

CONFIDENTIAL

ORIGINAL

19-21-38W

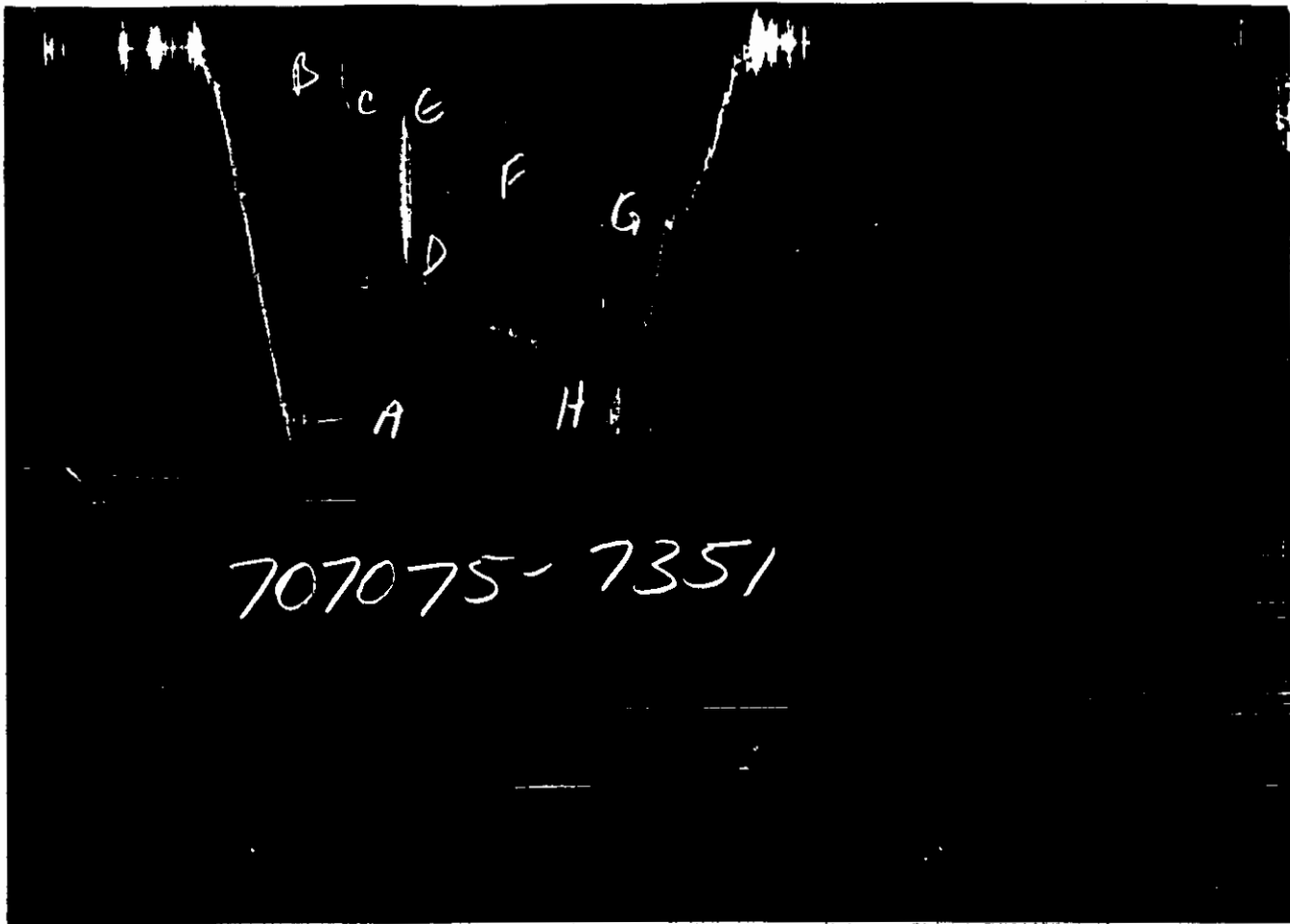
| | |
|--------------------------|--------|
| AMOCO PRODUCTION COMPANY | |
| LEASE : WYATT "E" | NCC |
| WELL NO. : 1-19 | JUL 20 |
| TEST NO. : 1 | COM |
| API # 15-093-21455 | |

TICKET NO. 70707500
 26-JUN-95
 LIBERAL

RELEASED
 APR 6 1998
 FROM CONFIDENTIAL

Computer inventoried

| | | | | | | | |
|------------------------------|------------------|----------|--------|----------|-----------------|--------------------------|--------------------------|
| LEGAL LOCATION LEASE NAME | 1-19 | WELL NO. | 1 | TEST NO. | 5136.0 - 5247.0 | TESTED INTERVAL | AMOCO PRODUCTION COMPANY |
| FIELD FRBR | 19 - 21 S - 38 W | COUNTY | KEARNY | STATE | KANSAS | LEASE OWNER/COMPANY NAME | |



707075-7351

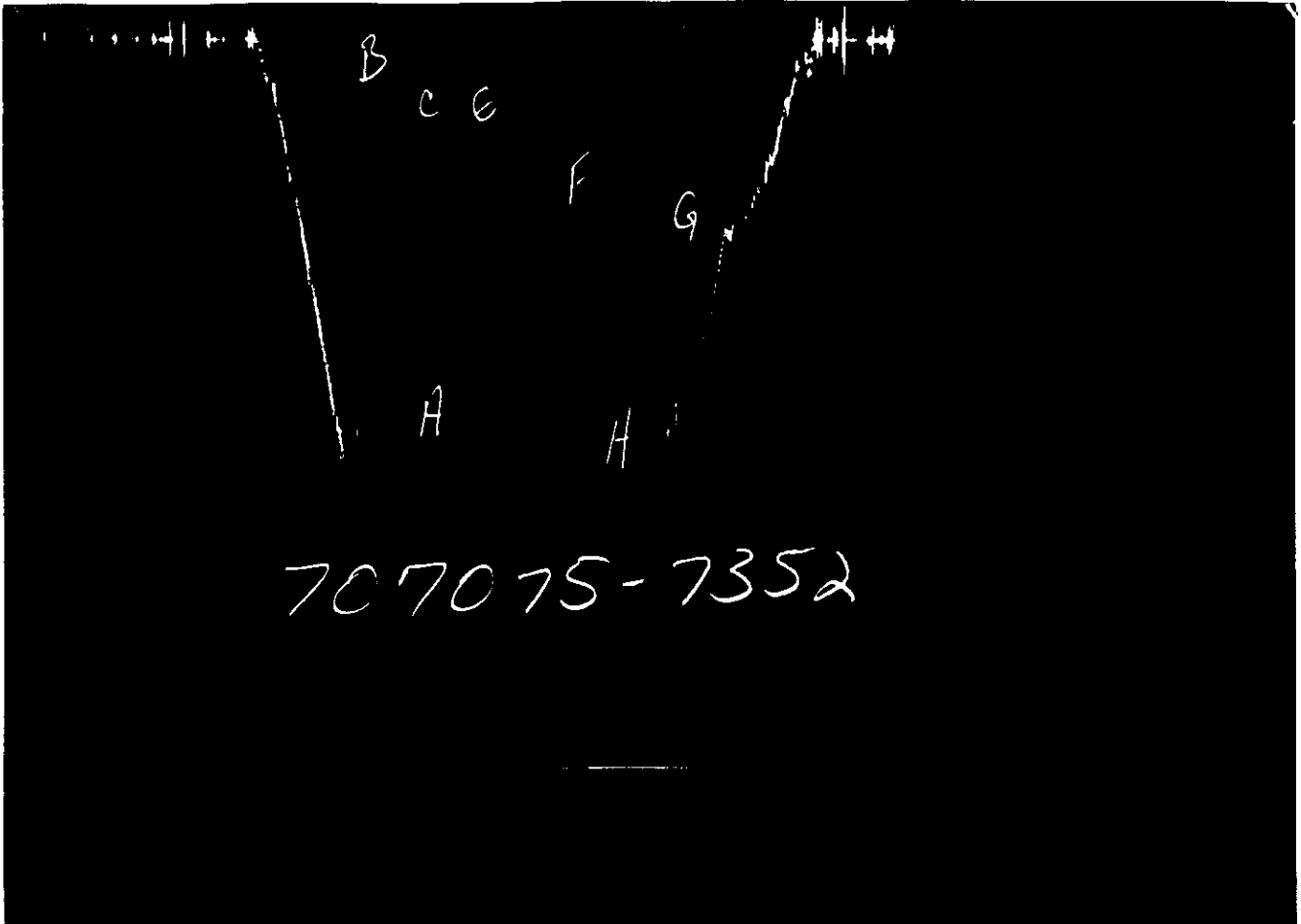
GAUGE NO: 7351 DEPTH: 5123.0 BLANKED OFF: NO HOUR OF CLOCK: 24

| ID | DESCRIPTION | PRESSURE | | TIME | | TYPE |
|----|--------------------------|----------|------------|----------|------------|------|
| | | REPORTED | CALCULATED | REPORTED | CALCULATED | |
| A | INITIAL HYDROSTATIC | 2402 | 2351.9 | | | |
| B | INITIAL FIRST FLOW | | 142.7 | | | |
| C | FINAL FIRST FLOW | | 452.0 | 11.0 | 11.2 | F |
| C | INITIAL FIRST CLOSED-IN | | 452.0 | | | |
| D | FINAL FIRST CLOSED-IN | | 1173.5 | 61.0 | 60.8 | C |
| E | INITIAL SECOND FLOW | | 488.1 | | | |
| F | FINAL SECOND FLOW | | 1066.7 | 121.0 | 121.4 | F |
| F | INITIAL SECOND CLOSED-IN | | 1066.7 | | | |
| G | FINAL SECOND CLOSED-IN | | 1150.3 | 119.0 | 118.6 | C |
| H | FINAL HYDROSTATIC | 2305 | 2376.1 | | | |

1-11-1980

OPERATED

...



GAUGE NO: 7352 DEPTH: 5242.0 BLANKED OFF: YES HOUR OF CLOCK: 24

| ID | DESCRIPTION | PRESSURE | | TIME | | TYPE |
|----|--------------------------|----------|------------|----------|------------|------|
| | | REPORTED | CALCULATED | REPORTED | CALCULATED | |
| A | INITIAL HYDROSTATIC | 2400 | 2403.1 | | | |
| B | INITIAL FIRST FLOW | 155 | 193.2 | | | |
| C | FINAL FIRST FLOW | 528 | 503.0 | 11.0 | 11.2 | F |
| C | INITIAL FIRST CLOSED-IN | 528 | 503.0 | | | |
| D | FINAL FIRST CLOSED-IN | 1245 | 1227.2 | 61.0 | 60.8 | C |
| E | INITIAL SECOND FLOW | 599 | 543.5 | | | |
| F | FINAL SECOND FLOW | 1182 | 1118.7 | 121.0 | 121.4 | F |
| F | INITIAL SECOND CLOSED-IN | 1182 | 1118.7 | | | |
| G | FINAL SECOND CLOSED-IN | 1213 | 1204.4 | 119.0 | 118.6 | C |
| H | FINAL HYDROSTATIC | 2368 | 2427.3 | | | |

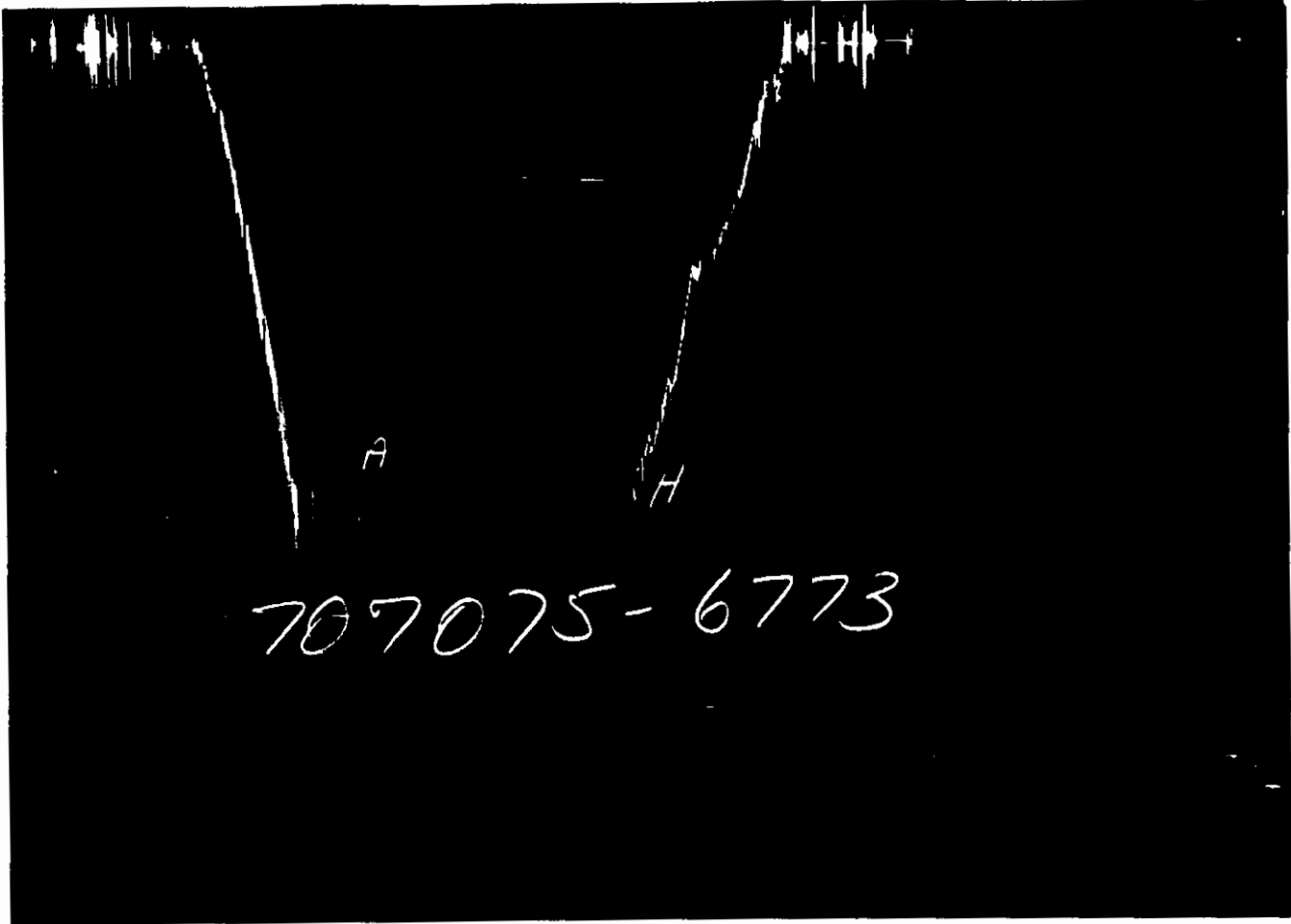
RELEASED

APR 6 1998

ORIGINAL

CONFIDENTIAL

FROM CONFIDENTIAL



GAUGE NO: 6773 DEPTH: 5445.0 BLANKED OFF: YES HOUR OF CLOCK: 24

| ID | DESCRIPTION | PRESSURE | | TIME | | TYPE |
|----|--------------------------|----------|------------|----------|------------|------|
| | | REPORTED | CALCULATED | REPORTED | CALCULATED | |
| A | INITIAL HYDROSTATIC | 2538 | 2501.2 | | | |
| B | INITIAL FIRST FLOW | | | 11.0 | | F |
| C | FINAL FIRST FLOW | | | | | |
| C | INITIAL FIRST CLOSED-IN | | | 61.0 | | C |
| D | FINAL FIRST CLOSED-IN | | | | | |
| E | INITIAL SECOND FLOW | | | 121.0 | | F |
| F | FINAL SECOND FLOW | | | | | |
| F | INITIAL SECOND CLOSED-IN | | | 119.0 | | C |
| G | FINAL SECOND CLOSED-IN | | | | | |
| H | FINAL HYDROSTATIC | 2538 | 2527.5 | | | |

EQUIPMENT & HOLE DATA

FORMATION TESTED: MORROW
 NET PAY (ft): 61.0
 GROSS TESTED FOOTAGE: 111.0 PKR. TO PKR.
 ALL DEPTHS MEASURED FROM: K.B.
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.875
 ELEVATION (ft): _____
 TOTAL DEPTH (ft): 5448.0
 PACKER DEPTH(S) (ft): 5136. 5247
 FINAL SURFACE CHOKE (in): 0.25000 (B. HOSE)
 BOTTOM HOLE CHOKE (in): 0.750
 MUD WEIGHT (lb/gal): 9.10
 MUD VISCOSITY (sec): 50
 ESTIMATED HOLE TEMP. (°F): 125
 ACTUAL HOLE TEMP. (°F): @ _____ ft

TICKET NUMBER: 70707500

DATE: 06-21-95 TEST NO: 1

TYPE DST: ON BTM. STRADDLE

FIELD CAMP: _____
LIBERAL

TESTER: _____
ARMSTRONG

WITNESS: _____
BILL CHATHAM

DRILLING CONTRACTOR: _____
CHEYENNE DRILLING RIG #3

FLUID PROPERTIES FOR RECOVERED MUD & WATER

| SOURCE | RESISTIVITY | CHLORIDES |
|---------------|----------------------|------------------|
| <u>PII</u> | <u>0.470 @ 80 °F</u> | <u>8354 ppm</u> |
| <u>TOP</u> | <u>0.200 @ 80 °F</u> | <u>18796 ppm</u> |
| <u>MIDDLE</u> | <u>0.130 @ 80 °F</u> | <u>33416 ppm</u> |
| <u>BOTTOM</u> | <u>0.120 @ 80 °F</u> | <u>37053 ppm</u> |
| _____ | _____ @ _____ °F | _____ ppm |
| _____ | _____ @ _____ °F | _____ ppm |

SAMPLER DATA

P_{sig} AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ @ _____ °F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

| TYPE | AMOUNT | WEIGHT |
|-------|--------|--------|
| _____ | _____ | _____ |
| _____ | _____ | _____ |

RECOVERED :

488 FT OF DRILLING MUD
 1962 FT OF SALTWATER
 6 FT OF SAND

MEASURED FROM
TESTER VALVE

REMARKS :

TICKET NO: 70707500

GAUGE NO: 7351

CLOCK NO: 17524 HOUR: 24

DEPTH: 5123.0

| REF | MINUTES | PRESSURE | AP | $\frac{t \times \Delta t}{t + \Delta t}$ | $\log \frac{t + \Delta t}{\Delta t}$ |
|-----------------|---------|----------|-------|--|--------------------------------------|
| FIRST FLOW | | | | | |
| B 1 | 0.0 | 142.7 | | | |
| 2 | 1.0 | 248.2 | 105.5 | | |
| 3 | 2.0 | 289.2 | 41.0 | | |
| 4 | 3.0 | 310.0 | 20.8 | | |
| 5 | 4.0 | 326.9 | 16.9 | | |
| 6 | 5.0 | 347.9 | 21.0 | | |
| 7 | 6.0 | 366.5 | 18.6 | | |
| 8 | 7.0 | 383.3 | 16.9 | | |
| 9 | 8.0 | 400.5 | 17.2 | | |
| 10 | 9.0 | 416.8 | 16.2 | | |
| 11 | 10.0 | 434.1 | 17.4 | | |
| C 12 | 11.2 | 452.0 | 17.8 | | |
| FIRST CLOSED-IN | | | | | |
| C 1 | 0.0 | 452.0 | | | |
| 2 | 1.0 | 953.9 | 501.9 | 0.9 | 1.085 |
| 3 | 2.0 | 995.4 | 543.5 | 1.7 | 0.824 |
| 4 | 3.0 | 1023.1 | 571.2 | 2.4 | 0.674 |
| 5 | 4.0 | 1042.9 | 591.0 | 3.0 | 0.579 |
| 6 | 5.0 | 1054.1 | 602.2 | 3.4 | 0.511 |
| 7 | 6.0 | 1067.1 | 615.2 | 3.9 | 0.458 |
| 8 | 7.0 | 1076.5 | 624.5 | 4.3 | 0.414 |
| 9 | 8.0 | 1085.2 | 633.2 | 4.7 | 0.378 |
| 10 | 9.0 | 1090.9 | 639.0 | 5.0 | 0.352 |
| 11 | 10.0 | 1097.8 | 645.9 | 5.3 | 0.326 |
| 12 | 12.0 | 1107.4 | 655.5 | 5.8 | 0.286 |
| 13 | 14.0 | 1115.6 | 663.6 | 6.2 | 0.255 |
| 14 | 16.0 | 1122.3 | 670.4 | 6.6 | 0.230 |
| 15 | 18.0 | 1127.8 | 675.8 | 6.9 | 0.209 |
| 16 | 20.0 | 1131.9 | 680.0 | 7.2 | 0.193 |
| 17 | 22.0 | 1136.4 | 684.4 | 7.4 | 0.179 |
| 18 | 24.0 | 1140.6 | 688.6 | 7.6 | 0.166 |
| 19 | 26.0 | 1143.8 | 691.8 | 7.8 | 0.155 |
| 20 | 28.0 | 1147.0 | 695.0 | 8.0 | 0.146 |
| 21 | 30.0 | 1150.2 | 698.2 | 8.1 | 0.137 |
| 22 | 35.0 | 1155.8 | 703.8 | 8.5 | 0.121 |
| 23 | 40.0 | 1160.7 | 708.8 | 8.7 | 0.107 |
| 24 | 45.0 | 1164.6 | 712.6 | 9.0 | 0.096 |
| 25 | 50.0 | 1167.9 | 716.0 | 9.1 | 0.088 |
| 26 | 55.0 | 1170.8 | 718.9 | 9.3 | 0.080 |
| D 27 | 60.8 | 1173.5 | 721.6 | 9.4 | 0.073 |
| SECOND FLOW | | | | | |
| E 1 | 0.0 | 488.1 | | | |
| 2 | 1.0 | 500.5 | 12.4 | | |
| 3 | 2.0 | 515.8 | 15.3 | | |
| 4 | 3.0 | 534.0 | 18.2 | | |
| 5 | 4.0 | 551.2 | 17.2 | | |

| REF | MINUTES | PRESSURE | AP | $\frac{t \times \Delta t}{t + \Delta t}$ | $\log \frac{t + \Delta t}{\Delta t}$ |
|-------------------------|---------|----------|------|--|--------------------------------------|
| SECOND FLOW - CONTINUED | | | | | |
| 6 | 5.0 | 566.8 | 15.6 | | |
| 7 | 6.0 | 583.6 | 16.7 | | |
| 8 | 7.0 | 598.6 | 15.0 | | |
| 9 | 8.0 | 612.3 | 13.7 | | |
| 10 | 9.0 | 626.5 | 14.2 | | |
| 11 | 10.0 | 639.6 | 13.1 | | |
| 12 | 12.0 | 666.7 | 27.1 | | |
| 13 | 14.0 | 689.7 | 23.0 | | |
| 14 | 16.0 | 709.9 | 20.3 | | |
| 15 | 18.0 | 729.6 | 19.6 | | |
| 16 | 20.0 | 747.0 | 17.4 | | |
| 17 | 22.0 | 765.3 | 18.4 | | |
| 18 | 24.0 | 781.6 | 16.3 | | |
| 19 | 26.0 | 797.6 | 16.0 | | |
| 20 | 28.0 | 810.2 | 12.6 | | |
| 21 | 30.0 | 823.6 | 13.4 | | |
| 22 | 35.0 | 854.8 | 31.2 | | |
| 23 | 40.0 | 880.5 | 25.7 | | |
| 24 | 45.0 | 903.7 | 23.2 | | |
| 25 | 50.0 | 924.5 | 20.8 | | |
| 26 | 55.0 | 942.1 | 17.6 | | |
| 27 | 60.0 | 958.9 | 16.8 | | |
| 28 | 70.0 | 986.1 | 27.2 | | |
| 29 | 80.0 | 1008.5 | 22.4 | | |
| 30 | 90.0 | 1026.9 | 18.4 | | |
| 31 | 100.0 | 1041.0 | 14.1 | | |
| 32 | 110.0 | 1053.3 | 12.3 | | |
| F 33 | 121.4 | 1066.7 | 13.4 | | |
| SECOND CLOSED-IN | | | | | |
| F 1 | 0.0 | 1066.7 | | | |
| 2 | 1.0 | 1090.9 | 24.2 | 1.0 | 2.144 |
| 3 | 2.0 | 1095.1 | 28.3 | 1.9 | 1.833 |
| 4 | 3.0 | 1097.3 | 30.6 | 2.9 | 1.660 |
| 5 | 4.0 | 1099.7 | 33.0 | 3.9 | 1.529 |
| 6 | 5.0 | 1100.5 | 33.8 | 4.8 | 1.439 |
| 7 | 6.0 | 1102.0 | 35.2 | 5.7 | 1.364 |
| 8 | 7.0 | 1103.6 | 36.8 | 6.6 | 1.301 |
| 9 | 8.0 | 1104.7 | 37.9 | 7.5 | 1.246 |
| 10 | 9.0 | 1105.5 | 38.7 | 8.4 | 1.196 |
| 11 | 10.0 | 1106.8 | 40.0 | 9.3 | 1.153 |
| 12 | 12.0 | 1109.2 | 42.4 | 11.0 | 1.081 |
| 13 | 14.0 | 1110.4 | 43.7 | 12.7 | 1.019 |
| 14 | 16.0 | 1112.5 | 45.8 | 14.2 | 0.969 |
| 15 | 18.0 | 1114.0 | 47.2 | 15.9 | 0.922 |
| 16 | 20.0 | 1114.9 | 48.2 | 17.4 | 0.882 |
| 17 | 22.0 | 1116.5 | 49.8 | 18.9 | 0.846 |
| 18 | 24.0 | 1118.0 | 51.2 | 20.3 | 0.815 |
| 19 | 26.0 | 1118.9 | 52.2 | 21.7 | 0.786 |
| 20 | 28.0 | 1120.4 | 53.6 | 23.1 | 0.758 |
| 21 | 30.0 | 1121.2 | 54.4 | 24.5 | 0.734 |
| 22 | 35.0 | 1123.6 | 56.8 | 27.7 | 0.680 |

REMARKS:

TICKET NO: 70707500
 CLOCK NO: 17524 HOUR: 24

GAUGE NO: 7351
 DEPTH: 5123.0

| REF | MINUTES | PRESSURE | AP | $\frac{t \times t}{t \times t}$ | $\log \frac{t \times t}{t \times t}$ |
|------------------------------|---------|----------|------|---------------------------------|--------------------------------------|
| SECOND CLOSED-IN - CONTINUED | | | | | |
| 23 | 40.0 | 1126.1 | 59.4 | 30.7 | 0.635 |
| 24 | 45.0 | 1128.1 | 61.3 | 33.6 | 0.596 |
| 25 | 50.0 | 1130.1 | 63.4 | 36.3 | 0.562 |
| 26 | 55.0 | 1132.4 | 65.6 | 38.9 | 0.533 |
| 27 | 60.0 | 1134.5 | 67.7 | 41.3 | 0.507 |
| 28 | 70.0 | 1138.0 | 71.3 | 45.8 | 0.462 |
| 29 | 80.0 | 1140.5 | 73.8 | 49.9 | 0.424 |
| 30 | 90.0 | 1143.7 | 77.0 | 53.6 | 0.393 |
| 31 | 100.0 | 1145.8 | 79.1 | 57.0 | 0.367 |
| 32 | 110.0 | 1147.9 | 81.2 | 60.1 | 0.343 |
| G 33 | 118.6 | 1150.3 | 83.6 | 62.6 | 0.326 |

| REF | MINUTES | PRESSURE | AP | $\frac{t \times t}{t \times t}$ | $\log \frac{t \times t}{t \times t}$ |
|-----|---------|----------|----|---------------------------------|--------------------------------------|
| | | | | | |

REMARKS:

TICKET NO: 70707500

CLOCK NO: 17532 HOUR: 24

GAUGE NO: 7352

DEPTH: 5242.0

| REF | MINUTES | PRESSURE | AP | $\frac{t \times \Delta t}{t + \Delta t}$ | $\log \frac{t + \Delta t}{\Delta t}$ |
|-----------------|---------|----------|-------|--|--------------------------------------|
| FIRST FLOW | | | | | |
| B 1 | 0.0 | 193.2 | | | |
| 2 | 1.0 | 280.4 | 87.2 | | |
| 3 | 3.0 | 352.1 | 71.7 | | |
| 4 | 4.0 | 372.7 | 20.6 | | |
| 5 | 5.0 | 391.6 | 18.9 | | |
| 6 | 6.0 | 413.0 | 21.4 | | |
| 7 | 7.0 | 430.8 | 17.8 | | |
| 8 | 8.0 | 451.0 | 20.2 | | |
| 9 | 9.0 | 468.4 | 17.4 | | |
| 10 | 9.9 | 484.4 | 15.0 | | |
| C 11 | 11.2 | 503.0 | 18.6 | | |
| FIRST CLOSED-IN | | | | | |
| C 1 | 0.0 | 503.0 | | | |
| 2 | 1.0 | 993.3 | 490.4 | 0.9 | 1.089 |
| 3 | 2.0 | 1036.8 | 533.8 | 1.7 | 0.828 |
| 4 | 3.0 | 1069.2 | 566.2 | 2.4 | 0.674 |
| 5 | 4.0 | 1089.7 | 586.8 | 3.0 | 0.577 |
| 6 | 5.0 | 1103.1 | 600.2 | 3.4 | 0.512 |
| 7 | 6.0 | 1115.9 | 612.9 | 3.9 | 0.456 |
| 8 | 7.0 | 1123.6 | 620.6 | 4.3 | 0.414 |
| 9 | 8.0 | 1131.2 | 628.2 | 4.7 | 0.381 |
| 10 | 9.0 | 1138.2 | 635.2 | 5.0 | 0.352 |
| 11 | 10.0 | 1145.1 | 642.1 | 5.3 | 0.327 |
| 12 | 12.0 | 1155.7 | 652.7 | 5.8 | 0.286 |
| 13 | 14.0 | 1164.4 | 661.4 | 6.2 | 0.255 |
| 14 | 16.0 | 1170.8 | 667.8 | 6.6 | 0.231 |
| 15 | 18.0 | 1176.2 | 673.3 | 6.9 | 0.210 |
| 16 | 20.0 | 1181.8 | 678.9 | 7.2 | 0.193 |
| 17 | 22.0 | 1186.4 | 683.4 | 7.4 | 0.179 |
| 18 | 24.0 | 1190.4 | 687.5 | 7.6 | 0.166 |
| 19 | 26.0 | 1193.9 | 690.9 | 7.8 | 0.155 |
| 20 | 28.0 | 1197.3 | 694.3 | 8.0 | 0.146 |
| 21 | 30.0 | 1199.9 | 697.0 | 8.1 | 0.138 |
| 22 | 35.0 | 1206.8 | 703.8 | 8.5 | 0.120 |
| 23 | 40.0 | 1211.6 | 708.7 | 8.7 | 0.107 |
| 24 | 45.0 | 1216.8 | 713.8 | 9.0 | 0.096 |
| 25 | 50.0 | 1220.8 | 717.9 | 9.1 | 0.088 |
| 26 | 55.0 | 1223.9 | 721.0 | 9.3 | 0.080 |
| D 27 | 60.8 | 1227.2 | 724.2 | 9.4 | 0.073 |
| SECOND FLOW | | | | | |
| E 1 | 0.0 | 543.5 | | | |
| 2 | 1.0 | 547.6 | 4.0 | | |
| 3 | 2.0 | 560.6 | 13.0 | | |
| 4 | 3.0 | 579.2 | 18.6 | | |
| 5 | 4.0 | 596.6 | 17.4 | | |
| 6 | 5.0 | 611.2 | 14.6 | | |

| REF | MINUTES | PRESSURE | AP | $\frac{t \times \Delta t}{t + \Delta t}$ | $\log \frac{t + \Delta t}{\Delta t}$ |
|-------------------------|---------|----------|------|--|--------------------------------------|
| SECOND FLOW - CONTINUED | | | | | |
| 7 | 6.0 | 627.6 | 16.3 | | |
| 8 | 7.0 | 643.1 | 15.5 | | |
| 9 | 8.0 | 657.7 | 14.6 | | |
| 10 | 9.0 | 670.9 | 13.2 | | |
| 11 | 10.0 | 684.3 | 13.4 | | |
| 12 | 12.0 | 708.2 | 23.9 | | |
| 13 | 14.0 | 731.1 | 22.9 | | |
| 14 | 16.0 | 753.3 | 22.2 | | |
| 15 | 18.0 | 773.2 | 19.9 | | |
| 16 | 20.0 | 793.1 | 19.9 | | |
| 17 | 22.0 | 811.8 | 18.7 | | |
| 18 | 24.0 | 828.0 | 16.2 | | |
| 19 | 26.0 | 844.3 | 16.3 | | |
| 20 | 28.0 | 858.5 | 14.2 | | |
| 21 | 30.0 | 870.9 | 12.5 | | |
| 22 | 35.0 | 901.9 | 31.0 | | |
| 23 | 40.0 | 929.3 | 27.4 | | |
| 24 | 45.0 | 952.5 | 23.2 | | |
| 25 | 50.0 | 972.8 | 20.2 | | |
| 26 | 55.0 | 991.6 | 18.8 | | |
| 27 | 60.0 | 1008.0 | 16.4 | | |
| 28 | 70.0 | 1035.6 | 27.6 | | |
| 29 | 80.0 | 1057.9 | 22.3 | | |
| 30 | 90.0 | 1076.6 | 18.7 | | |
| 31 | 100.0 | 1092.6 | 16.1 | | |
| 32 | 110.0 | 1106.2 | 13.6 | | |
| F 33 | 121.4 | 1118.7 | 12.5 | | |
| SECOND CLOSED-IN | | | | | |
| F 1 | 0.0 | 1118.7 | | | |
| 2 | 1.0 | 1140.5 | 21.8 | 1.0 | 2.142 |
| 3 | 2.0 | 1145.3 | 26.7 | 2.0 | 1.825 |
| 4 | 3.0 | 1148.9 | 30.3 | 2.9 | 1.654 |
| 5 | 4.0 | 1150.9 | 32.3 | 3.9 | 1.537 |
| 6 | 5.0 | 1152.7 | 34.0 | 4.8 | 1.440 |
| 7 | 6.0 | 1154.4 | 35.7 | 5.7 | 1.367 |
| 8 | 7.0 | 1156.1 | 37.4 | 6.7 | 1.299 |
| 9 | 8.0 | 1157.2 | 38.5 | 7.5 | 1.245 |
| 10 | 9.0 | 1158.4 | 39.8 | 8.4 | 1.196 |
| 11 | 10.0 | 1159.4 | 40.7 | 9.3 | 1.156 |
| 12 | 12.0 | 1162.0 | 43.4 | 11.0 | 1.080 |
| 13 | 14.0 | 1163.9 | 45.2 | 12.6 | 1.021 |
| 14 | 16.0 | 1165.4 | 46.8 | 14.2 | 0.969 |
| 15 | 18.0 | 1167.0 | 48.3 | 15.9 | 0.922 |
| 16 | 20.0 | 1168.1 | 49.4 | 17.4 | 0.882 |
| 17 | 22.0 | 1170.1 | 51.5 | 18.9 | 0.847 |
| 18 | 24.0 | 1171.5 | 52.9 | 20.3 | 0.815 |
| 19 | 26.0 | 1172.8 | 54.1 | 21.7 | 0.786 |
| 20 | 28.0 | 1174.0 | 55.4 | 23.1 | 0.758 |
| 21 | 30.0 | 1175.6 | 56.9 | 24.4 | 0.734 |
| 22 | 35.0 | 1177.6 | 59.0 | 27.7 | 0.680 |
| 23 | 40.0 | 1179.6 | 61.0 | 30.7 | 0.635 |

REMARKS:

TICKET NO : 70707500

CLOCK NO : 17532 HOUR : 24




























GAUGE NO : 7352

DEPTH : 5242.0

| REF | MINUTES | PRESSURE | AP | $\frac{t \times \Delta t}{t + \Delta t}$ | $\log \frac{t + \Delta t}{\Delta t}$ |
|------------------------------|---------|----------|------|--|--------------------------------------|
| SECOND CLOSED-IN - CONTINUED | | | | | |
| 24 | 45.0 | 1182.4 | 63.8 | 33.6 | 0.596 |
| 25 | 50.0 | 1184.8 | 65.1 | 36.3 | 0.563 |
| 26 | 55.0 | 1186.5 | 67.8 | 38.8 | 0.533 |
| 27 | 60.0 | 1189.0 | 70.3 | 41.3 | 0.507 |
| 28 | 70.0 | 1192.6 | 73.9 | 45.8 | 0.462 |
| 29 | 80.0 | 1194.8 | 76.1 | 49.9 | 0.424 |
| 30 | 90.0 | 1199.1 | 80.5 | 53.6 | 0.393 |
| 31 | 100.0 | 1201.3 | 82.7 | 57.0 | 0.366 |
| 32 | 110.0 | 1202.9 | 84.2 | 60.1 | 0.343 |
| G 33 | 118.6 | 1204.4 | 85.8 | 62.6 | 0.326 |

| REF | MINUTES | PRESSURE | AP | $\frac{t \times \Delta t}{t + \Delta t}$ | $\log \frac{t + \Delta t}{\Delta t}$ |
|-----|---------|----------|----|--|--------------------------------------|
|-----|---------|----------|----|--|--------------------------------------|

REMARKS :

| | | O.D. | I.D. | LENGTH | DEPTH | |
|----|---|----------------------------------|-------|--------|--------|--------|
| 1 |  | DRILL PIPE..... | 4.500 | 3.826 | 4643.3 | |
| 3 |  | DRILL COLLARS..... | 6.000 | 2.250 | 431.5 | |
| 50 |  | IMPACT REVERSING SUB..... | 6.000 | 2.170 | 1.0 | 5075.4 |
| 3 |  | DRILL COLLARS..... | 6.000 | 2.250 | 28.1 | |
| 5 |  | CROSSOVER..... | 6.000 | 2.370 | 1.0 | |
| 11 |  | HANDLING SUB & CHOKE ASSEMBLY... | 4.500 | 2.430 | 5.0 | |
| 12 |  | DUAL CIP VALVE..... | 5.000 | 0.750 | 7.0 | |
| 60 |  | HYDROSPRING TESTER..... | 5.000 | 0.750 | 5.0 | 5121.0 |
| 80 |  | AP RUNNING CASE..... | 5.000 | 2.250 | 4.0 | 5123.0 |
| 15 |  | JAR..... | 5.000 | 1.750 | 5.0 | |
| 17 |  | PRESSURE EQUALIZING CROSSOVER... | 5.000 | 1.000 | 1.0 | |
| 70 |  | OPEN HOLE PACKER..... | 6.750 | 1.530 | 6.0 | 5136.0 |
| 20 |  | FLUSH JOINT ANCHOR..... | 5.000 | 2.370 | 11.0 | |
| 17 |  | PRESSURE EQUALIZING CROSSOVER... | 5.000 | 1.000 | 1.0 | |
| 5 |  | CROSSOVER..... | 6.000 | 2.370 | 1.0 | |
| 3 |  | DRILL COLLARS..... | 6.000 | 2.250 | 88.0 | |
| 5 |  | CROSSOVER..... | 6.000 | 2.370 | 1.0 | |
| 5 |  | CROSSOVER..... | 6.000 | 2.370 | 1.0 | |
| 81 |  | BLANKED-OFF RUNNING CASE..... | 5.000 | | 4.0 | 5242.0 |
| 70 |  | OPEN HOLE PACKER..... | 6.750 | 1.530 | 6.0 | 5247.0 |
| 5 |  | CROSSOVER..... | 6.000 | 2.370 | 1.0 | |
| 5 |  | CROSSOVER..... | 6.000 | 2.370 | 1.0 | |
| 3 |  | DRILL COLLARS..... | 6.000 | 2.250 | 178.0 | |
| 5 |  | CROSSOVER..... | 6.000 | 2.370 | 1.0 | |
| 5 |  | CROSSOVER..... | 6.000 | 2.370 | 1.0 | |
| 20 |  | FLUSH JOINT ANCHOR..... | 5.000 | 2.370 | 11.0 | |
| 81 |  | BLANKED-OFF RUNNING CASE..... | 5.000 | | 4.0 | 5445.0 |

TOTAL DEPTH

5448.0

EQUIPMENT DATA

1000

GAUGE NO 7351 CIP 1 2

GAUGE NO 7352 CIP 1 2

GAUGE NO 6773 CIP 1 2

TICKET NO 70707500

DP, PSI

100

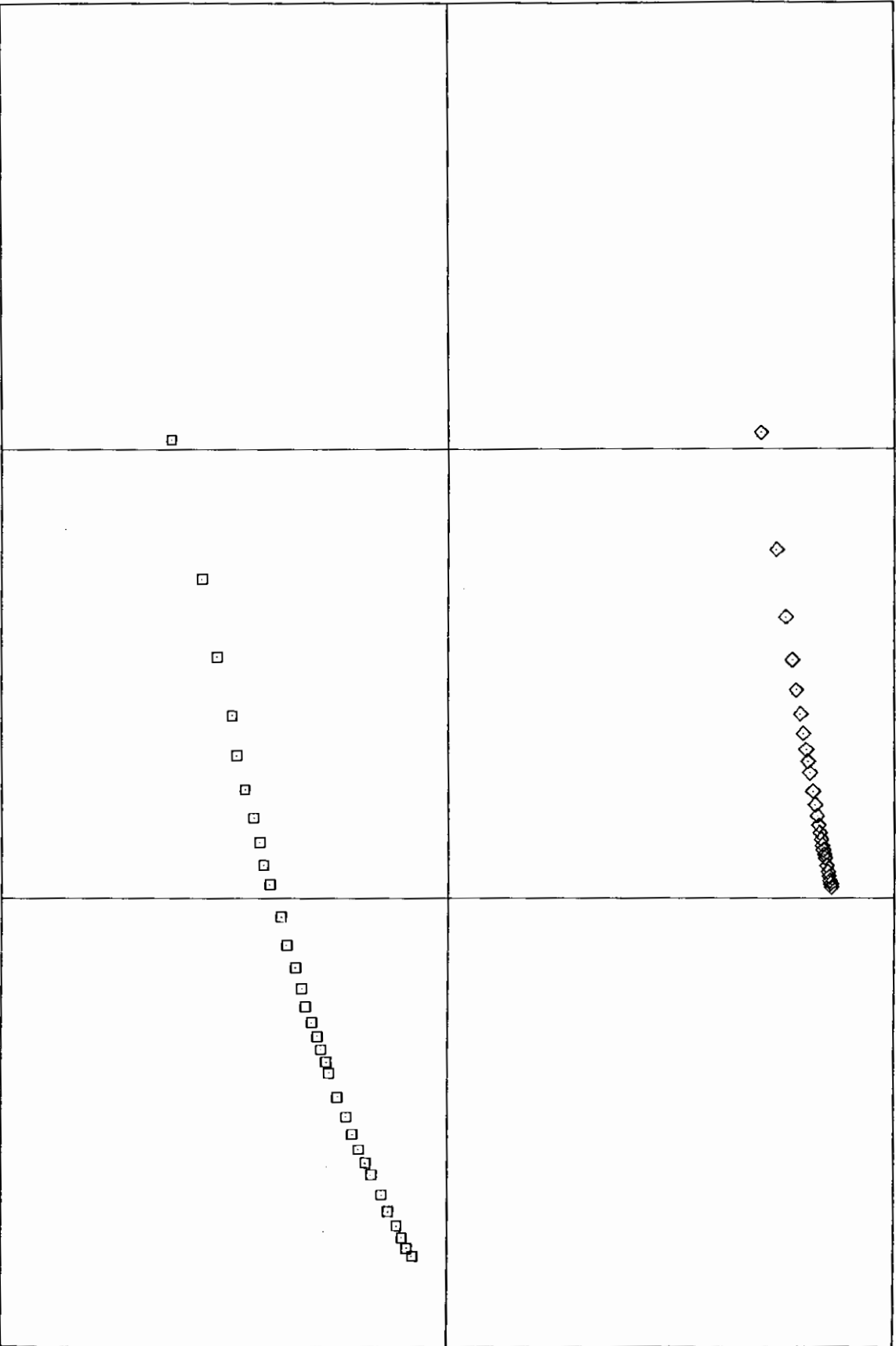
10
0.1

1.

10.

100.

$T*DT / (T+DT)$



DP, PSI

1000

GAUGE NO 7351 CIP 1 2

GAUGE NO 7352 CIP 1 2

GAUGE NO 6773

TICKET NO 70707500

100

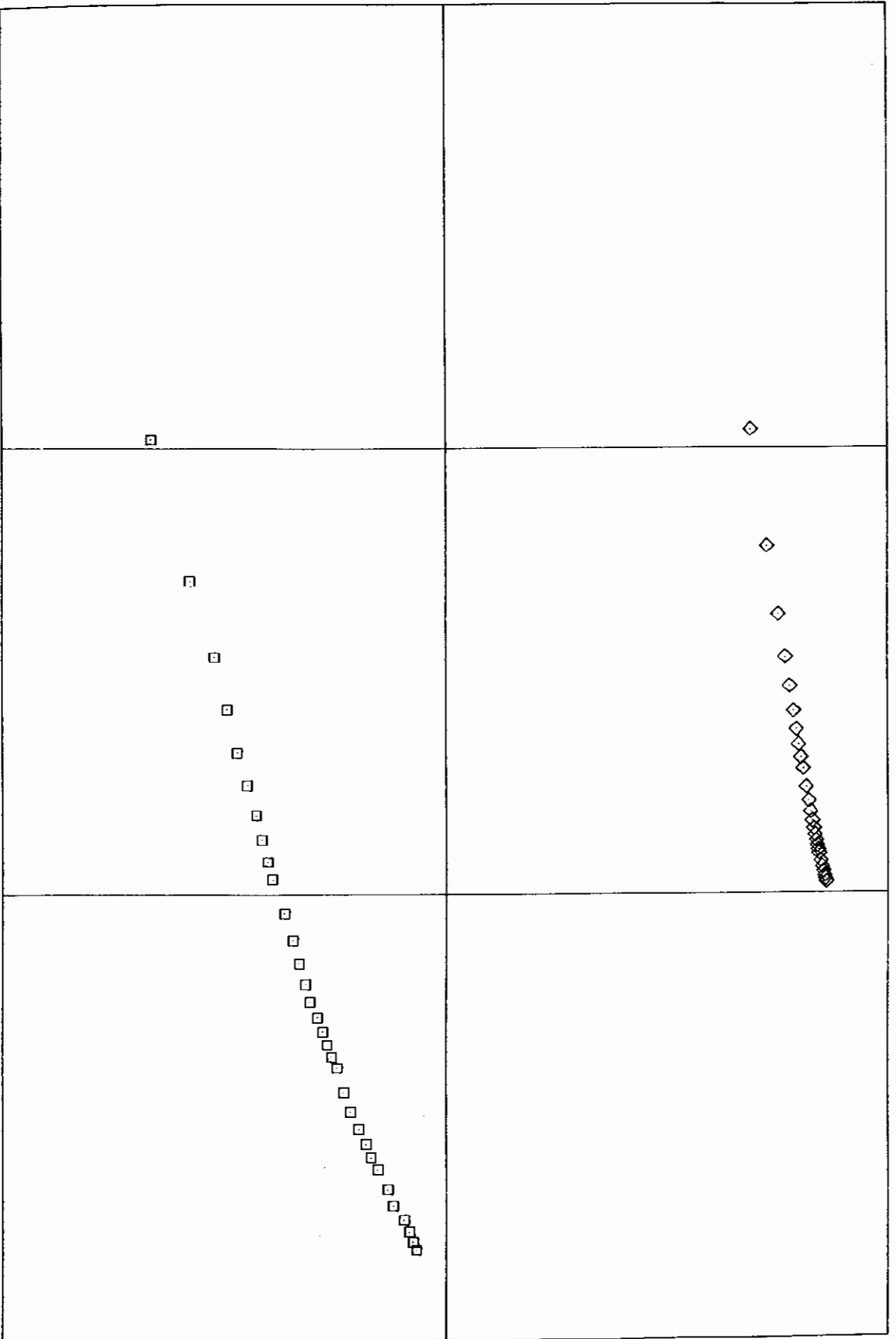
10
0.1

1.

10

100.

$T*DT / (T+DT)$

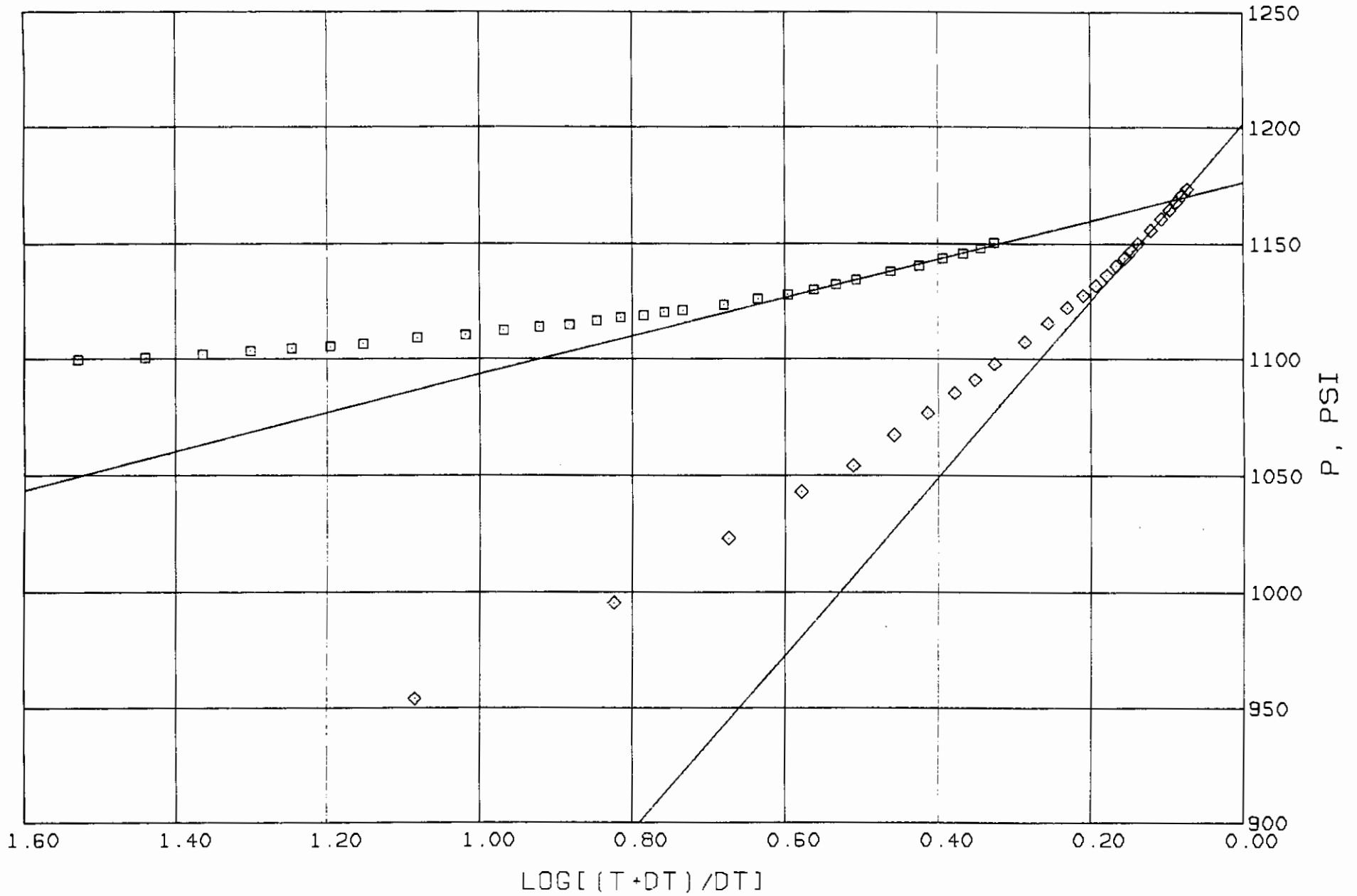


TICKET NO 70707500

GAUGE NO CIP 1 2
7351 ◇ □

GAUGE NO CIP 1 2
7352

GAUGE NO CIP 1 2
6773

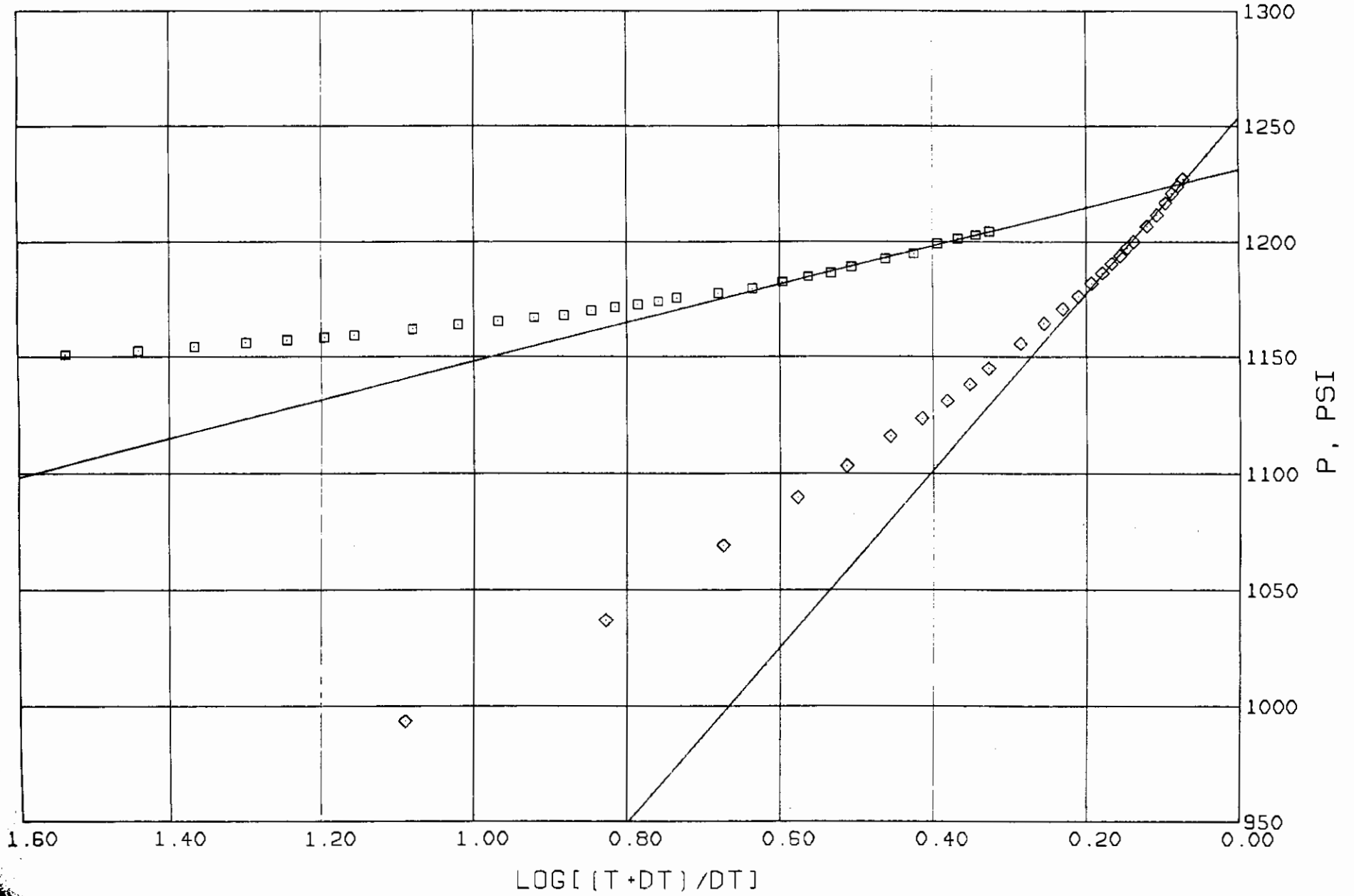


TICKET NO 70707500

GAUGE NO CIP 1 2
7351

GAUGE NO CIP 1 2
7352 ◊ □

GAUGE NO CIP 1 2
6773



SUMMARY OF RESERVOIR PARAMETERS USING HORNER METHOD FOR LIQUID WELLS

OIL GRAVITY 0.0 °API@60 °F WATER SALINITY 3.7 % SALT
 GAS GRAVITY 0.700 FLUID GRADIENT 0.4448 psi/ft
 GAS/OIL RATIO 0.0 SCF/STB FLUID PROPERTIES AT 1231.3 psig
 TEMPERATURE 125.0 °F VISCOSITY 0.573 cp
 NET PAY 61.0 ft FMT VOL FACTOR 1.009 Rvol/Svol
 POROSITY 10.0 % SYSTEM COMPRESSIBILITY 7.73 x10⁻⁶ vol/vol/psi
 PIPE CAPACITY FACTORS 0.00492 0.01422 bbl/ft

| GAUGE NUMBER | | 7351 | 7351 | 7352 | 7352 | | |
|-------------------------|--------------------|---------|---------|---------|---------|--|-------------|
| GAUGE DEPTH | | 5123.0 | 5123.0 | 5242.0 | 5242.0 | | |
| FLOW AND CIP PERIOD | | 1 | 2 | 1 | 2 | | UNITS |
| FINAL FLOW PRESSURE | P _r | 452.0 | 1066.7 | 503.0 | 1118.7 | | psig |
| TOTAL FLOW TIME | t | 11.2 | 132.6 | 11.2 | 132.6 | | min |
| EXTRAPOLATED PRESSURE | P* | 1201.5 | 1176.6 | 1253.7 | 1231.3 | | psig |
| ONE CYCLE PRESSURE | | 819.9 | 1093.4 | 872.8 | 1148.2 | | psig |
| PRODUCTION RATE | Q | 953.4 | 624.4 | 1048.3 | 617.1 | | BPD |
| TRANSMISSIBILITY | k _h / μ | 410.1 | 1230.9 | 451.6 | 1217.5 | | md-ft cp |
| FLOW CAPACITY | k _h | 235.002 | 705.390 | 258.800 | 697.740 | | md-ft |
| PERMEABILITY | k | 3.85250 | 11.5638 | 4.24262 | 11.4384 | | md |
| SKIN FACTOR | S | -2.3 | -4.8 | -2.3 | -4.8 | | |
| DAMAGE RATIO | DR | 0.5 | 0.2 | 0.5 | 0.2 | | |
| POTENTIAL RATE | Q ₁ | 953.4 | 624.4 | 1048.3 | 617.1 | | BPD |
| RADIUS OF INVESTIGATION | r _i | 40.7 | 243.0 | 42.7 | 241.7 | | ft |

REMARKS: ANALYSIS RESULTS SHOWN ABOVE ARE RELATIVE TO SALTWATER. THE NATURE OF THE PLOTS INDICATE THE PRESENCE OF A PERMEABILITY ANOMALY WITHIN THE TESTED INTERVAL (I.E. NATURAL FRACTURES, LAYERED FORMATION, ETC.)

NOTICE: BECAUSE OF THE UNCERTAINTY OF VARIABLE WELL CONDITIONS AND THE NECESSITY OF RELYING ON FACTS AND SUPPORTING SERVICES FURNISHED BY OTHERS, HRS IS UNABLE TO GUARANTEE THE ACCURACY OF ANY CHART INTERPRETATION, RESEARCH ANALYSIS, JOB RECOMMENDATION OR OTHER DATA FURNISHED BY HRS. HRS PERSONNEL WILL USE THEIR BEST EFFORTS IN GATHERING SUCH INFORMATION AND THEIR BEST JUDGMENT IN INTERPRETING IT BUT CUSTOMER AGREES THAT HRS SHALL NOT BE RESPONSIBLE FOR ANY DAMAGES ARISING FROM THE USE OF SUCH INFORMATION EXCEPT WHERE DUE TO HRS GROSS NEGLIGENCE OR WILLFUL MISCONDUCT IN THE PREPARATION OF FURNISHING OF INFORMATION.