

**KANSAS CORPORATION COMMISSION  
ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST**

FORM G-2  
(Rev. 8/98)

TYPE TEST:

- Open Flow  
 Deliverability

TEST DATE: 11/20/01

API No. 15-071-20700

Company Midcontinent Resources		Lease Angell			Well Number 2	
County Greeley	Location c NW	Section 5	TWP 20s	RNG (E/W)	Acres Attributed 640	
Field Bradshaw		Reservoir Winfield		Gas Gathering Connection Duke Energy		
Completion Date		Plug Back Total Depth 2880		Packer Set at		
Casing Size 4.500	Weight 10.500	Internal Diameter 4.052	Set at	Perforations 2811	To 2824	
Tubing Size 2.375	Weight 4.700	Internal Diameter 1.995	Set at 2834	Perforations	To	
Type Completion (Describe) natural		Type Fluid Production water		Pump Unit or Traveling Plunger? pumping unit		
Producing Thru (Annulus/Tubing) annulus		% Carbon Dioxide .023		% Nitrogen 25.574		Gas Gravity- Gg .838
Vertical Depth (H) 2820		Pressure Taps flange			Meter Run Size 2.067	
Pressure Buildup: Shut in		2001/11/16 @ 1300		TAKEN	2001/11/19 @ 1020	
Well on Line: Started		2001/11/19 @ 1020		TAKEN	2001/11/20 @ 1245	

**OBSERVED SURFACE DATA**

Static/ Dynamic Property	Orifice Size in.	Meter Pressure psig	Pressure Diff. In. H <sub>2</sub> O	Flowing Temp. t.	WellHead Temp. t.	Casing WellHead Press. (P <sub>w</sub> ) (P <sub>t</sub> ) (P <sub>c</sub> )		Tubing WellHead Press. (P <sub>w</sub> ) (P <sub>t</sub> ) (P <sub>c</sub> )		Duration (Hours)	Liquid Prod. Barrels
						psig	psia	psig	psia		
Shut-in						150	164				
Flow	1.000	106.0	15.00	56		106	120				

**FLOW STREAM ATTRIBUTES**

COEFFICIENT (F <sub>b</sub> ) Mcf/d	(METER) PRESSURE psia	EXTENSION $\sqrt{P_m \times H_w}$	GRAVITY FACTOR Fg	FLOWING TEMP FACTOR Ft	DEVIATION FACTOR Fpv	RATE OF FLOW R Mcf/d	GOR	G <sub>m</sub>
5.070	120.4	42.50	1.0924	1.0039	1.0128	239	3510	1.701

**(OPEN FLOW)(DELIVERABILITY) CALCULATIONS**

(P<sub>c</sub>)<sup>2</sup> = 27.0      (P<sub>w</sub>)<sup>2</sup> = 14.7      P<sub>d</sub> =      %      (P<sub>c</sub> - 14.4) + 14.4 =      (P<sub>a</sub>)<sup>2</sup> = 0.207  
(P<sub>d</sub>)<sup>2</sup> =

$(P_c)^2 - (P_a)^2$	$(P_c)^2 - (P_w)^2$	$\frac{(P_c)^2 - (P_a)^2}{(P_c)^2 - (P_w)^2}$ or $\frac{(P_c)^2 - (P_d)^2}{(P_c)^2 - (P_w)^2}$	LOG	Backpressure Curve Slope "n" ----- or ----- Assigned Standard Slope	n x LOG	Antilog	Open Flow Deliverability = R x Antilog Mcf/d
26.82	12.31	2.179	.3383	.848	.2869	1.936	463

OPEN FLOW      463      Mcfd @ 14.65 psia      DELIVERABILITY      Mcfd @ 14.65 psia

The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated herein and that said report is true and correct. Executed this the \_\_\_\_\_ day of \_\_\_\_\_, 20 \_\_\_\_\_

\_\_\_\_\_  
Witness (if any)  
\_\_\_\_\_  
For Commission

\_\_\_\_\_  
For Company  
\_\_\_\_\_  
Checked by