CORE ANALYSIS REPORT

FOR

WAGNER AND BROWN
ROSE NO. 1 WELL
KEARNY COUNTY, KANSAS

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
DALLAS, TEXAS 75207

REPLY TO
SUITE 133
400 SOUTH VERMONT
OKLAHOMA CITY, OKLA.
73108

June 5, 1978

Wagner and Brown
2625 Liberty Tower
Oklahoma City, Oklahoma 73102

Attn: Mr. Patrick Clare

Subject: Core Analysis Data
Rose No. 1 Well
Kearny County, Kansas
CLI File 3402-9324

Gentlemen:

Cores taken in the subject well in the Chase Group formation were received at the Oklahoma City laboratory for special analytical testing described on the procedure page.

The accompanying Coregraph presents the Surface Core-Gamma Log and binomially averaged core analysis data in graphical form to aid correlation with downhole electrical surveys.

Tabular presentation of the measured physical properties may be found on pages one through eleven of this report. Data averages reflecting zone changes are presented on pages twelve and thirteen.

Transparent overlays of a water cut curve have been furnished to Wagner and Brown's Oklahoma City and Midland, Texas offices. These curves are presented as an aid in selecting the most desirous zones for perforation in this well.

It is a pleasure to have this opportunity of serving you.

Very truly yours,

CORE LABORATORIES, INC.

Dale E. Boyle (VJP)

Dale E. Boyle
District Manager

DEB:VJP:nt

3 cc - Addressee
3 cc - Wagner and Brown
P. O. Box 1714
Midland, Texas 79701

Wagner And Brown
Rose No. 1 Well
CLI File 3402-9324

Procedure Page

Handling and Analytical Procedures

Diamond coring equipment and salt base mud were used to obtain 4.0 inch diameter cores between 2647 and 3025, 3092 and 3152 feet.

The cores were preserved at the well site in plastic bags by CLI personnel.

The cores were transported to Oklahoma City by CLI personnel.

A Core-Gamma Log was recorded for downhole E-Log correlation.

Core analysis was made in the intervals requested on right cylinder full diameter samples.

Fluid removal was accomplished using vacuum retorts.

Porosity was determined by density balance method.

Air permeability in two horizontal directions--measured without Klinkenberg correction.

Temporary storage of cores in Oklahoma City laboratory awaiting additional instructions.

WAGNER AND BROWN
ROSE NO. 1 WELL
WILDCAT
KEARNY COUNTY, KANSAS

DATE: 5/5/78
FORMATION: CHASE GROUP
DRLG. FLUID: SALT BASE MUD
LOCATION: SEC. 34-21S-37W

FILE NO: 3402-9324
ENGINEER: PUGH
ELEVATION: 3295' GL

* INDICATES PLUG PERM

WHOLE CORE ANALYSIS

SMP. NO.		DEPTH	PERM. TO AIR MD. MAXIMUM	90 DEG	POROSITY PERCENT	FLUID SATS. OIL	WTR.	GR. DEN.	DESCRIPTION
+	1	2647.0-48.0	12.0	5.1	13.7	0.0	69.2	2.74	SLT,DOL,CLAY
+	2	2648.0-49.0	51.0	14.0	16.4	0.0	64.5	2.71	SLT,DOL,CLAY
+	3	2649.0-50.0	65.0	28.0	16.1	0.0	68.3	2.70	SLT,DOL,CLAY
		2650.0-51.0							SH,SLTY,
+	4	2651.0-52.0	74.0	13.0	13.5	0.0	69.5	2.70	SLT,DOL,CLAY
+	5	2652.0-53.0	16.0	9.2	9.8	0.0	70.8	2.79	SLT,DOL,ANHY,CLAY
#	6	2653.0-54.0	245.0	173.0	21.7	0.0	64.5	2.76	SLT,ANHY,CLAY
+	7	2654.0-55.0	13.0	1.8	12.4	0.0	68.4	2.69	SLT,DOL,CLAY
#	8	2655.0-56.0	266.0	190.0	20.8	0.0	65.2	2.66	SLT,SHY,CLAY
#+	9	2656.0-57.0	653.0	597.0	21.9	0.0	60.8	2.69	SLT,SHY
+	10	2657.0-58.0	20.0	9.3	16.4	0.0	71.4	2.68	SLT,SL/DOL,CLAY
+	11	2658.0-59.0	296.0	290.0	15.2	0.0	73.8	2.75	SLT,DOL,CLAY
	12	2659.0-60.0	0.3	0.1	13.9	0.0	63.3	2.72	DOL,SLTY,CLAY
	13	2660.0-61.0	8.0	0.3	9.6	0.0	68.3	2.81	DOL,SLTY,SDY,CLAY
	14	2661.0-62.0	<0.1	<0.1	2.3	0.0	78.6	2.82	DOL,SDY
	15	2662.0-63.0	<0.1	<0.1	3.4	0.0	74.5	2.82	DOL,SDY,PP VGS,FOSS
	16	2663.0-64.0	<0.1	<0.1	3.8	0.0	73.8	2.84	DOL,SDY,PP VGS,ANHY
	17	2664.0-65.0	12.0	12.0	16.4	0.0	45.1	2.75	SD,DOL,MICA
	18	2665.0-66.0	12.0	11.0	14.0	0.0	50.8	2.73	SD,DOL,MICA
	19	2666.0-67.0	24.0	21.0	19.3	0.0	46.2	2.71	SD,DOL,MICA
	20	2667.0-68.0	0.4	0.3	6.7	0.0	54.2	2.83	DOL,SDY,MICA
	21	2668.0-69.0	7.5	7.5	19.6	0.0	46.8	2.72	SD,DOL,MICA
	22	2669.0-70.0	0.6	0.4	9.0	0.0	47.5	2.75	DOL,SDY,MICA
	23	2670.0-71.0	0.2	0.1	8.0	0.0	50.9	2.76	DOL,SDY,MICA
	24	2671.0-72.0	<0.1	<0.1	12.8	0.0	45.2	2.71	DOL,SHY,SDY,ANHY
	25	2672.0-73.0	50.0	31.0	14.0	0.0	62.7	2.79	SLT,DOL,SH STKS,ANHY

CORE LABORATORIES, INC.

Petroleum Reservoir Engineering

DALLAS, TEXAS

WAGNER AND BROWN
ROSE NO. 1 WELL

DATE: 5/5/78
FORMATION: CHASE GROUP

FILE NO: 3402-9324
ENGINEER: PUGH

SMP. NO.	DEPTH	PERM. TO AIR MD. MAXIMUM	90 DEG	POROSITY PERCENT	FLUID SATS. OIL	WTR.	GR. DEN.	DESCRIPTION
+ 26	2673.0-74.0	3.1	2.7	11.4	0.0	48.6	2.81	SLT,DOL,SH STKS,ANH
	2674.0-78.0							SH
+ 27	2678.0-79.0	23.0	0.8	13.2	0.0	65.6	2.70	SLT,DOL,SHY
28	2679.0-80.0	<0.1	<0.1	9.1	0.0	68.8	2.74	DOL,SL/SLTY
	2680.0-82.0							SH
+ 29	2682.0-83.0	104.0	90.0	13.7	0.0	69.9	2.73	SLT,DOL,CLAY
+ 30	2683.0-84.0	18.0	0.2	10.2	0.0	71.3	2.72	SLT,DOL,CLAY
+ 31	2684.0-85.0	101.0	41.0	10.9	0.0	72.2	2.68	SLT,SL/DOL,CLAY
	2685.0-86.0							SH
+ 32	2686.0-87.0	90.0	0.3	6.1	0.0	89.9	2.79	SLT,DOL,ANHY,CLAY
33	2687.0-88.0	0.1	0.1	11.0	0.0	72.6	2.72	SLT,DOL,SL/SDY,CLAY
+ 34	2688.0-89.0	1.0	0.5	15.4	0.0	68.8	2.72	SLT,DOL,SL/SDY,CLAY
+ 35	2689.0-90.0	71.0	34.0	11.9	0.0	70.1	2.71	SLT,DOL,SL/SDY,CLAY
36	2690.0-91.0	0.7	0.2	11.5	0.0	69.1	2.77	SLT,DOL,SL/SDY,CLAY
+ 37	2691.0-92.0	17.0	1.0	12.3	0.0	68.8	2.69	SLT,DOL,SL/SDY,CLAY
38	2692.0-93.0	0.1	<0.1	13.6	0.0	68.3	2.70	SLT,DOL,SL/SDY,CLAY
+ 39	2693.0-94.0	17.0	6.5	15.2	0.0	63.5	2.68	SD,SL/DOL,SDY,CLAY
+ 40	2694.0-95.0	2.2	0.1	9.2	0.0	75.5	2.70	SLT,SL/DOL,CLAY
+ 41	2695.0-96.0	4.7	0.4	11.6	0.0	70.9	2.71	SLT,SL/DOL,CLAY
42	2696.0-97.0	0.1	0.1	16.4	0.0	64.4	2.70	SLT,SL/DOL,SDY,CLAY
+ 43	2697.0-98.0	56.0	34.0	16.5	0.0	63.5	2.68	SLT,SL/DOL,SDY,CLAY
+ 44	2698.0-99.0	14.0	4.8	13.9	0.0	68.7	2.71	SLT,DOL,SDY,CLAY
+ 45	2699.0-00.0	4.6	0.2	13.5	0.0	68.0	2.70	SLT,DOL,CLAY
#+ 46	2700.0-01.0	13.0	11.0	14.5	0.0	65.1	2.65	SLT,CLAY
	2701.0-04.0							SH
+ 47	2704.0-05.0	57.0	22.0	9.5	0.0	73.8	2.71	SLT,DOL,CLAY
48	2705.0-06.0	0.5	0.3	11.5	0.0	69.9	2.69	SLT,SL/DOL,CLAY
+ 49	2706.0-07.0	15.0	2.5	18.3	0.0	62.0	2.54	SLT,CLAY
+ 50	2707.0-08.0	29.0	27.0	15.1	0.0	72.2	2.75	SLT,DOL,CLAY
	2708.0-09.0							SH
51	2709.0-10.0	0.3	<0.1	14.6	0.0	68.1	2.86	DOL,SHY,SLTY,PP VGS
52	2710.0-11.0	0.9	0.8	13.3	0.0	57.3	2.7?	SLT,DOL

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ENGINEER: PUGH

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53	2711.0-12.0	0.9	0.9	14.9	0.0	52.2	2.78	SLT,DOL,ANHY
54	2712.0-13.0	0.8	0.8	12.2	0.0	56.1	2.77	SLT,DOL,MICA
55	2713.0-14.0	0.2	0.2	10.9	0.0	51.1	2.76	SLT,DOL,MICA
56	2714.0-15.0	0.2	0.1	10.7	0.0	64.0	2.81	SLT,DOL,SH STKS,ANHY
57	2715.0-16.0	0.1	0.1	8.6	0.0	73.8	2.83	SLT,DOL,SL/SHY,ANHY
58	2716.0-17.0	<0.1	<0.1	7.3	0.0	75.5	2.87	SLT,DOL,SL/SHY,ANHY
+ 59	2717.0-18.0	37.0	19.0	10.6	0.0	55.3	2.84	DOL,SLTY,ANHY
60	2718.0-19.0	0.2	0.2	10.1	0.0	54.7	2.86	DOL,SLTY,ANHY
61	2719.0-20.0	<0.1	<0.1	8.5	0.0	70.1	2.86	DOL,SLTY,ANHY
+ 62	2720.0-21.0	17.0	7.7	15.3	0.0	73.1	2.69	SLT,DOL,SL/SHY,ANHY
63	2721.0-22.0	0.1	<0.1	8.6	0.0	75.9	2.74	SLT,SL/DOL,ANHY
64	2722.0-23.0	0.1	0.1	8.7	0.0	74.5	2.74	SLT,SL/DOL,ANHY
+ 65	2723.0-24.0	8.9	0.2	13.0	0.0	54.7	2.74	SLT,DOL
+ 66	2724.0-25.0	5.6	1.2	14.7	0.0	52.3	2.73	SLT,DOL
+ 67	2725.0-26.0	5.8	4.1	14.9	0.0	54.1	2.73	SLT,DOL
+ 68	2726.0-27.0	26.0	19.0	18.3	0.0	43.6	2.71	SLT,SL/DOL,ANHY
+ 69	2727.0-28.0	17.0	7.4	17.0	0.0	49.0	2.71	SLT,SL/DOL,ANHY
70	2728.0-29.0	0.3	0.3	13.5	0.0	53.9	2.74	SLT,DOL
+ 71	2729.0-30.0	<0.1	<0.1	10.8	0.0	63.9	2.82	SLT,SL/DOL,ANHY
72	2730.0-31.0	0.1	<0.1	8.6	0.0	86.6	2.78	SLT,DOL,CLAY
+ 73	2731.0-32.0	4.3	0.4	15.9	0.0	70.7	2.74	SLT,DOL,CLAY
74	2732.0-33.0	0.4	0.3	10.2	0.0	77.7	2.75	SLT,DOL,CLAY
#+ 75	2733.0-34.0	297.0	291.0	14.8	0.0	75.1	2.80	SLT,SL/DOL,ANHY
#+ 76	2734.0-35.0	112.0	100.0	12.0	0.0	78.6	2.76	SLT,DOL,CLAY
#+ 77	2735.0-36.0	110.0	75.0	15.9	0.0	71.6	2.83	SLT,DOL,ANHY
78	2736.0-37.0	*	0.3	18.0	0.0	65.1	2.78	SLT,DOL,CLAY
	2737.0-38.0							SH,SLTY
79	2738.0-39.0	*	0.3	17.3	0.0	72.5	2.73	SLT,ANHY,CLAY
80	2739.0-40.0	*	0.1	14.6	0.0	84.2	2.79	SLT,SL/DOL,ANHY,CLAY
#+ 81	2740.0-41.0	425.0	225.0	11.5	0.0	73.1	2.77	SLT,DOL,SL/ANHY
+ 82	2741.0-42.0	0.6	<0.1	10.5	0.0	75.4	2.75	SLT,DOL,SL/ANHY
+ 83	2742.0-43.0	6.9	0.2	11.9	0.0	80.2	2.75	SLT,DOL,SL/SHY

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
DALLAS, TEXAS

WAGNER AND BROWN
ROSE NO. 1 WELL

DATE: 5/5/78
FORMATION: CHASE GROUP

FILE NO: 3402-9324
ENGINEER: PUGH

SMP. NO.	DEPTH	PERM. TO AIR MD. MAXIMUM	PERM. TO AIR MD. 90 DEG	POROSITY PERCENT	FLUID SATS. OIL	FLUID SATS. WTR.	GR. DEN.	DESCRIPTION
84	2743.0-44.0	*	0.3	18.6	0.0	65.7	2.68	SLT,SHY,CLAY
85	2744.0-45.0	0.1	<0.1	8.6	0.0	75.1	2.73	SLT,DOL,CLAY
	2745.0-47.0							SH
+ 86	2747.0-48.0	1.3	<0.1	9.2	0.0	80.6	2.75	SLT,DOL,CLAY
87	2748.0-49.0	*	1.0	18.5	0.0	66.0	2.68	SLT,SDY,CLAY
+ 88	2749.0-50.0	0.9	0.6	14.6	0.0	70.7	2.74	SLT,DOL,CLAY
#+ 89	2750.0-51.0	107.0	87.0	19.4	0.0	56.8	2.68	SLT,SL/DOL,SDY,CLAY
+ 90	2751.0-52.0	5.6	0.2	15.8	0.0	63.1	2.74	SLT,DOL,SDY
91	2752.0-53.0	0.1	0.1	17.1	0.0	60.8	2.66	SLT,ANHY,SDY
92	2753.0-54.0	0.1	<0.1	18.2	0.0	54.6	2.68	SLT,SL/DOL,SDY
+ 93	2754.0-55.0	69.0	62.0	22.5	0.0	56.7	2.68	SLT,SDY
+ 94	2755.0-56.0	8.3	6.4	17.2	0.0	58.0	2.70	SLT,SL/DOL,SDY,CLAY
95	2756.0-57.0	0.5	0.4	14.0	0.0	61.9	2.70	SLT,SL/DOL,ANHY,CLAY
+ 96	2757.0-58.0	41.0	9.7	17.8	0.0	58.7	2.68	SLT,SL/DOL,SDY
	2758.0-59.0							SH,SLTY
+ 97	2759.0-60.0	7.6	0.4	12.8	0.0	71.8	2.69	SLT,SL/DOL
98	2760.0-61.0	2.8	2.5	16.9	0.0	65.6	2.69	SLT,SL/DOL,CLAY
+ 99	2761.0-62.0	0.6	0.2	12.9	0.0	70.9	2.71	SLT,DOL,CLAY
+ 100	2762.0-63.0	0.7	0.6	8.6	0.0	80.7	2.66	SLT,SHY,CLAY
+ 101	2763.0-64.0	*	1.0	18.1	0.0	59.9	2.68	SLT,SL/DOL,CLAY
#+102	2764.0-65.0	13.0	2.2	14.8	0.0	68.4	2.71	SLT,SL/DOL,CLAY
#+103	2765.0-66.0	48.0	41.0	13.9	0.0	72.0	2.72	SLT,SL/DOL,CLAY
104	2766.0-67.0	1.0	0.2	16.7	0.0	64.6	2.70	SLT,SL/DOL,CLAY
#+105	2767.0-68.0	*	0.1	15.6	0.0	69.9	2.74	SLT,DOL,SHY
#+106	2768.0-69.0	*	0.1	14.2	0.0	69.8	2.71	SLT,DOL,SHY
107	2769.0-70.0	0.1	<0.1	10.5	0.0	74.8	2.71	SLT,SL/DOL,SHY,ANHY
#+108	2770.0-71.0	111.0	27.0	11.3	0.0	71.9	2.76	SLT,SL/DOL,SHY,ANHY
109	2771.0-72.0	<0.1	<0.1	2.5	0.0	69.0	2.92	SLT,V/ANHY,SHY
110	2772.0-73.0	*	0.1	13.6	0.0	69.9	2.81	SLT,DOL,ANHY,SHY
111	2773.0-74.0	<0.1	<0.1	1.6	0.0	69.8	2.94	SLT,V/ANHY,SHY
112	2774.0-75.0	*	1.1	20.1	0.0	65.8	2.73	SLT,SDY,CLAY
113	2775.0-76.0	*	0.6	19.2	0.0	62.4	2.71	SLT,SDY,CLAY

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114	2776.0-77.0	*	0.2	13.7	0.0	75.3	2.67	SLT,SL/DOL,CLAY
115	2777.0-78.0	<0.1	<0.1	13.3	0.0	76.5	2.72	SLT,SL/DOL,CLAY
+ 116	2778.0-79.0	0.4	0.2	13.9	0.0	72.6	2.74	SLT,DOL,CLAY
+ 117	2779.0-80.0	3.0	2.5	16.0	0.0	67.8	2.73	SLT,DOL,CLAY
+ 118	2780.0-81.0	9.5	6.3	17.6	0.0	62.5	2.72	SLT,SL/DOL,ANHY,CLAY
+ 119	2781.0-82.0	1.7	1.6	15.9	0.0	66.1	2.73	SLT,DOL,CLAY
+ 120	2782.0-83.0	1.6	1.2	15.5	0.0	65.4	2.73	SLT,DOL,CLAY
+ 121	2783.0-84.0	12.0	4.8	18.6	0.0	60.9	2.72	SLT,DOL,CLAY
+ 122	2784.0-85.0	1.5	1.3	16.9	0.0	61.8	2.72	SLT,DOL,CLAY
+ 123	2785.0-86.0	0.4	0.1	16.2	0.0	64.3	2.73	SLT,DOL,CLAY
	2786.0-87.0							SH,SLTY
+ 124	2787.0-88.0	16.0	16.0	17.8	0.0	66.7	2.70	SLT,SL/DOL,CLAY
125	2788.0-89.0	0.2	0.1	9.8	0.0	77.3	2.72	SLT,DOL,CLAY
126	2789.0-90.0	<0.1	<0.1	8.7	0.0	78.6	2.70	SLT,DOL,CLAY
+ 127	2790.0-91.0	0.6	0.5	7.7	0.0	79.3	2.72	SLT,DOL,CLAY
# 128	2791.0-92.0	13.0	8.6	15.4	0.0	69.3	2.69	SLT,SL/DOL,CLAY
	2792.0-94.0							SH,SLTY
+ 129	2794.0-95.0	<0.1	<0.1	13.4	0.0	63.0	2.74	SLT,DOL,CLAY
130	2795.0-96.0	0.1	<0.1	14.0	0.0	58.9	2.72	SLT,DOL,CLAY
131	2796.0-97.0	1.3	1.0	16.3	0.0	50.3	2.71	SLT,DOL,CLAY
132	2797.0-98.0	1.0	0.9	13.9	0.0	58.1	2.77	SLT,DOL,ANHY,CLAY
133	2798.0-99.0	2.9	1.6	14.3	0.0	58.8	2.77	SLT,DOL,ANHY,CLAY
134	2799.0-00.0	0.7	0.6	11.7	0.0	60.2	2.75	SLT,DOL,CLAY
135	2800.0-01.0	0.7	0.6	9.4	0.0	68.6	2.75	SLT,DOL,CLAY
136	2801.0-02.0	1.9	1.6	16.8	0.0	54.3	2.72	SLT,SL/DOL,CLAY
+ 137	2802.0-03.0	17.0	0.9	15.0.	0.0	55.4	2.74	SLT,SL/DOL,ANHY
+ 138	2803.0-04.0	1151.0	822.0	13.6	0.0	72.8	2.68	SLT,SHY,ANHY
139	2804.0-05.0	1.4	1.2	14.0	0.0	55.0	2.85	DOL,SLTY,ANHY
140	2805.0-06.0	3.2	2.7	15.2	0.0	48.8	2.85	SLT,DOL,ANHY
141	2806.0-07.0	0.2	0.2	12.1	0.0	66.7	2.84	DOL,SLTY,ANHY
142	2807.0-08.0	0.3	0.2	14.2	0.0	64.4	2.84	DOL,SLTY,SHY,ANHY
143	2808.0-09.0	<0.1	<0.1	13.4	0.0	67.5	2.84	DOL,SLTY,SHY,ANHY

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144	2809.0-10.0	0.1	<0.1	13.9	0.0	65.8	2.84	DOL,SLTY,SHY,ANHY
145	2810.0-11.0	<0.1	<0.1	10.6	0.0	70.3	2.83	DOL,SLTY,SHY,ANHY
146	2811.0-12.0	<0.1	<0.1	12.1	0.0	67.8	2.86	DOL,SLTY,SL/SHY,PEL
147	2812.0-13.0	<0.1	<0.1	11.0	0.0	69.2	2.85	DOL,SLTY,SL/SHY,PEL
148	2813.0-14.0	0.1	<0.1	9.9	0.0	73.7	2.85	DOL,SLTY,SL/SHY,PEL
149	2814.0-15.0	0.1	<0.1	10.4	0.0	66.6	2.86	DOL,SLTY,PEL,ANHY
150	2815.0-16.0	0.8	0.7	13.4	0.0	59.7	2.86	DOL,SLTY,PEL,ANHY
151	2816.0-17.0	<0.1	<0.1	11.9	0.0	66.6	2.82	DOL,SLTY,SL/SHY,PEL
152	2817.0-18.0	0.4	0.2	11.2	0.0	69.8	2.83	DOL,SLTY,SL/SHY,PEL
153	2818.0-19.0	0.1	0.1	13.9	0.0	66.5	2.83	DOL,SLTY,SL/SHY,PEL
154	2819.0-20.0	*	0.4	14.3	0.0	58.8	2.85	DOL,SLTY,SL/SHY,PEL
155	2820.0-21.0	0.3	0.2	14.7	0.0	56.6	2.85	DOL,SLTY,SL/SHY,PEL
156	2821.0-22.0	0.3	0.2	14.9	0.0	54.5	2.85	DOL,SLTY,PEL,ANHY
157	2822.0-23.0	0.1	<0.1	13.7	0.0	60.3	2.84	DOL,SLTY,PEL,ANHY
158	2823.0-24.0	0.4	0.3	13.4	0.0	61.7	2.86	DOL,SLTY,PEL,ANHY
159	2824.0-25.0	0.5	0.4	15.5	0.0	51.4	2.83	DOL,SLTY,PEL,ANHY
160	2825.0-26.0	2.1	1.7	17.9	0.0	49.2	2.84	DOL,SLTY,PEL,ANHY
161	2826.0-27.0	*	0.3	15.9	0.0	50.2	2.89	DOL,SLTY,PEL,ANHY
162	2827.0-28.0	6.2	5.0	13.9	0.0	53.1	2.86	DOL,SLTY,PEL,ANHY
163	2828.0-29.0	12.0	10.0	15.3	0.0	49.9	2.86	DOL,SLTY,PEL,ANHY
164	2829.0-30.0	5.2	4.0	14.5	0.0	49.8	2.86	DOL,SLTY,PEL,ANHY
165	2830.0-31.0	22.0	20.0	18.1	0.0	41.0	2.85	DOL,SLTY,PEL,ANHY
166	2831.0-32.0	9.3	8.2	14.2	0.0	48.8	2.86	DOL,SLTY,PEL,ANHY
167	2832.0-33.0	11.0	10.0	15.2	0.0	51.9	2.85	DOL,SLTY,PEL,ANHY
168	2833.0-34.0	8.3	6.9	14.5	0.0	58.7	2.85	DOL,SLTY,PEL,ANHY
169	2834.0-35.0	2.4	1.9	14.1	0.0	54.9	2.86	DOL,SLTY,PEL,ANHY
170	2835.0-36.0	1.5	1.3	13.0	0.0	55.1	2.85	DOL,SLTY,PEL,ANHY
171	2836.0-37.0	2.6	2.3	12.9	0.0	55.1	2.87	DOL,SLTY,PEL,ANHY
172	2837.0-38.0	4.2	3.6	13.6	0.0	59.6	2.86	DOL,SLTY,ANHY
173	2838.0-39.0	5.7	4.6	16.7	0.0	68.3	2.85	DOL,SLTY,ANHY
174	2839.0-40.0	9.8	8.0	18.7	0.0	65.9	2.86	DOL,SLTY,ANHY
175	2840.0-41.0	0.3	0.2	16.2	0.0	64.2	2.83	SLT,DOL,SL/SHY,ANHY

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	2841.0-42.0	*	0.1	14.5	0.0	80.6	2.69	SLT, SHY, SL/DOL
176	2842.0-43.0	0.1	<0.1	12.4	0.0	75.6	2.71	SLT, DOL, ANHY
# 177	2843.0-44.0	2.5	2.3	19.6	0.0	66.5	2.70	SLT, SL/DOL, ANHY
178	2844.0-45.0	2.2	1.8	18.3	0.0	65.9	2.70	SLT, SL/DOL, ANHY
179	2845.0-46.0	6.3	5.3	21.0	0.0	60.9	2.70	SLT, SL/DOL, ANHY
180	2846.0-47.0	9.3	8.1	22.3	0.0	58.0	2.70	SLT, SL/DOL, ANHY
181	2847.0-48.0	7.9	6.5	20.2	0.0	60.6	2.72	SLT, DOL, ANHY
182	2848.0-49.0	0.8	0.6	12.6	0.0	70.4	2.75	SLT, DOL, ANHY
183	2849.0-50.0	13.0	12.0	21.3	0.0	61.2	2.71	SLT, SL/DOL
184	2850.0-51.0	6.1	5.1	20.3	0.0	62.3	2.63	SLT, SL/DOL
185	2851.0-52.0	4.2	3.1	19.7	0.0	63.1	2.72	SLT, SL/DOL
186	2852.0-53.0	1.2	1.1	17.2	0.0	66.9	2.72	SLT, SL/DOL
187	2853.0-54.0	14.0	12.0	16.5	0.0	68.5	2.73	SLT, SL/DOL
+ 188	2854.0-55.0	11.0	4.2	15.3	0.0	73.1	2.70	SLT, SL/DOL
#+189	2855.0-62.0							SH
190	2862.0-63.0	<0.1	<0.1	10.4	0.0	79.6	2.74	SLT, DOL
191	2863.0-64.0	<0.1	<0.1	10.1	0.0	75.2	2.71	SLT, DOL
192	2864.0-65.0	<0.1	<0.1	11.6	0.0	73.5	2.71	SLT, DOL
193	2865.0-66.0	0.6	0.5	15.7	0.0	67.0	2.74	SLT, SL/DOL, ANHY
194	2866.0-67.0	0.2	0.1	15.5	0.0	65.2	2.75	SLT, SL/DOL, ANHY
	2867.0-79.0							SH
195	2879.0-80.0	0.1	<0.1	19.4	0.0	59.2	2.84	SLT, DOL, ANHY
196	2880.0-81.0	<0.1	<0.1	21.7	0.0	66.2	2.83	SLT, DOL, ANHY
197	2881.0-82.0	0.1	0.1	17.5	0.0	63.5	2.79	SLT, DOL, ANHY
198	2882.0-83.0	<0.1	<0.1	5.7	0.0	74.6	2.74	LM, SLTY, SH STKS
199	2883.0-84.0	<0.1	<0.1	6.0	0.0	71.8	2.79	LM, SLTY, ANHY
200	2884.0-85.0	<0.1	<0.1	6.8	0.0	70.9	2.76	LM, SLTY, ANHY
201	2885.0-86.0	2.0	0.8	15.2	0.0	65.1	2.78	SLT, DOL
202	2886.0-87.0	0.8	0.8	15.8	0.0	60.4	2.80	SLT, DOL, ANHY
203	2887.0-88.0	0.1	<0.1	15.1	0.0	64.7	2.80	SLT, DOL, ANHY
204	2888.0-89.0	<0.1	<0.1	11.3	0.0	63.5	2.77	SLT, DOL, SL/LMY, ANHY
	2889.0-96.0							SH

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#+205	2896.0-97.0	24.0	<0.1	10.8	0.0	66.5	2.70	SLT,SL/DOL,ANHY,CLAY
+ 206	2897.0-98.0	3.2	<0.1	9.5	0.0	75.7	2.72	SLT,SL/DOL,CLAY
207	2898.0-99.0	0.1	0.1	10.0	0.0	73.2	2.72	SLT,SL/DOL,CLAY
208	2899.0-00.0	0.1	<0.1	10.8	0.0	71.1	2.73	SLT,SL/DOL,CLAY
209	2900.0-01.0	1443.0	0.1	12.2	0.0	67.8	2.76	SLT,SL/DOL,ANHY,CLAY
210	2901.0-02.0	0.1	0.1	13.8	0.0	63.2	2.71	SLT,SL/DOL,CLAY
211	2902.0-03.0	1.0	0.9	17.6	0.0	57.6	2.71	SLT,SL/DOL,CLAY
212	2903.0-04.0	0.6	0.5	16.9	0.0	61.9	2.71	SLT,SL/DOL,ANHY,CLAY
213	2904.0-05.0	6.6	5.5	21.1	0.0	54.9	2.71	SLT,SL/DOL,CLAY
214	2905.0-06.0	6.2	6.2	20.8	0.0	52.8	2.70	SLT,SL/DOL,CLAY
215	2906.0-07.0	6.0	6.0	20.9	0.0	56.3	2.70	SLT,SL/DOL,ANHY,CLAY
+ 216	2907.0-08.0	26.0	24.0	22.4	0.0	51.5	2.72	SLT,SL/DOL,ANHY,CLAY
217	2908.0-09.0	16.0	12.0	20.0	0.0	54.6	2.74	SLT,SL/DOL,ANHY,CLAY
218	2909.0-10.0	7.9	7.9	22.4	0.0	50.9	2.72	SLT,SL/DOL,ANHY,CLAY
219	2910.0-11.0	13.0	9.7	23.7	0.0	51.6	2.71	SLT,SL/DOL,ANHY,CLAY
220	2911.0-12.0	10.0	9.7	20.3	0.0	57.5	2.71	SLT,SL/DOL,ANHY,CLAY
221	2912.0-13.0	*	12.0	19.0	0.0	60.7	2.71	SLT,SL/DOL,ANHY,CLAY
222	2913.0-14.0	*	20.0	20.2	0.0	56.9	2.71	SLT,SL/DOL,ANHY,CLAY
223	2914.0-15.0	2.6	1.9	18.3	0.0	61.5	2.72	SLT,SL/DOL,ANHY,CLAY
224	2915.0-16.0	2.1	2.0	18.9	0.0	63.2	2.72	SLT,SL/DOL,CLAY
225	2916.0-17.0	1.1	0.8	17.1	0.0	65.5	2.72	SLT,SL/DOL,CLAY
#+226	2917.0-18.0	138.0	0.4	13.1	0.0	71.8	2.72	SLT,SL/DOL,CLAY
227	2918.0-19.0	*	0.3	12.7	0.0	73.0	2.66	SLT,SL/DOL,SHY
228	2919.0-20.0	0.1	0.1	11.7	0.0	74.0	2.71	SLT,DOL
	2920.0-25.0							SH
229	2925.0-26.0	1.0	0.7	13.9	0.0	68.2	2.73	LM,SL/DOL,SLTY
230	2926.0-27.0	0.7	0.5	13.8	0.0	66.4	2.73	LM,SLTY
231	2927.0-28.0	0.4	0.4	12.8	0.0	66.3	2.72	LM,SLTY
232	2928.0-29.0	<0.1	<0.1	12.1	0.0	73.8	2.82	DOL,SLT STKS,FOSS
233	2929.0-30.0	0.5	0.2	10.9	0.0	61.6	2.74	LM,SLTY,ANHY
234	2930.0-31.0	1.2	1.1	12.5	0.0	66.5	2.76	LM,SLTY
235	2931.0-32.0	0.9	0.8	13.8	0.0	64.7	2.74	LM,SLTY,SH STKS

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236	2932.0-33.0	0.5	0.4	12.8	0.0	65.0	2.73	LM, SLTY
237	2933.0-34.0	0.7	0.6	12.6	0.0	63.1	2.74	LM, SLTY
238	2934.0-35.0	0.5	0.5	9.3	0.0	62.0	2.75	LM, SL/SLTY
239	2935.0-36.0	0.1	0.1	5.5	0.0	75.8	2.81	LM, SL/SLTY, FOSS
240	2936.0-37.0	0.1	0.1	9.4	0.0	68.8	2.73	LM, SLTY, SH STKS, FOSS
241	2937.0-38.0	<0.1	<0.1	5.9	0.0	73.1	2.77	LM, SLTY, FOSS, ANHY
	2938.0-40.0							SH
242	2940.0-41.0	<0.1	<0.1	8.2	0.0	69.5	2.71	LM, SLTY, FOSS
243	2941.0-42.0	0.7	0.7	10.4	0.0	61.1	2.72	LM, SLTY, FOSS
244	2942.0-43.0	0.6	0.6	12.0	0.0	63.1	2.73	LM, SLTY, FOSS
245	2943.0-44.0	0.6	0.5	11.4	0.0	59.1	2.72	LM, SLTY, FOSS
246	2944.0-45.0	<0.1	<0.1	6.1	0.0	76.8	2.73	LM, SHY, SLTY, FOSS, PEL
247	2945.0-46.0	<0.1	<0.1	6.7	0.0	72.1	2.72	LM, SL/DOL, SLT STKS
248	2946.0-47.0	<0.1	<0.1	4.3	0.0	79.0	2.70	LM, SLT STKS
# 249	2947.0-48.0	6.7	6.3	11.5	0.0	69.6	2.77	SLT, DOL, ANHY
#+250	2948.0-49.0	*	0.1	8.0	0.0	77.9	2.73	SLT, LMY
	2949.0-57.0							SH
251	2957.0-58.0	0.3	0.2	12.3	0.0	71.3	2.73	SLT, DOL, ANHY, CLAY
252	2958.0-59.0	0.2	0.2	12.4	0.0	61.7	2.69	SLT, DOL, CLAY
253	2959.0-60.0	1.1	0.3	14.0	0.0	57.1	2.69	SLT, DOL, CLAY
254	2960.0-61.0	0.4	0.3	13.7	0.0	65.1	2.70	SLT, DOL, CLAY
255	2961.0-62.0	0.3	0.3	13.5	0.0	64.5	2.69	SLT, DOL, CLAY
256	2962.0-63.0	0.2	0.1	11.0	0.0	69.1	2.69	SLT, DOL, CLAY
257	2963.0-64.0	0.9	0.7	14.4	0.0	61.0	2.70	SLT, DOL, CLAY
258	2964.0-65.0	0.3	0.2	15.6	0.0	62.5	2.72	SLT, DOL, CLAY
259	2965.0-66.0	0.1	0.1	12.2	0.0	68.3	2.69	SLT, DOL, CLAY
# 260	2966.0-67.0	12.0	1.3	11.9	0.0	71.0	2.69	SLT, DOL
	2967.0-71.0							SH
261	2971.0-72.0	0.5	0.4	9.4	0.0	73.5	2.78	LM, SLTY, ANHY
262	2972.0-73.0	0.2	0.1	4.9	0.0	80.9	2.72	LM, SLTY, FOSS
+ 263	2973.0-74.0	103.0	7.5	5.9	0.0	78.8	2.77	LM, SLTY, ANHY
264	2974.0-75.0	1.8	1.8	15.5	0.0	66.6	2.80	LM, SLTY, ANHY

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265	2975.0-76.0	2.2	2.1	17.0	0.0	70.2	2.79	LM, SLTY
266	2976.0-77.0	0.1	0.1	12.9	0.0	72.3	2.77	LM, SLTY, ANHY
267	2977.0-78.0	0.1	0.1	15.7	0.0	62.0	2.78	LM, SL/DOL, SLTY SH
	2978.0-82.0							
268	2982.0-83.0	<0.1	<0.1	8.5	0.0	72.5	2.71	SLT, DOL, ANHY, CLAY
269	2983.0-84.0	<0.1	<0.1	6.0	0.0	81.9	2.71	SLT, DOL, CLAY
270	2984.0-85.0	<0.1	<0.1	16.3	0.0	62.3	2.81	SLT, DOL, ANHY, CLAY
271	2985.0-86.0	<0.1	<0.1	15.2	0.0	64.5	2.80	SLT, DOL, ANHY, CLAY SH
	2986.0-92.0							
272	2992.0-93.0	<0.1	<0.1	5.1	0.0	79.1	2.68	SLT, LMY, ANHY, CLAY
273	2993.0-94.0	<0.1	<0.1	4.9	0.0	83.6	2.69	SLT, LMY, ANHY, CLAY
# 274	2994.0-95.0	0.1	0.1	6.0	0.0	77.9	2.71	SLT, LMY, ANHY, CLAY SH, SLTY
	2995.0-05.0							
275	3005.0-06.0	<0.1	<0.1	10.7	0.0	69.7	2.74	SLT, DOL, ANHY
	3006.0-15.0							SLT, SHY, ANHY, CLAY SH
	3015.0-16.0							
	3016.0-23.0							SLT, DOL, ANHY, CLAY SH
	3023.0-25.0							
	3025.0-3092.0	DRILLED						
	3092.0-02.0							SH, SLTY, SL/LMY
276	3102.0-03.0	0.5	0.4	10.7	0.0	72.4	2.73	LM, SLTY, ANHY
277	3103.0-04.0	<0.1	<0.1	6.2	0.0	82.0	2.74	LM, SLTY, ANHY
278	3104.0-05.0	<0.1	<0.1	5.7	0.0	86.9	2.70	LM, SLTY, ANHY
279	3105.0-06.0	0.1	<0.1	7.4	0.0	79.2	2.70	LM, SLTY, ANHY
280	3106.0-07.0	0.1	0.1	12.0	0.0	71.0	2.70	LM, SL/DOL, SLTY, ANHY
281	3107.0-08.0	0.1	<0.1	10.2	0.0	71.2	2.71	LM, SL/DOL, SLTY, ANHY
+ 282	3108.0-09.0	2.0	0.7	12.2	0.0	70.3	2.72	LM, SL/DOL, SLTY, ANHY
283	3109.0-10.0	0.1	<0.1	13.3	0.0	70.5	2.73	LM, SL/DOL, SLTY, ANHY
284	3110.0-11.0	0.1	<0.1	11.4	0.0	72.7	2.74	DOL, SL/LMY, SLTY, ANHY
285	3111.0-12.0	0.1	0.1	13.6	0.0	68.4	2.78	DOL, SLTY, ANHY

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286	3112.0-13.0	0.5	0.5	16.7	0.0	75.4	2.78	DOL,SLTY,ANHY
287	3113.0-14.0	0.1	0.1	16.9	0.0	75.5	2.77	SLT,DOL,ANHY
288	3114.0-15.0	0.2	0.2	17.3	0.0	77.1	2.77	SLT,DOL,ANHY
289	3115.0-16.0	0.6	0.4	18.3	0.0	74.3	2.75	SLT,DOL,ANHY
290	3116.0-17.0	<0.1	<0.1	16.2	0.0	74.3	2.77	SLT,DOL,ANHY
291	3117.0-18.0	0.8	0.1	14.7	0.0	71.1	2.76	SLT,DOL,ANHY
292	3118.0-19.0	<0.1	<0.1	9.8	0.0	73.3	2.72	SLT,DOL,ANHY
293	3119.0-20.0	<0.1	<0.1	8.4	0.0	74.9	2.71	SLT,DOL,SL/LMY,ANHY
+ 294	3120.0-21.0	5.7	<0.1	7.9	0.0	76.0	2.70	SLT,DOL,SL/LMY,ANHY
295	3121.0-22.0	<0.1	<0.1	6.9	0.0	75.8	2.69	SLT,LMY,SL/DOL
+ 296	3122.0-23.0	16.0	0.1	5.9	0.0	79.3	2.70	SLT,LMY,SL/DOL
+ 297	3123.0-24.0	5.0	<0.1	4.8	0.0	81.8	2.67	SLT,LMY
+ 298	3124.0-25.0	4.6	<0.1	6.1	0.0	80.6	2.68	SLT,LMY
299	3125.0-26.0	<0.1	<0.1	6.0	0.0	79.4	2.70	SLT,LMY
# 300	3126.0-27.0	1.3	1.2	6.2	0.0	79.0	2.71	SLT,LMY
#+301	3127.0-28.0	7.9	6.1	6.9	0.0	78.3	2.73	SLT,LMY
	3128.0-34.0							SH
302	3134.0-35.0	0.1	0.1	10.6	0.0	63.4	2.70	LM,SLTY
303	3135.0-36.0	0.2	0.2	9.9	0.0	73.1	2.69	LM,SLTY,ANHY
+ 304	3136.0-37.0	0.4	0.4	8.6	0.0	69.6	2.73	LM,SLTY,ANHY
305	3137.0-38.0	0.1	<0.1	7.3	0.0	69.7	2.72	LM,SLTY,SHY,PEL,ANHY
	3138.0-42.0							SH
+ 306	3142.0-43.0	0.9	0.6	6.5	0.0	72.2	2.73	LM,SLTY,FOSS,ANHY
+ 307	3143.0-44.0	4.2	0.3	11.3	0.0	68.5	2.73	LM,SLTY,FOSS,ANHY
308	3144.0-45.0	0.6	0.5	10.9	0.0	69.0	2.74	LM,SLTY,ANHY
309	3145.0-46.0	0.4	0.3	11.8	0.0	66.1	2.75	LM,SLTY,ANHY
310	3146.0-47.0	0.2	0.1	8.9	0.0	71.0	2.72	LM,SLTY
311	3147.0-48.0	0.2	0.2	9.0	0.0	71.7	2.72	LM,SLTY
312	3148.0-49.0	0.2	0.1	9.5	0.0	70.9	2.72	LM,SLTY,ANHY
313	3149.0-50.0	0.1	0.1	7.1	0.0	74.0	2.74	LM,SLTY,SL/SHY,ANHY
+ 314	3150.0-51.0	14.0	0.4	8.4	0.0	70.0	2.72	LM,SLT STKS,ANHY
315	3151.0-52.0	6.7	0.1	10.2	0.0	69.1	2.72	LM,SLT STKS

\+ DENOTES HORIZONTAL CRACKS
\# DENOTES CHAOTIC FISSURES

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
DALLAS, TEXAS

CORE SUMMARY

Company WAGNER AND BROWN
Well ROSE NO. 1
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DEPTH FEET	HORIZONTAL PERMEABILITY, Md. MAXIMUM	90 DEGREES	POROSITY PER CENT	SATURATION OIL	WATER	GRAIN DENSITY
2647.0-50.0	43	16	15.4	0.0	67.3	2.72
2651.0-59.0	198	160	16.5	0.0	68.1	2.72
2659.0-64.0	1.7	0.1	6.6	0.0	71.7	2.80
2664.0-69.0	14	13	17.3	0.0	47.2	2.73
2669.0-72.0	0.3	0.2	9.9	0.0	47.9	2.74
2672.0-74.0	27	17	12.7	0.0	55.7	2.80
2678.0-80.0	12	0.4	11.2	0.0	67.2	2.72
2682.0-85.0	74	44	11.6	0.0	71.1	2.71
2686.0-01.0	19	6.2	12.8	0.0	69.8	2.71
2704.0-08.0	25	13	13.6	0.0	69.5	2.67
2708.0-17.0	0.4	0.4	11.6	0.0	62.3	2.81
2717.0-20.0	12	6.4	9.7	0.0	60.0	2.85
2720.0-58.0	42	26	14.5	0.0	66.7	2.73
2759.0-06.0	39	22	13.8	0.0	66.5	2.74
2806.0-40.0	3.3	2.7	13.9	0.0	59.7	2.85
2840.0-55.0	5.6	4.2	17.8	0.0	66.5	2.71

CORE SUMMARY

Company WAGNER AND BROWN
Well ROSE NO. 1
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DEPTH FEET	HORIZONTAL PERMEABILITY, Md. MAXIMUM	90 DEGREES	POROSITY PER CENT	SATURATION OIL	WATER	GRAIN DENSITY
2862.0-67.0	0.2	0.1	12.7	0.0	72.1	2.73
2879.0-82.0	0.1	<0.1	19.5	0.0	63.0	2.82
2882.0-85.0	<0.1	<0.1	6.2	0.0	72.4	2.76
2885.0-89.0	0.7	0.4	14.4	0.0	63.4	2.79
2896.0-20.0	81	5.0	16.8	0.0	62.2	2.71
2925.0-47.0	0.4	0.4	10.2	0.0	67.8	2.74
2947.0-49.0	6.7	3.2	9.8	0.0	73.8	2.75
2957.0-67.0	1.6	0.4	13.1	0.0	66.2	2.70
2971.0-78.0	15	1.7	11.6	0.0	72.0	2.77
2982.0-86.0	<0.1	<0.1	11.5	0.0	70.3	2.76
2992.0-06.0	<0.1	<0.1	6.7	0.0	77.6	2.71
3102.0-13.0	0.3	0.2	10.9	0.0	74.5	2.73
3113.0-28.0	2.8	0.6	10.2	0.0	76.7	2.72
3134.0-38.0	0.2	0.2	9.1	0.0	69.0	2.71
3142.0-52.0	2.8	0.3	9.4	0.0	70.3	2.73