 4400-4404 feet. Initial production rates: 53 bopd and 97 bwpd.

Sw vs. Phi - at air/brine Pc = 70 psi
 Rock fabric A - Lyle#10,15,42 & Foos#16,20,26

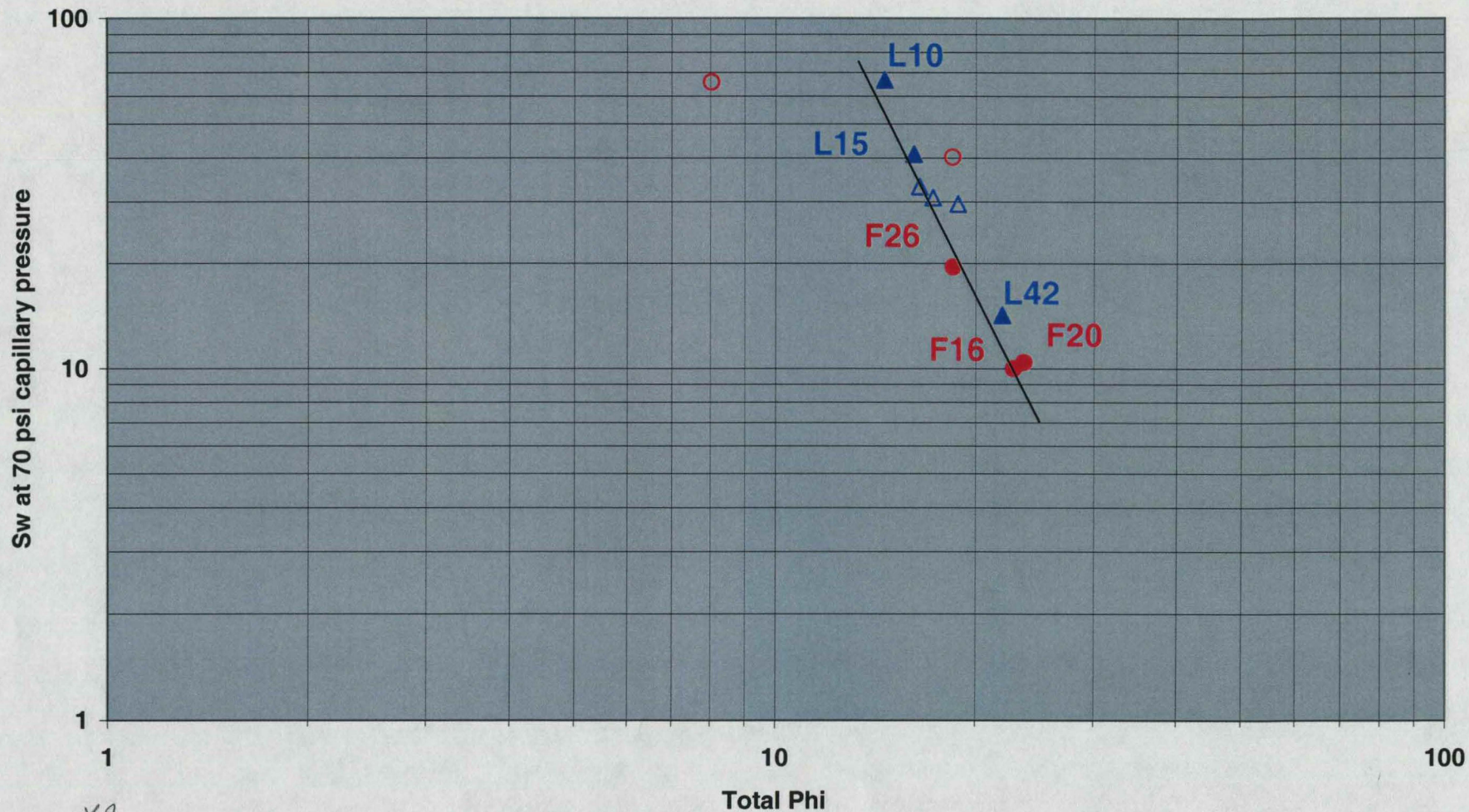


Figure 10^{x2}

- ▲ Rock fabric A - Lyle
- Rock fabric A - Foos
- Foos - other core plugs
- △ Lyle - other core plugs

Lyle Schaben 2P

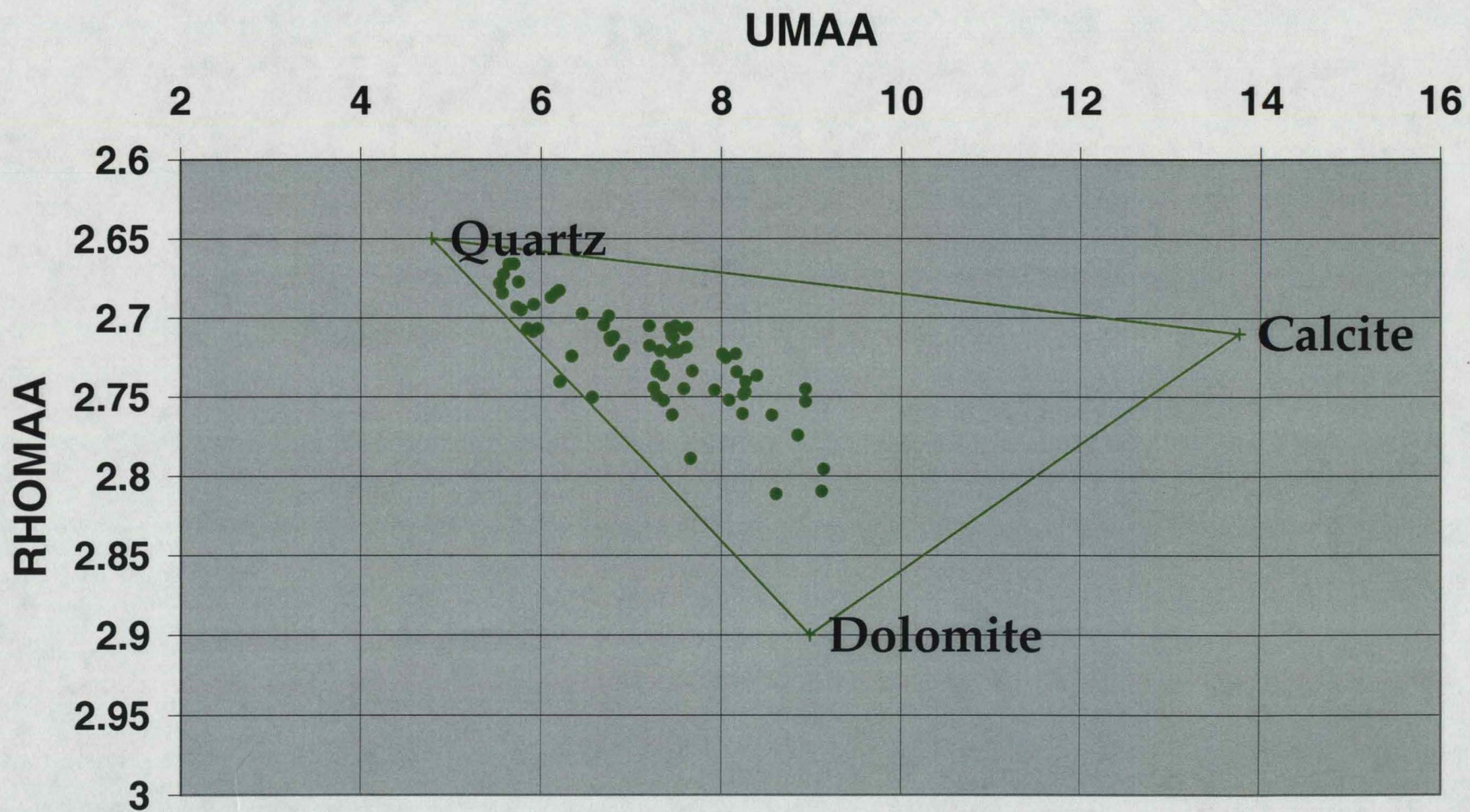


Figure 6

Lyle Schaben 2P - Pc @ 70 psi

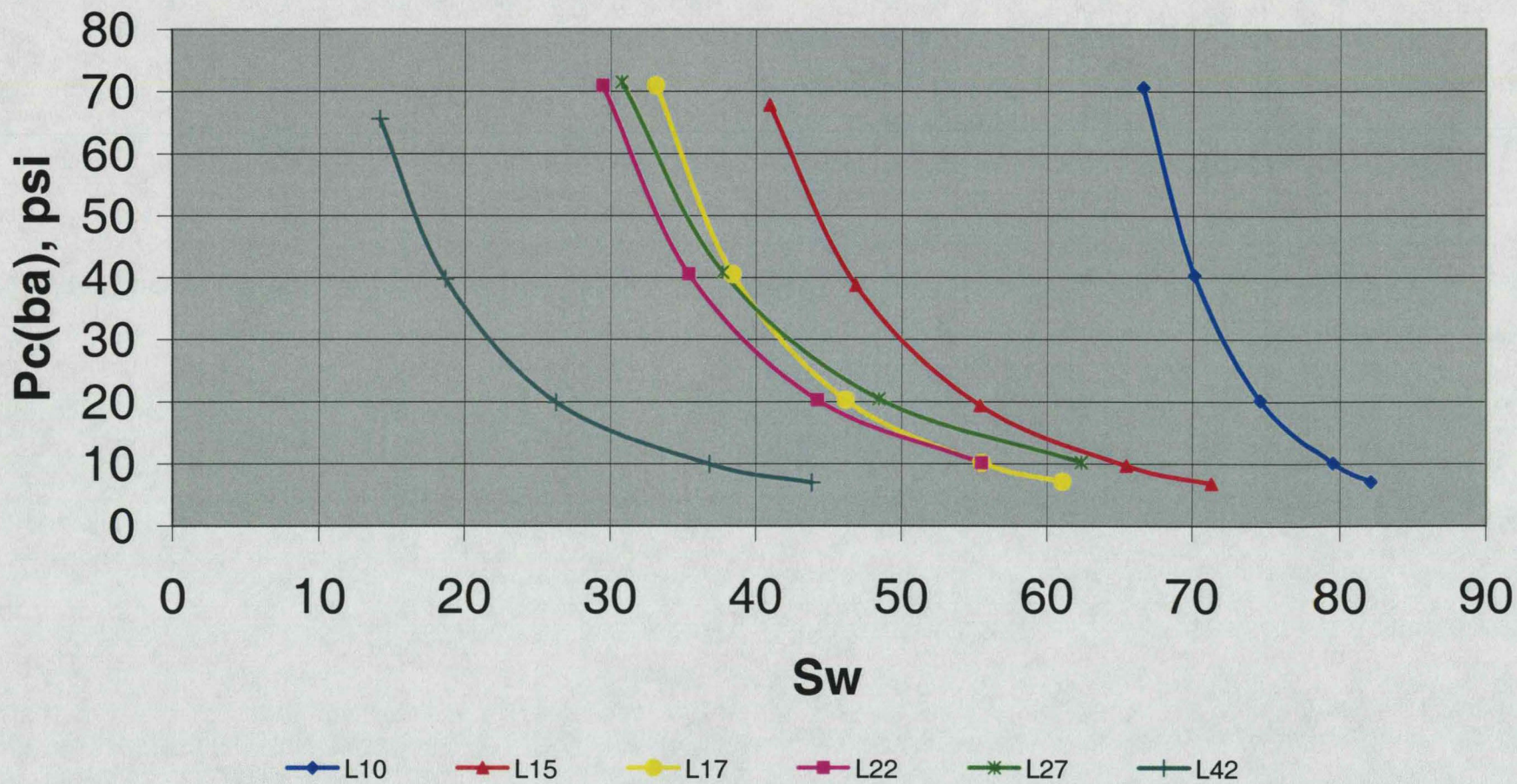


Figure: 7

Distribution of micro and macro porosity in Schaben field reservoir

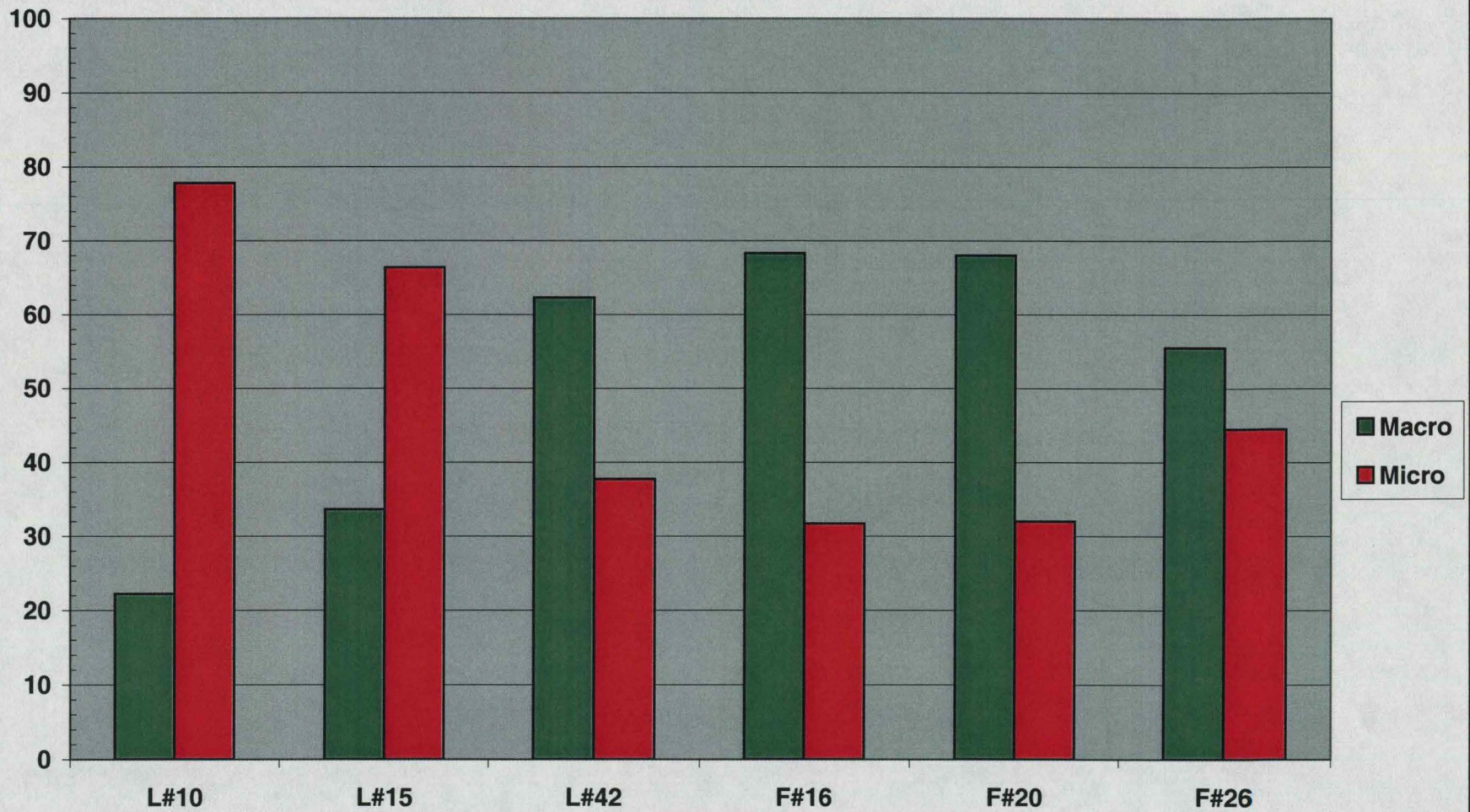
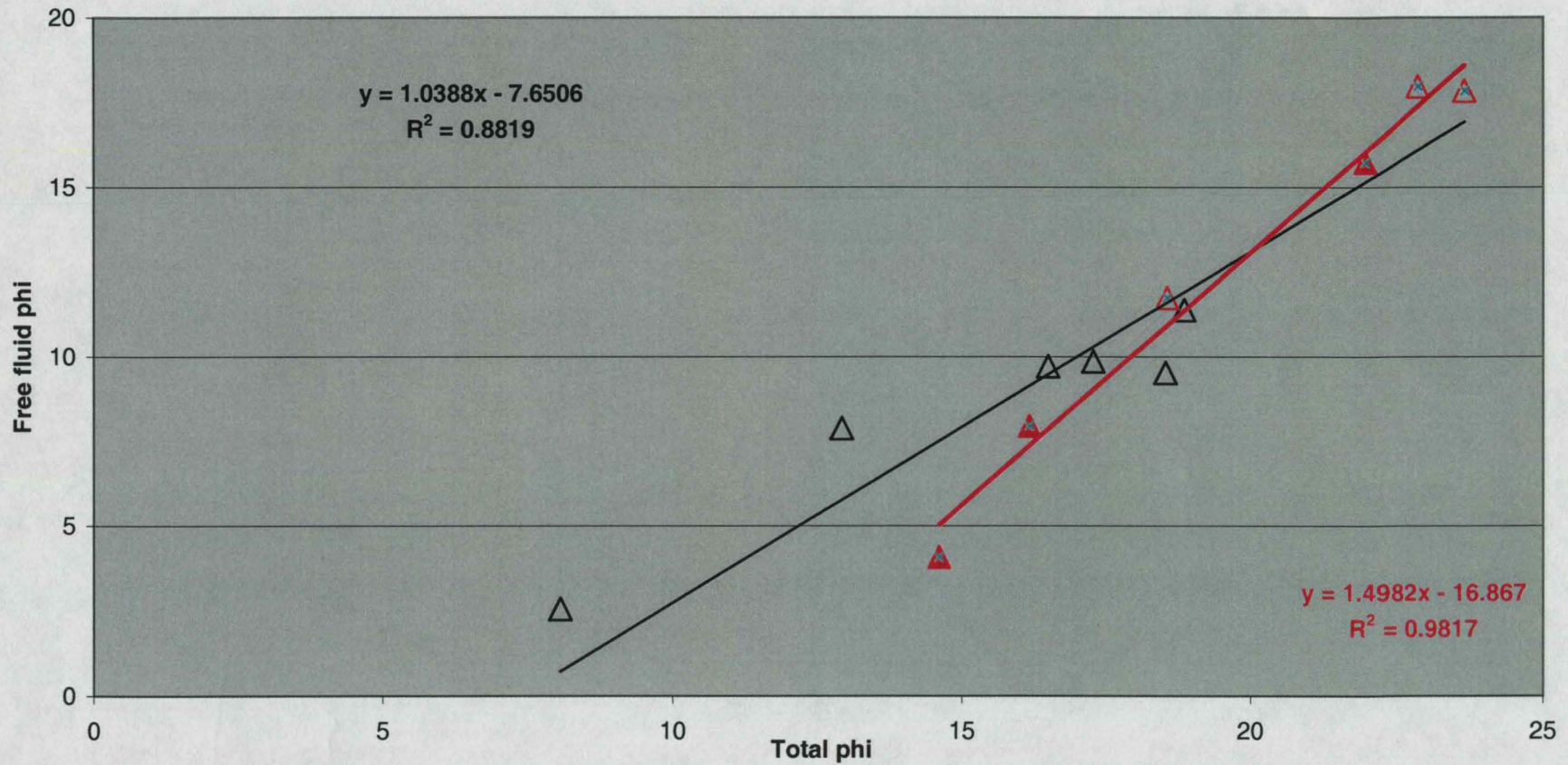


Figure 11/a

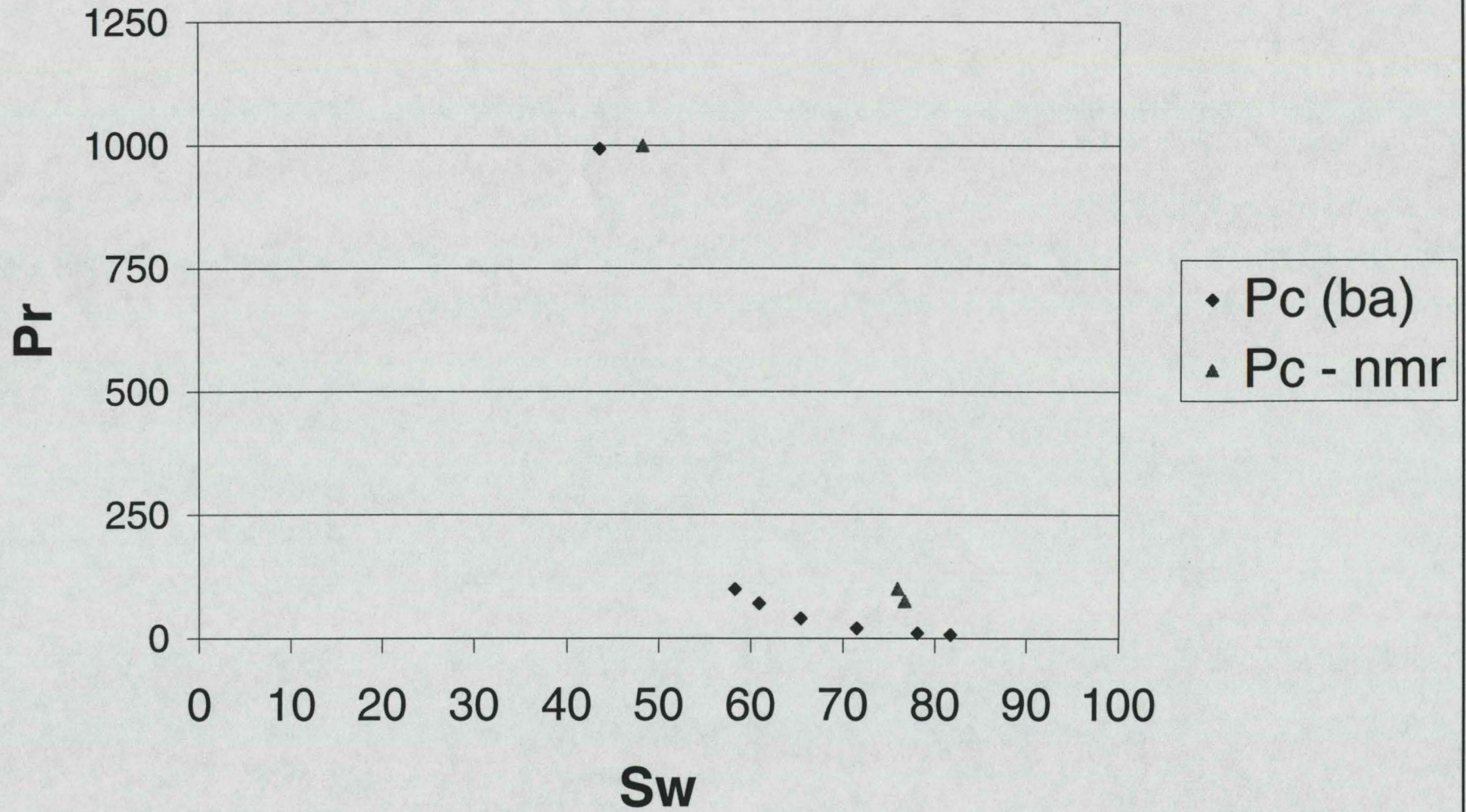
Free fluid phi vs. Total phi
Rock fabric A - Lyle#10,15, 42 & Foos#16,20,26



Δ All Plugs
 \blacktriangle Lyle - Rock fabric A
 \triangle Foos - Rock fabric A
 \times Rock fabric A
 — Linear (All Plugs)
 — Linear (Rock fabric A)

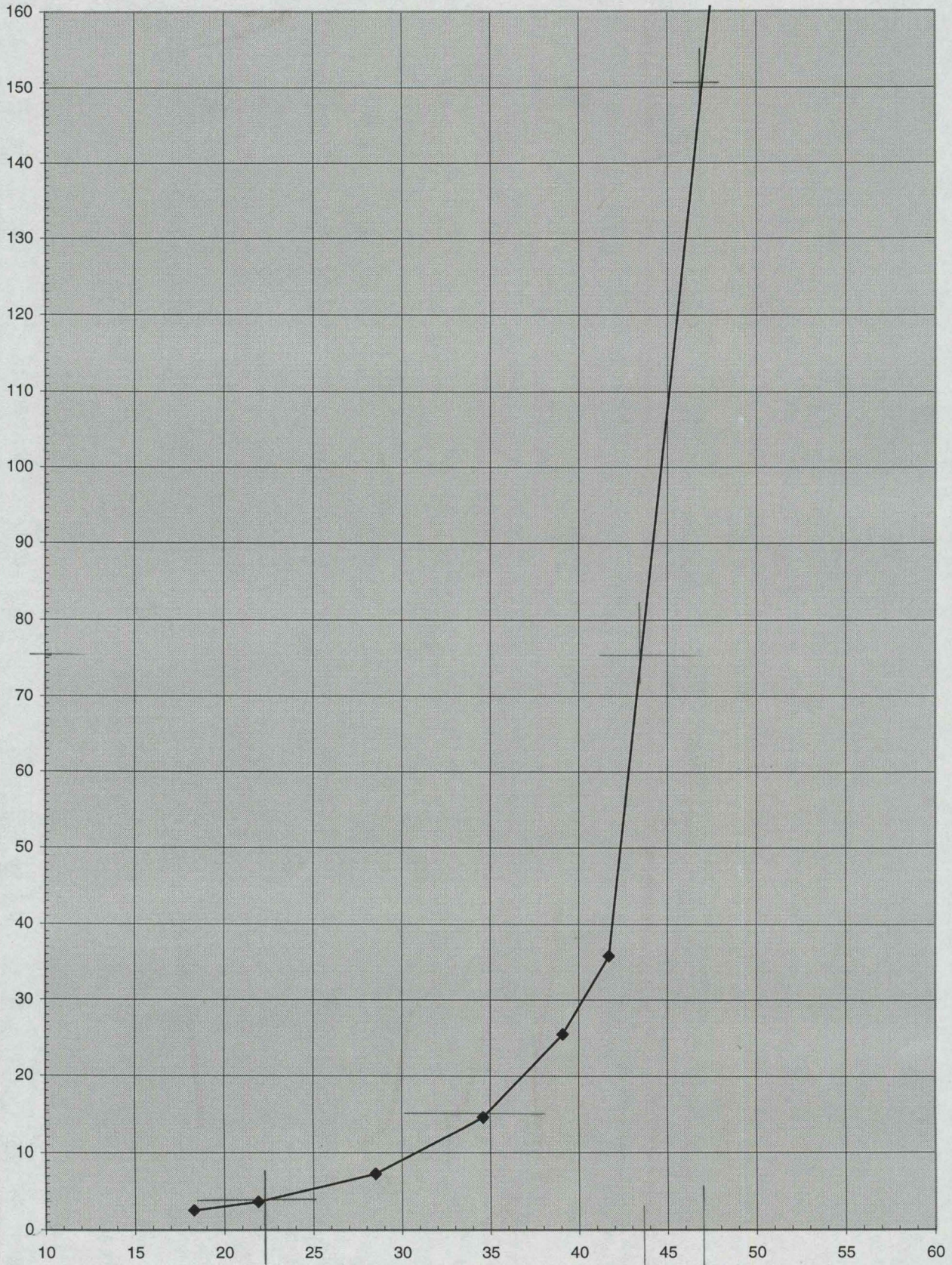
Figure 12 ¹⁰

S # 10 Lyle



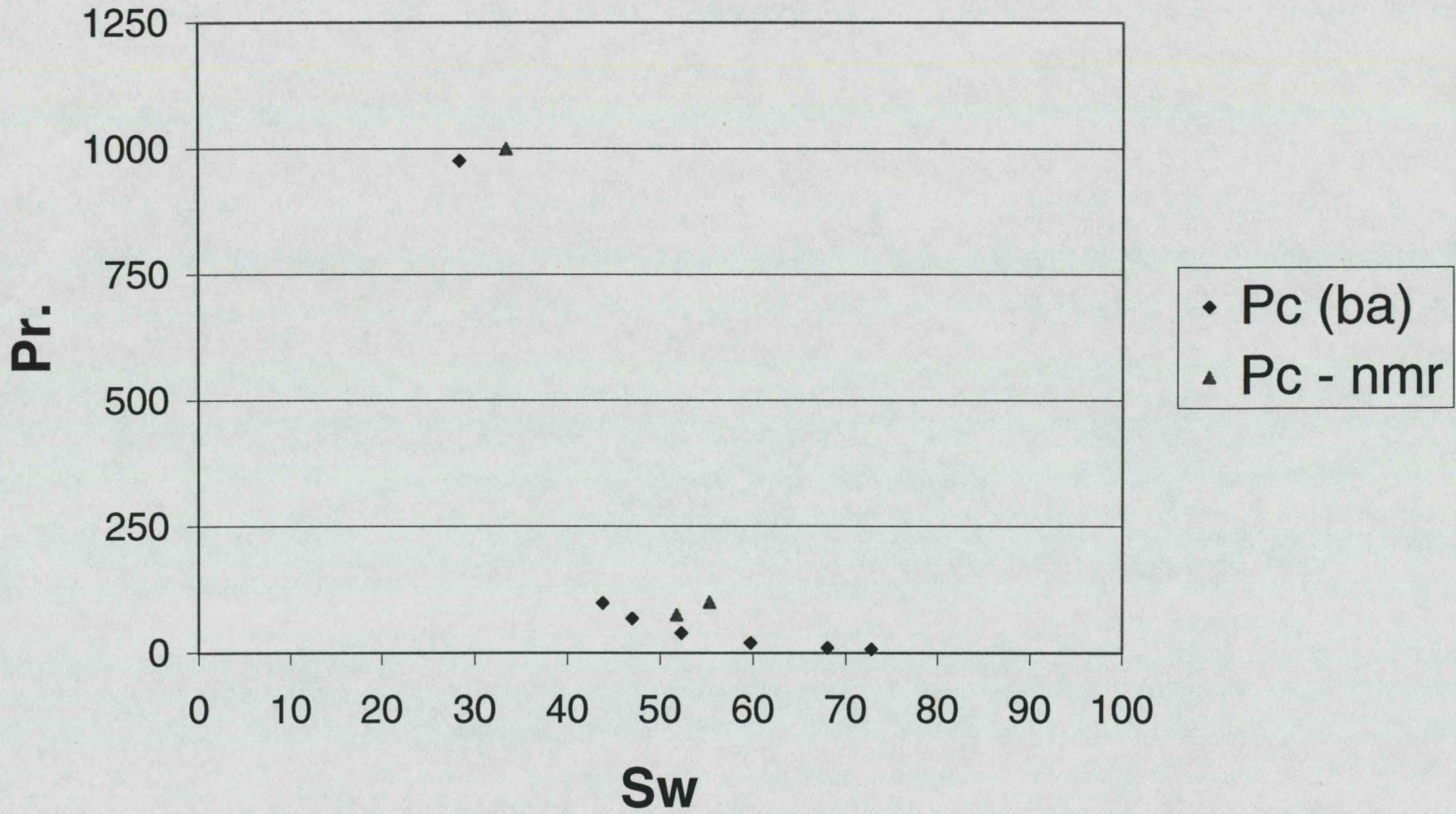
Sample #10 Lyle Schaben

Lyle Schaben

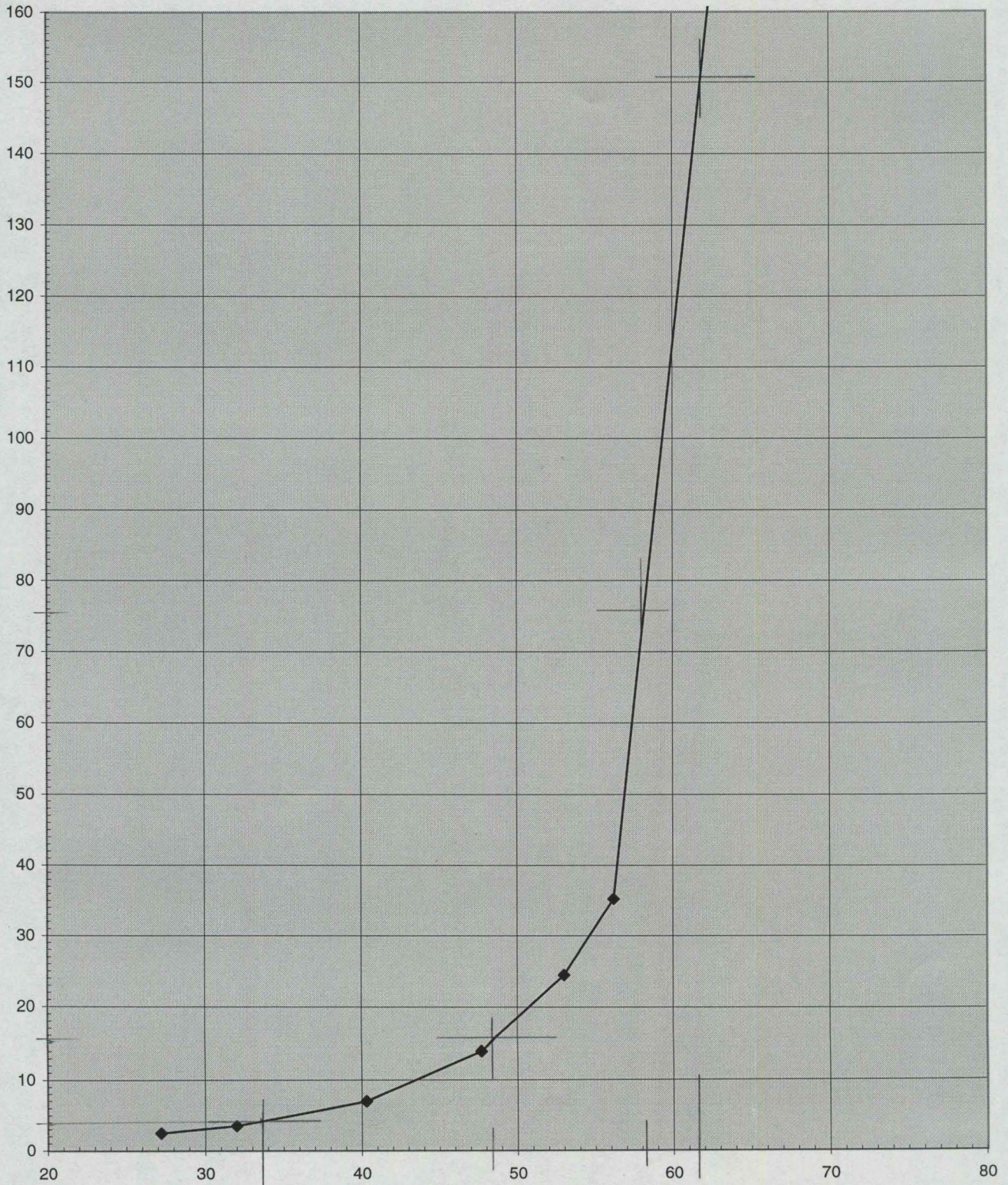


X

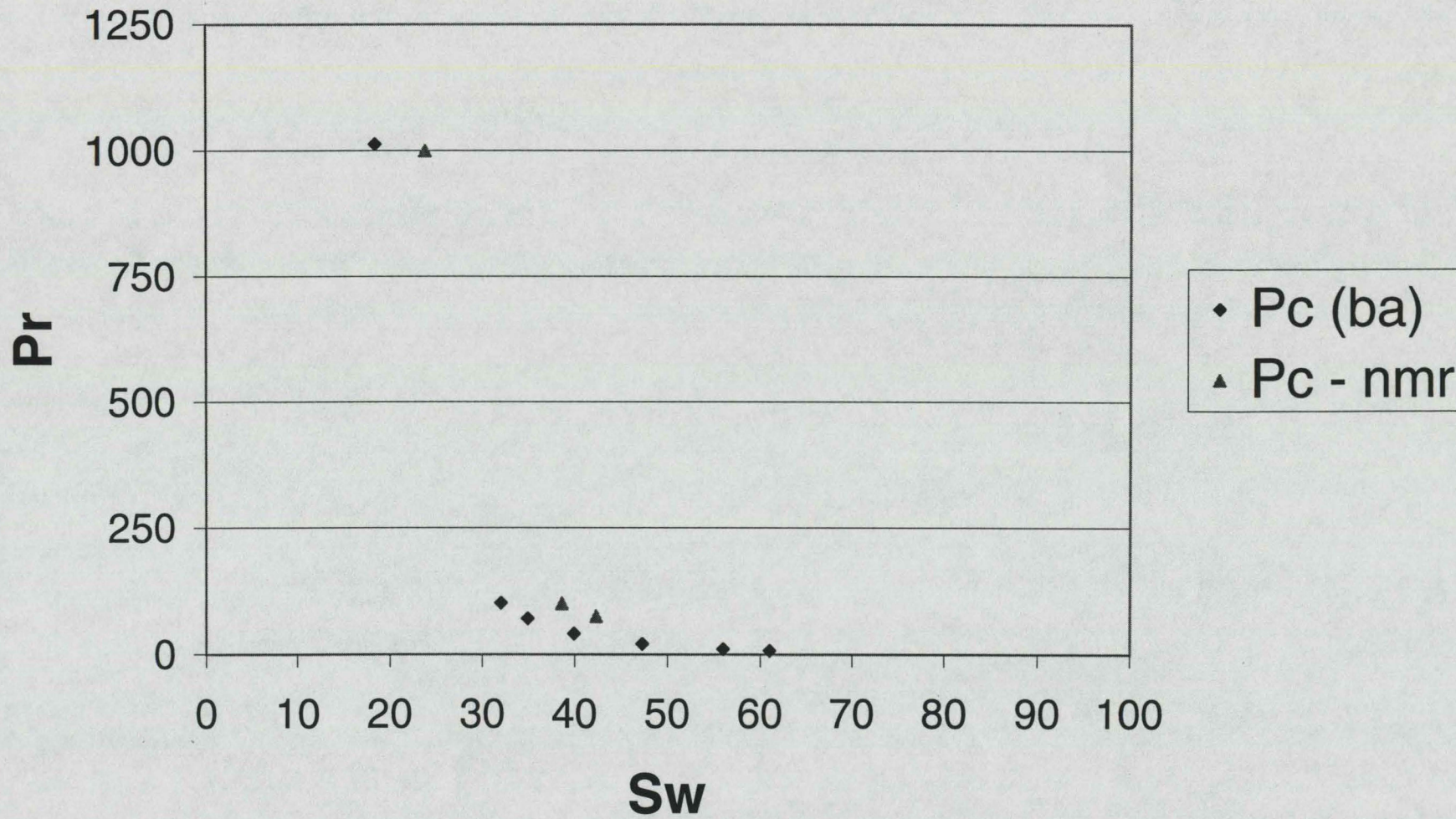
S # 15 Lyle



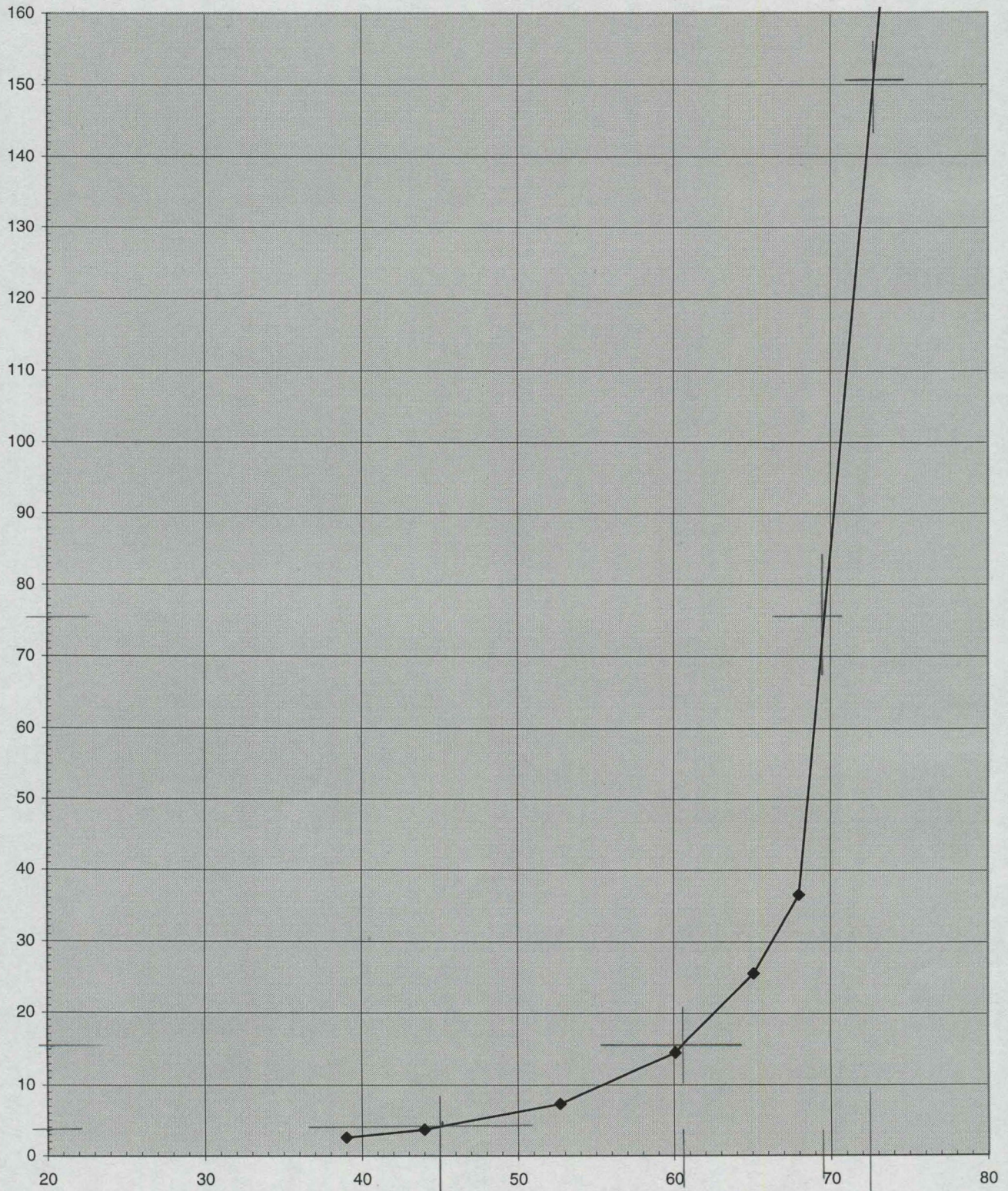
Sample #15



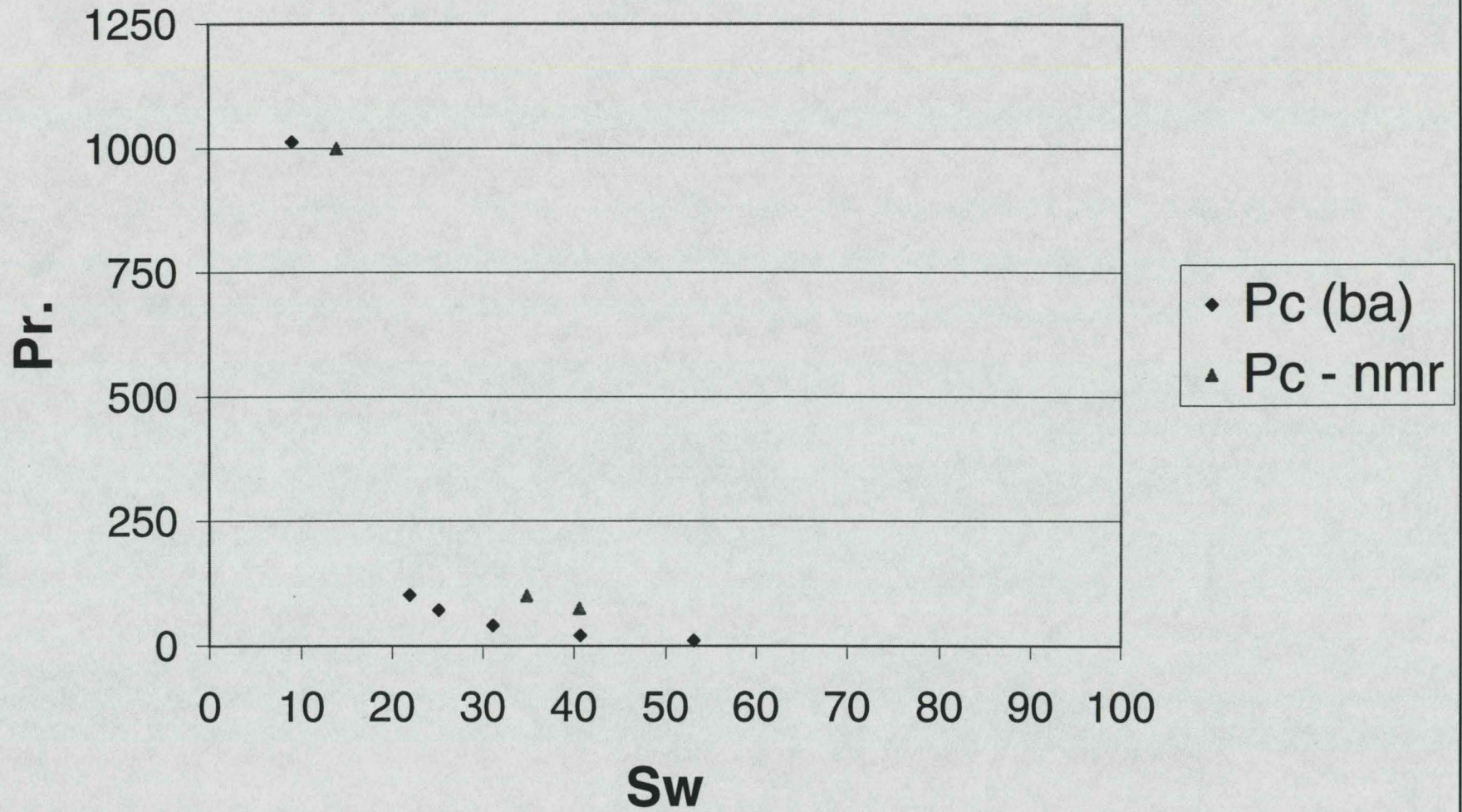
S # 17 Lyle



Sample #17

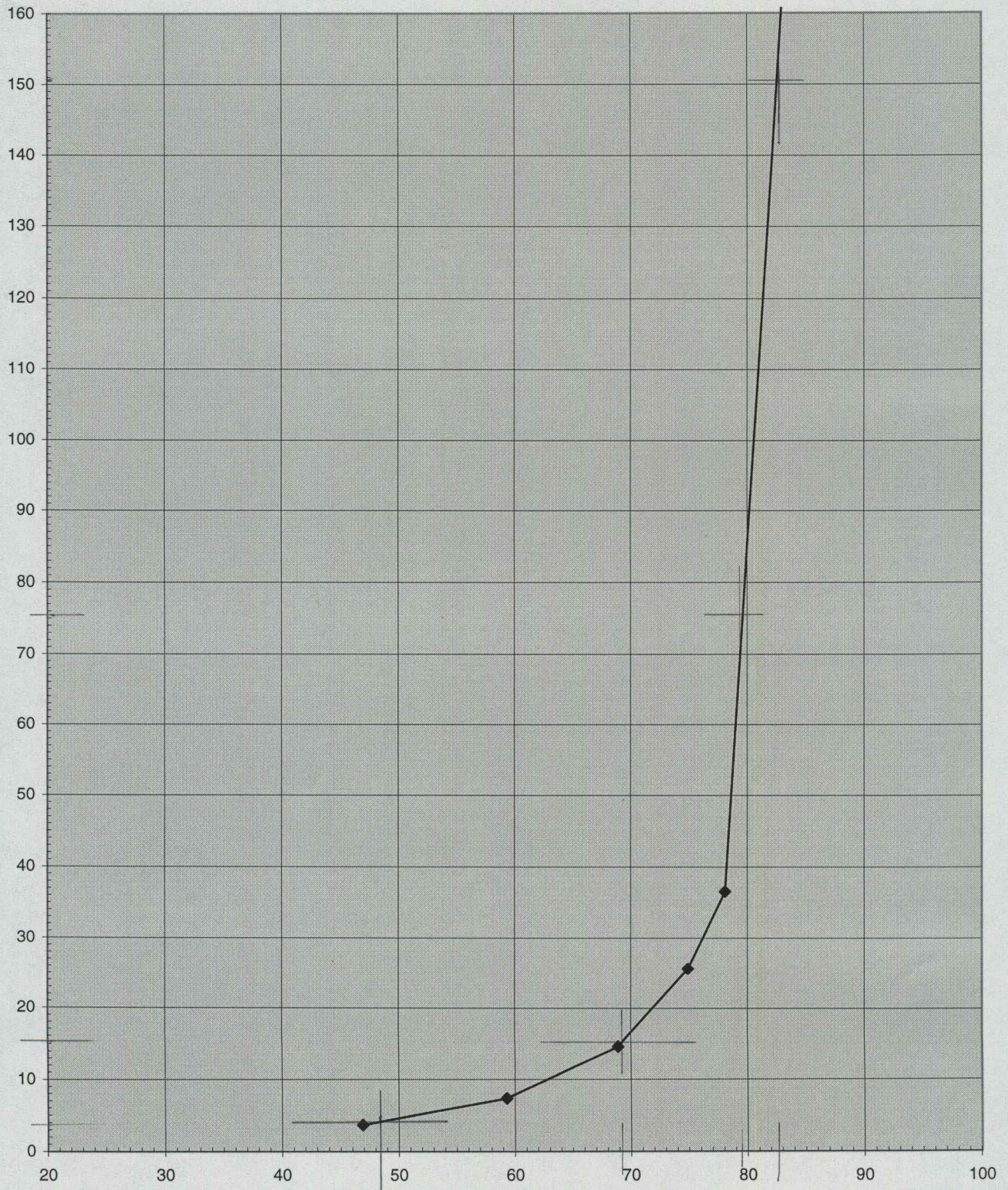


S # 22 Lyle



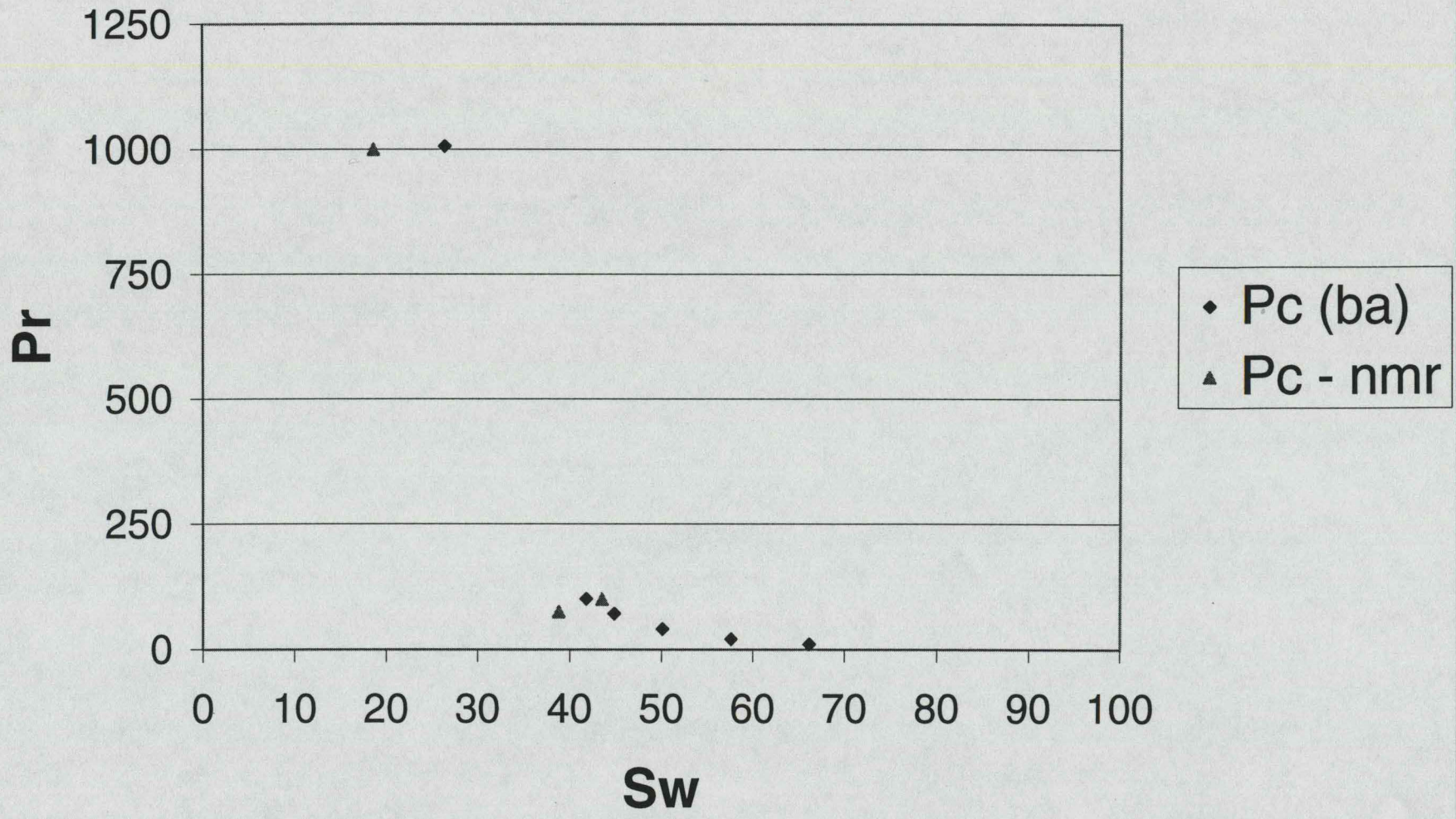
S# 22 Chart 12

Sample #22

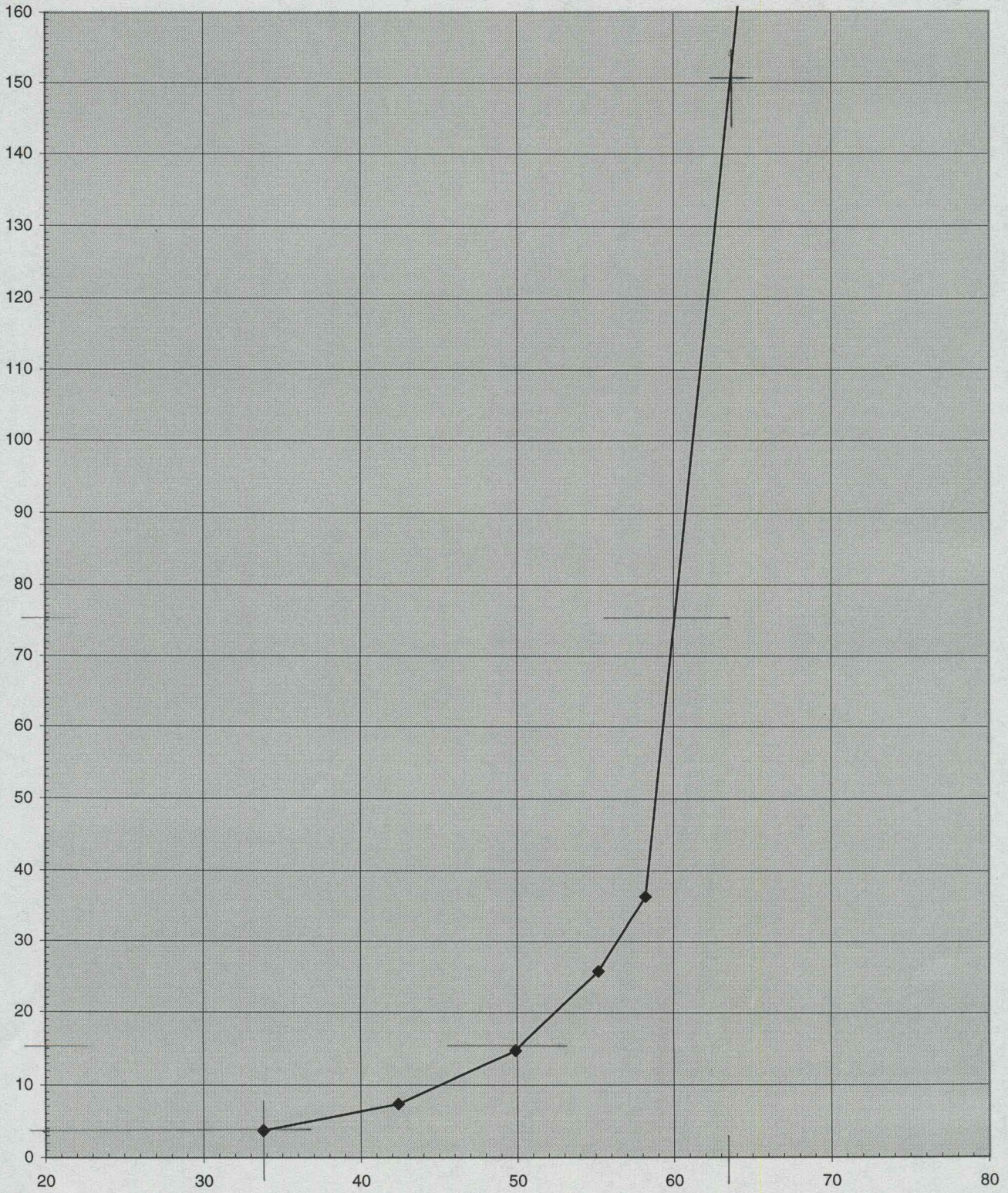


A

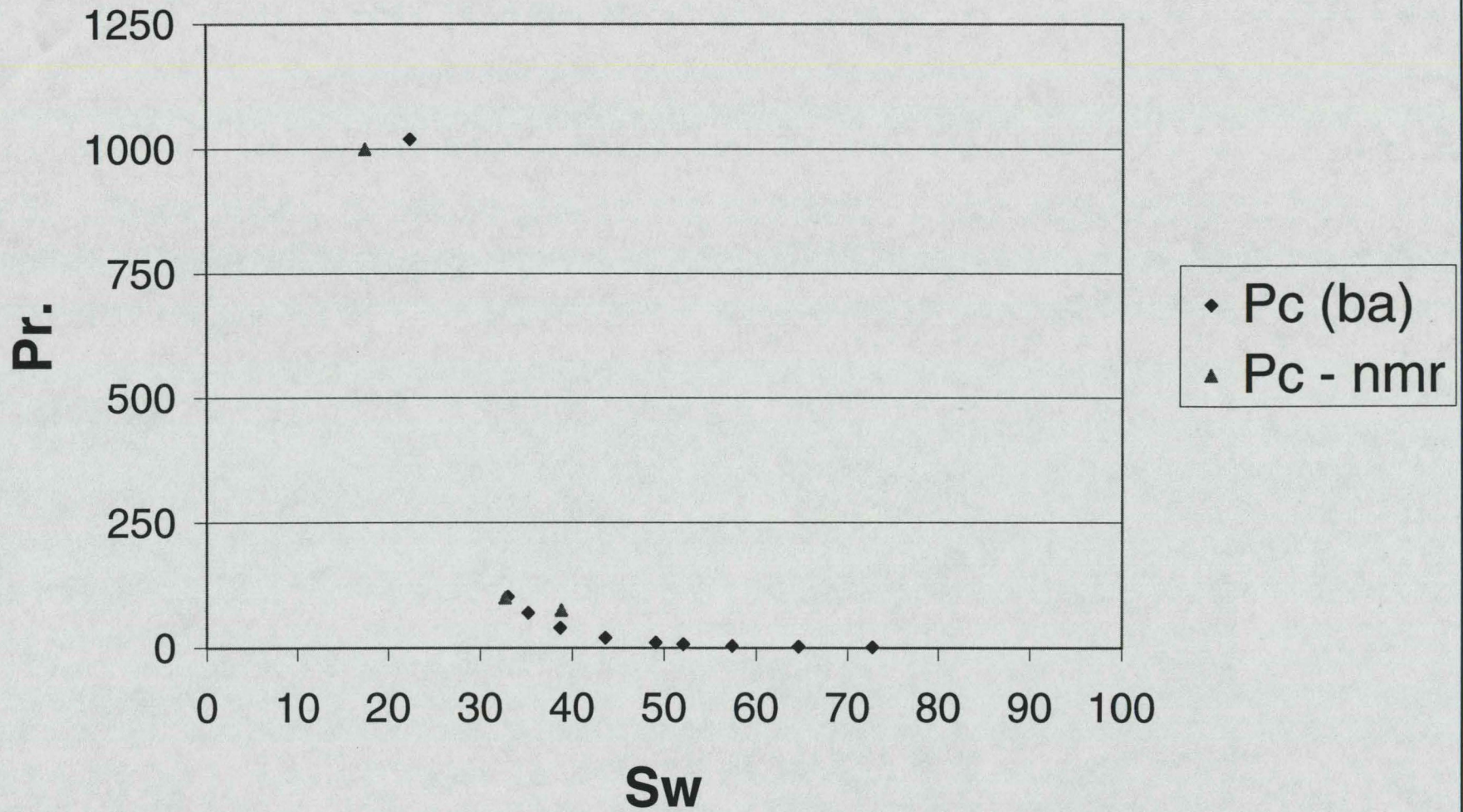
S # 27 Lyle



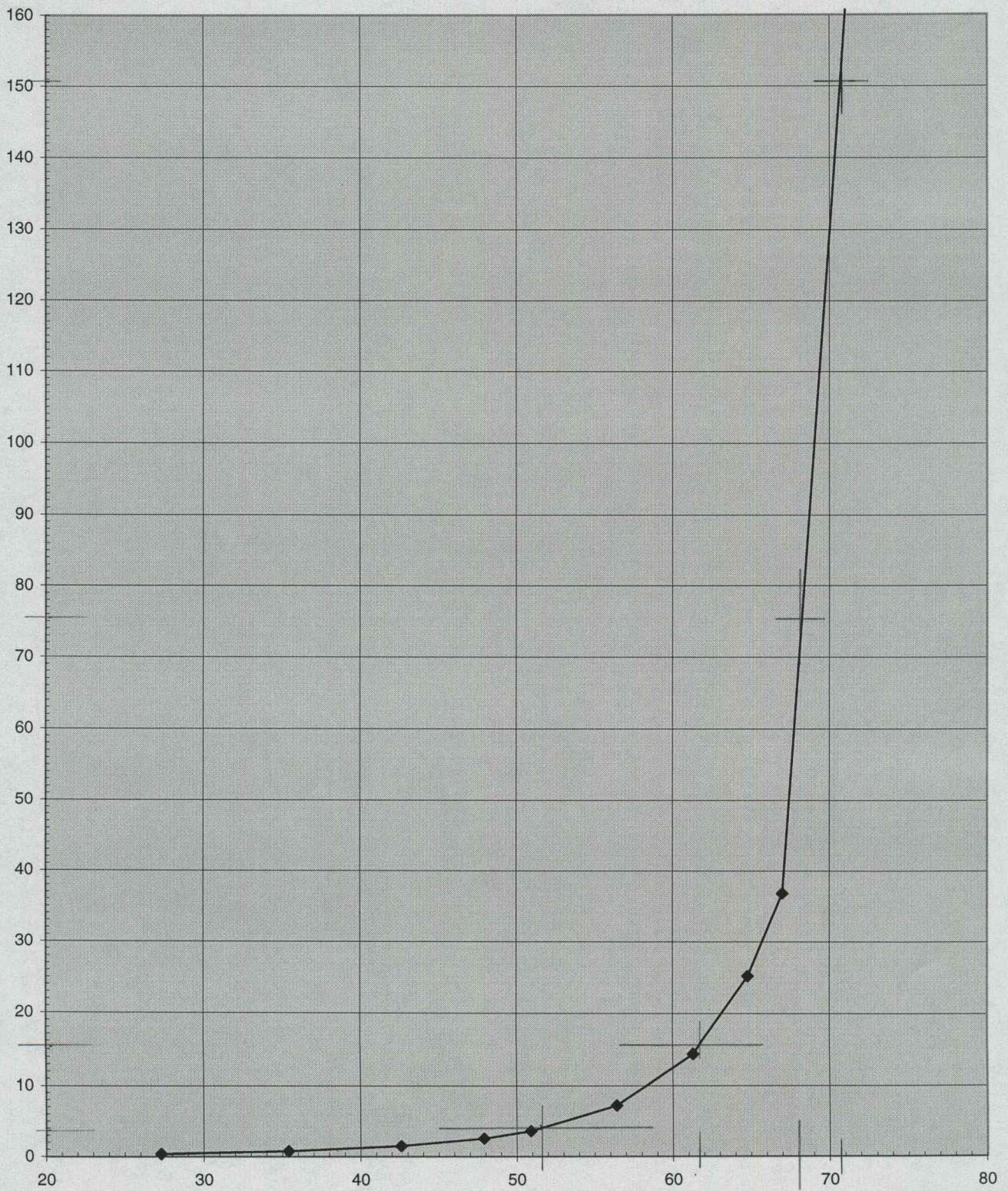
Sample #27



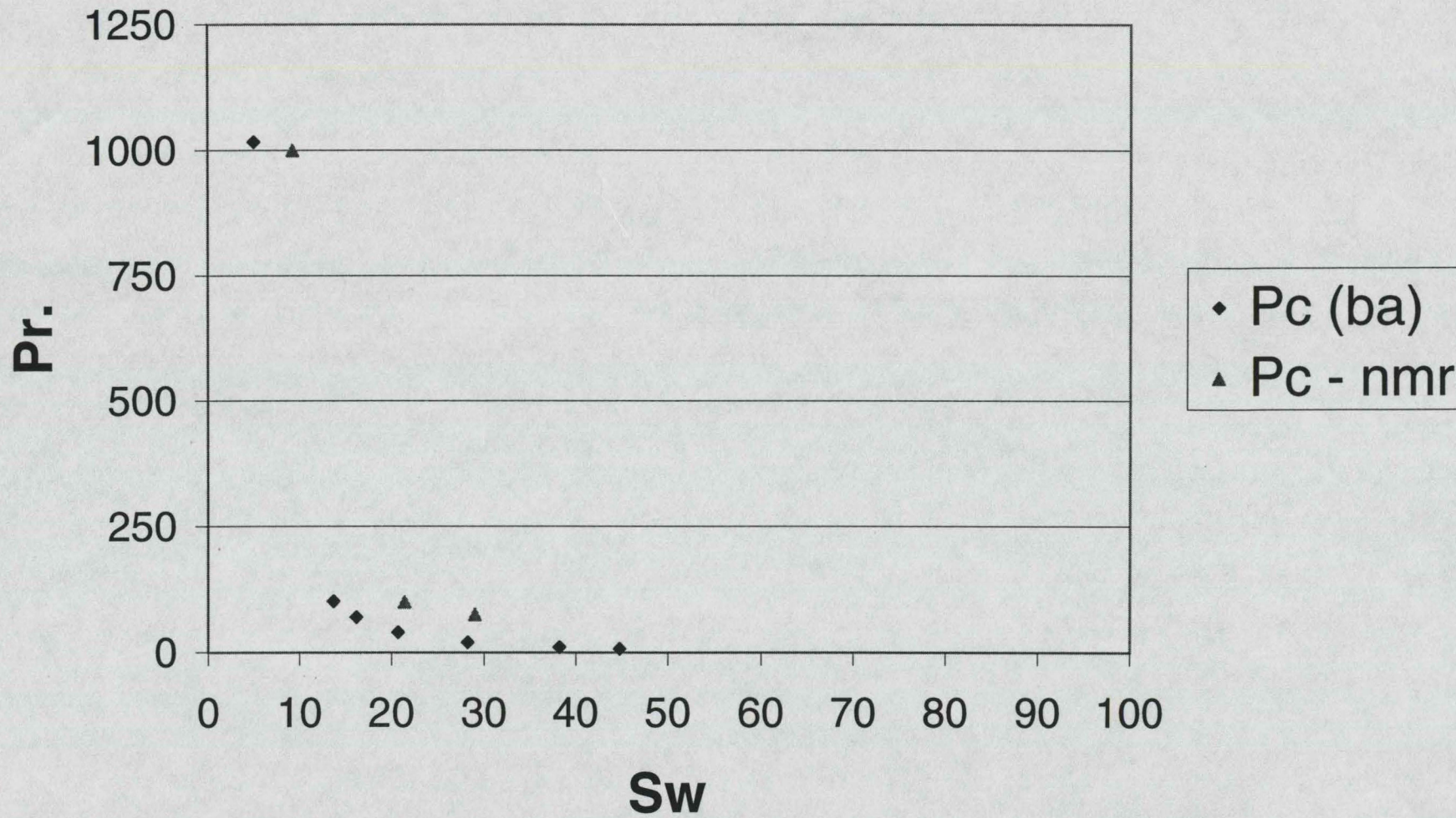
S # 31 Lyle



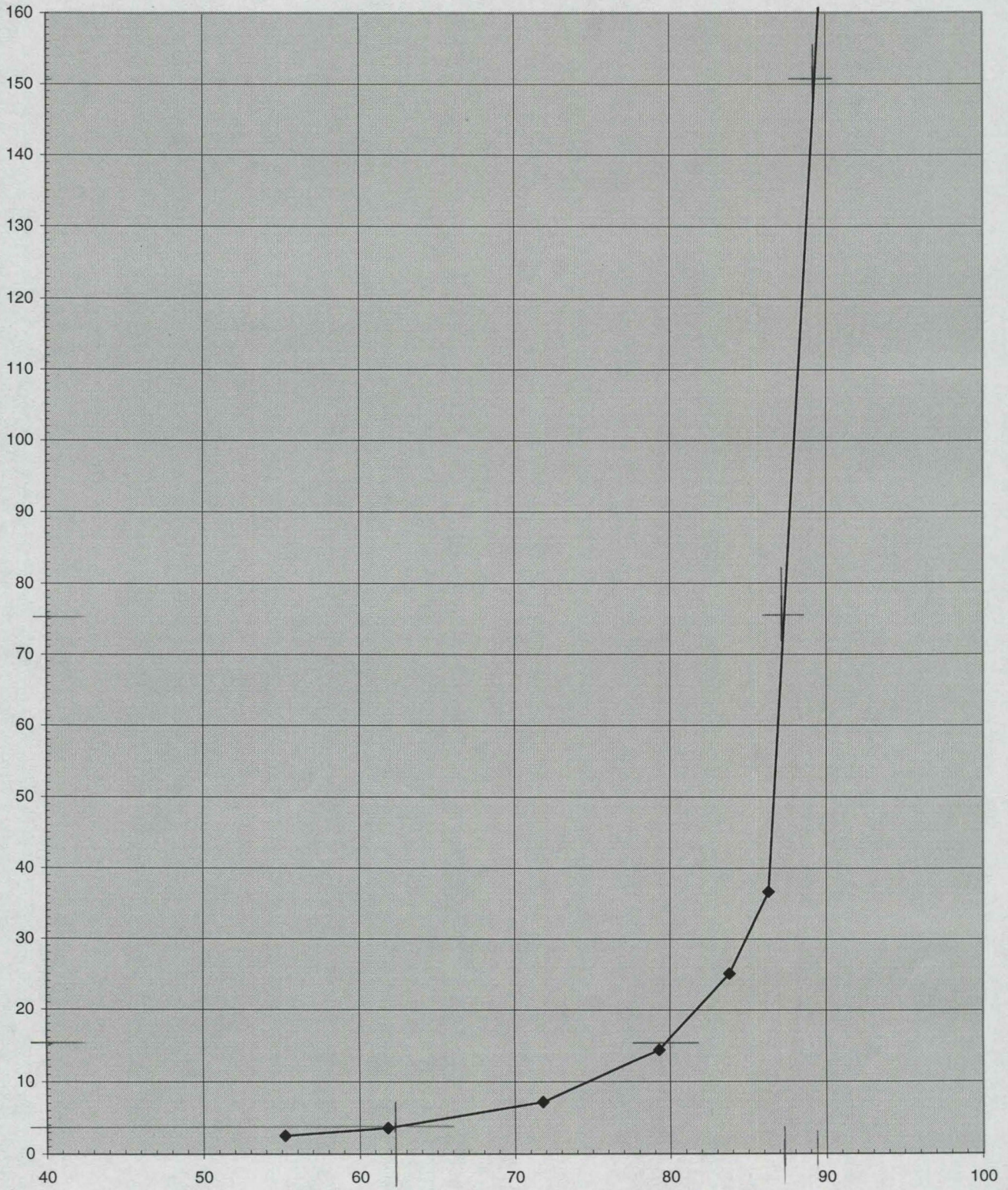
Sample #31



S # 42 Lyle



Sample #42



Lyle Schaben 2P (15-135-23925)

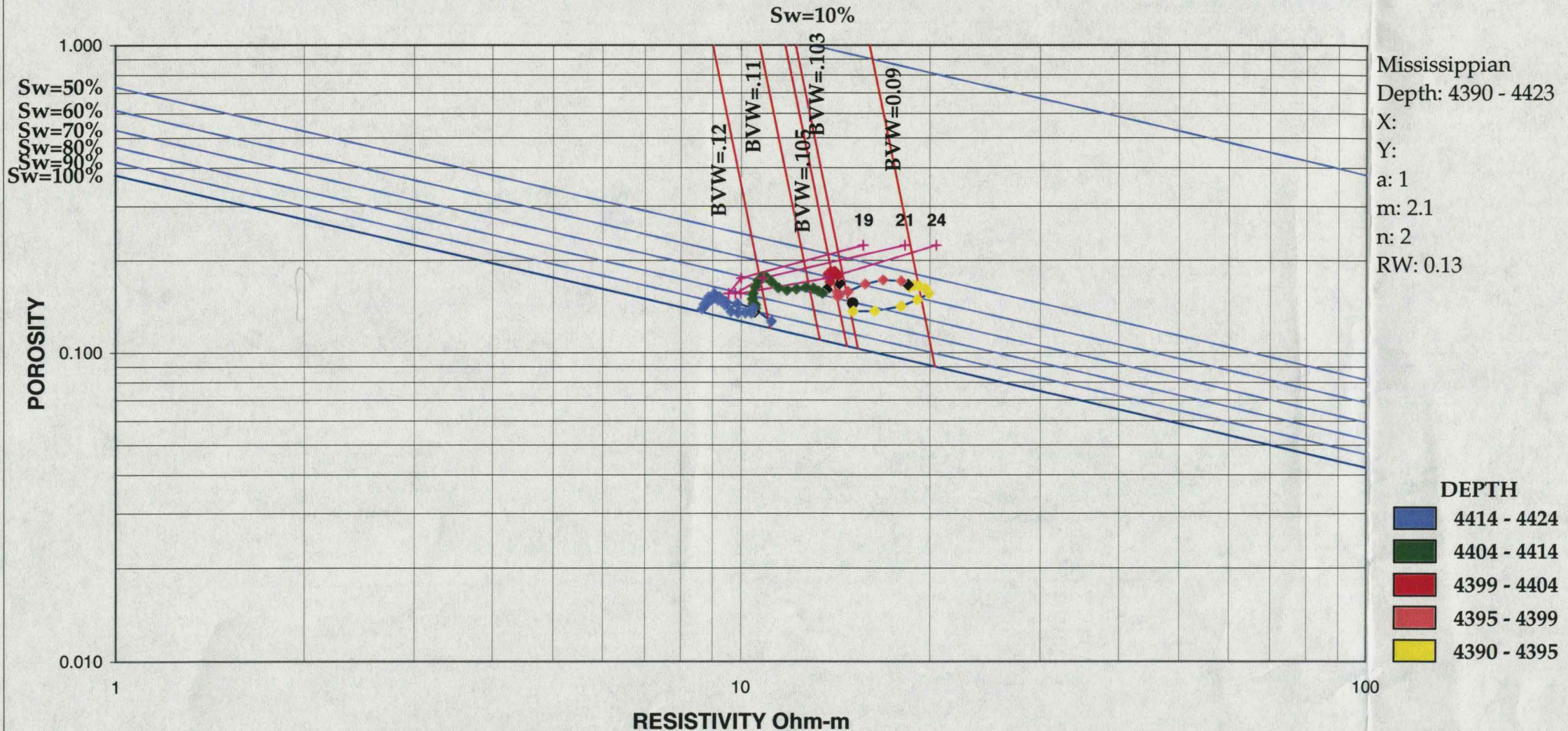


Figure: 3

Perf 4400-04: 53 bopd & 97 bwpd
Capillary pressure mapped: data from samples #10, 15, & 42

