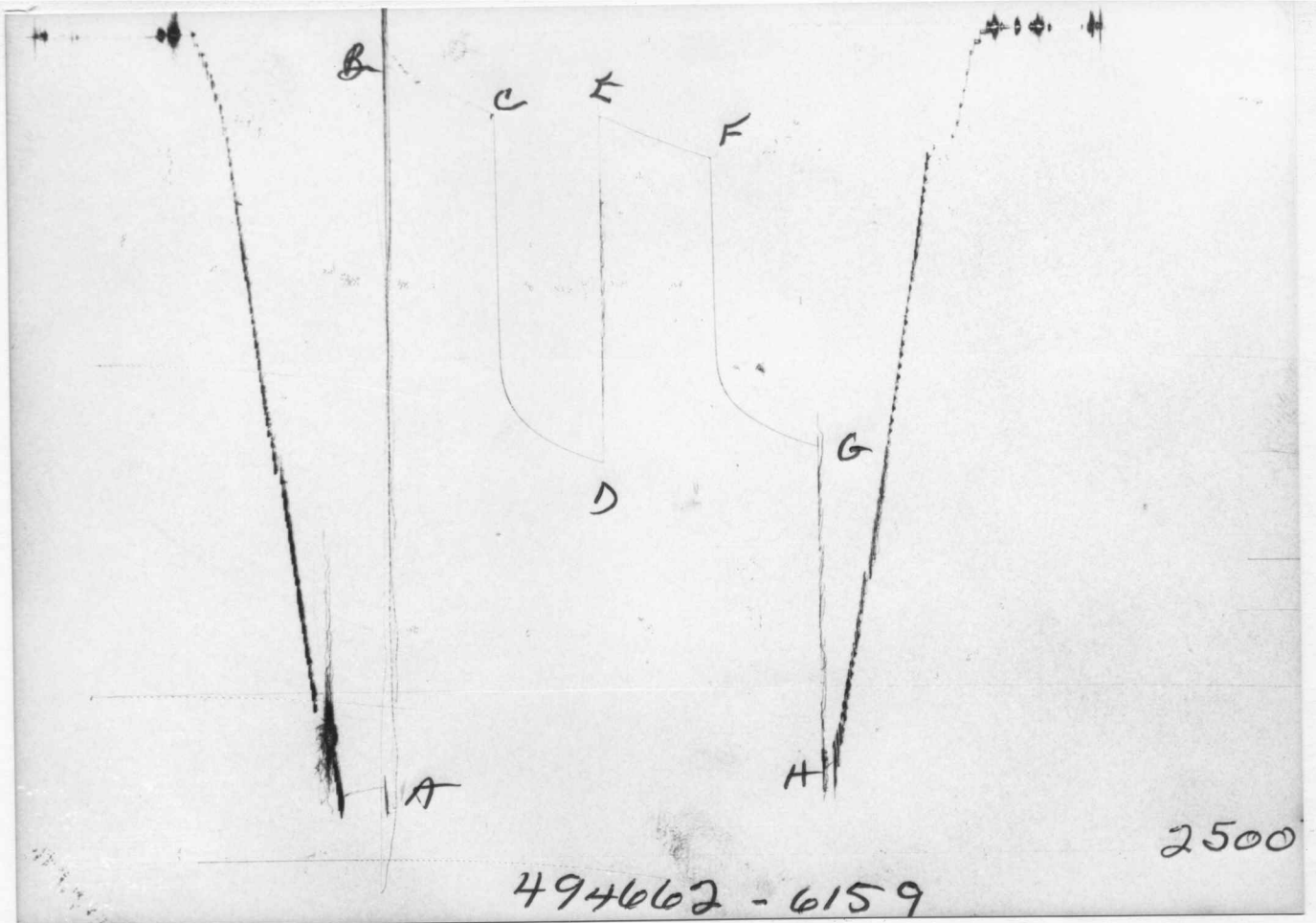




TICKET NO. 49466200
23-NOV-83
GREAT BEND

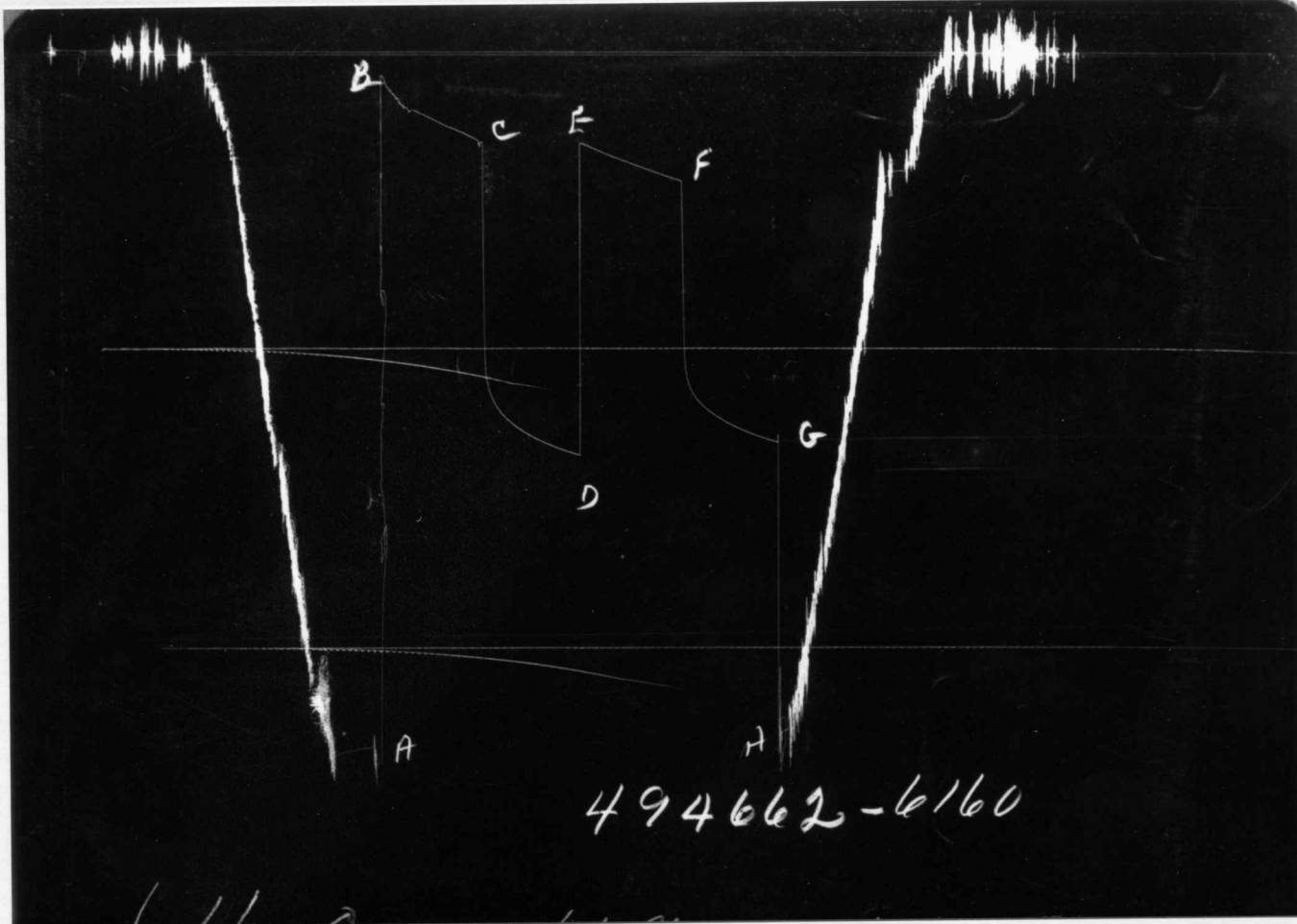
FORMATION TESTING SERVICE REPORT

PRATT	1	1	4288.1 - 4359.1	SPINES EXPLORATION INCORPORATED
LEASE NAME	WELL NO.	TEST NO.	TESTED INTERVAL	LEASE OWNER/COMPANY NAME
C-NE-NW-15-24-18W				
LEGAL LOCATION SEC. - TWP. - RMC.	FIELD AREA	COUNTY	STATE	
		EDWARDS	KANSAS	OR



GAUGE NO: 6159 DEPTH: 4267.2 BLANKED OFF: NO HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		2281.7			
B	INITIAL FIRST FLOW		16.4			
C	FINAL FIRST FLOW		249.9	60.0	60.7	F
C	INITIAL FIRST CLOSED-IN		249.9			
D	FINAL FIRST CLOSED-IN		1314.6	60.0	57.6	C
E	INITIAL SECOND FLOW		264.3			
F	FINAL SECOND FLOW		393.0	60.0	61.6	F
F	INITIAL SECOND CLOSED-IN		393.0			
G	FINAL SECOND CLOSED-IN		1271.7	60.0	57.5	C
H	FINAL HYDROSTATIC		2226.9			



GAUGE NO: 6160 DEPTH: 4356.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	2366	2329.2			
B	INITIAL FIRST FLOW	68	78.9			
C	FINAL FIRST FLOW	297	302.9	60.0	60.7	F
C	INITIAL FIRST CLOSED-IN	297	302.9			
D	FINAL FIRST CLOSED-IN	1349	1356.7	60.0	57.6	C
E	INITIAL SECOND FLOW	297	309.4			
F	FINAL SECOND FLOW	433	436.8	60.0	61.6	F
F	INITIAL SECOND CLOSED-IN	433	436.8			
G	FINAL SECOND CLOSED-IN	1307	1313.2	60.0	57.5	C
H	FINAL HYDROSTATIC	2267	2271.7			

EQUIPMENT & HOLE DATA

FORMATION TESTED: MARMATON
 NET PAY (ft): _____
 GROSS TESTED FOOTAGE: 71.0
 ALL DEPTHS MEASURED FROM: KELLY BUSHING
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.875
 ELEVATION (ft): 2149
 TOTAL DEPTH (ft): 4359.0
 PACKER DEPTH(S) (ft): 4282, 4288
 FINAL SURFACE CHOKE (in): _____
 BOTTOM HOLE CHOKE (in): _____
 MUD WEIGHT (lb/gal): 9.80
 MUD VISCOSITY (sec): 42
 ESTIMATED HOLE TEMP. (°F): _____
 ACTUAL HOLE TEMP. (°F): 110 @ 4354.0 ft

TICKET NUMBER: 49466200
 DATE: 11-20-83 TEST NO: 1
 TYPE DST: OPEN HOLE
 HALLIBURTON CAMP:
GREAT BEND
 TESTER: T.R. GAUNT
 WITNESS: DOUG DAVIS
 DRILLING CONTRACTOR:
BIG SPRINGS #3

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES
<u>PIT SAMPLE</u>	<u> </u> @ <u> </u> °F	<u>40000</u> ppm
<u>RECOVERY</u>	<u> </u> @ <u> </u> °F	<u>93500</u> ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

SAMPLER DATA

P_{sig} AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ @ _____ °F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____

RECOVERED:

700 FEET OF WATER

MEASURED FROM TESTER VALVE

REMARKS:

TICKET NO: 49466200
 CLOCK NO: 3722 HOUR: 12



GAUGE NO: 6159
 DEPTH: 4267.2

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B	1	0.0	16.4		
	2	10.0	99.4	83.0	
	3	20.0	151.1	51.6	
	4	30.0	170.3	19.3	
	5	40.0	195.3	25.0	
	6	50.0	220.3	24.9	
C	7	60.7	249.9	29.7	
FIRST CLOSED-IN					
C	1	0.0	249.9		
	2	4.0	1066.9	817.0	3.7 1.212
	3	8.0	1134.7	884.8	7.1 0.933
	4	12.0	1169.6	919.7	10.0 0.782
	5	16.0	1194.9	945.0	12.6 0.682
	6	20.0	1213.1	963.2	15.0 0.607
	7	24.0	1229.4	979.5	17.2 0.547
	8	28.0	1244.7	994.7	19.2 0.501
	9	32.0	1257.5	1007.6	21.0 0.462
	10	36.0	1268.4	1018.5	22.6 0.429
	11	40.0	1277.5	1027.6	24.1 0.401
	12	44.0	1287.5	1037.5	25.5 0.377
	13	48.0	1296.1	1046.2	26.8 0.355
	14	52.0	1304.6	1054.7	28.0 0.336
	15	56.0	1311.5	1061.6	29.1 0.319
D	16	57.6	1314.6	1064.7	29.6 0.313
SECOND FLOW					
E	1	0.0	264.3		
	2	10.0	281.8	17.5	
	3	20.0	306.8	25.0	
	4	30.0	327.6	20.8	
	5	40.0	348.6	21.0	
	6	50.0	368.5	19.9	
F	7	61.6	393.0	24.4	
SECOND CLOSED-IN					
F	1	0.0	393.0		
	2	4.0	1074.9	681.9	3.9 1.499
	3	8.0	1117.6	724.7	7.5 1.211
	4	12.0	1144.1	751.1	10.9 1.049
	5	16.0	1164.2	771.3	14.1 0.938
	6	20.0	1181.1	788.2	17.2 0.852
	7	24.0	1194.3	801.3	20.1 0.785
	8	28.0	1206.4	813.4	22.8 0.730
	9	32.0	1218.0	825.1	25.4 0.684
	10	36.0	1228.7	835.7	27.8 0.644

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
	11	40.0	1238.2	845.2	30.1 0.609
	12	44.0	1246.8	853.8	32.3 0.578
	13	48.0	1254.5	861.6	34.5 0.550
	14	52.0	1261.8	868.8	36.5 0.525
	15	56.0	1269.4	876.4	38.4 0.503
G	16	57.5	1271.7	878.7	39.1 0.495

REMARKS:

TICKET NO: 49466200

CLOCK NO: 13851 HOUR: 12





















GAUGE NO: 6160

DEPTH: 4356.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	78.9			
2	10.0	157.0	78.1		
3	20.0	197.4	40.4		
4	30.0	224.0	26.7		
5	40.0	252.1	28.1		
6	50.0	275.8	23.7		
C 7	60.7	302.9	27.1		
FIRST CLOSED-IN					
C 1	0.0	302.9			
2	4.0	1149.6	846.7	3.8	1.207
3	8.0	1197.7	894.8	7.1	0.933
4	12.0	1225.5	922.6	10.1	0.781
5	16.0	1246.6	943.7	12.7	0.681
6	20.0	1263.9	961.0	15.0	0.606
7	24.0	1278.0	975.1	17.2	0.548
8	28.0	1291.1	988.2	19.2	0.501
9	32.0	1302.6	999.7	21.0	0.462
10	36.0	1313.2	1010.3	22.6	0.429
11	40.0	1322.7	1019.8	24.1	0.401
12	44.0	1331.8	1028.9	25.5	0.376
13	48.0	1339.7	1036.8	26.8	0.355
14	52.0	1347.0	1044.1	28.0	0.336
15	56.0	1354.2	1051.3	29.1	0.319
D 16	57.6	1356.7	1053.8	29.6	0.313
SECOND FLOW					
E 1	0.0	309.4			
2	10.0	329.1	19.7		
3	20.0	353.2	24.1		
4	30.0	373.9	20.7		
5	40.0	395.0	21.1		
6	50.0	414.9	19.9		
F 7	61.6	436.8	21.9		
SECOND CLOSED-IN					
F 1	0.0	436.8			
2	4.0	1123.5	686.6	3.8	1.504
3	8.0	1165.7	728.8	7.5	1.213
4	12.0	1190.9	754.0	10.9	1.050
5	16.0	1209.8	773.0	14.1	0.937
6	20.0	1225.5	788.7	17.2	0.853
7	24.0	1238.8	801.9	20.1	0.785
8	28.0	1251.3	814.4	22.8	0.730
9	32.0	1262.6	825.8	25.4	0.684
10	36.0	1272.3	835.4	27.8	0.643

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
11	40.0	1281.3	844.5	30.2	0.608
12	44.0	1290.1	853.3	32.4	0.578
13	48.0	1297.2	860.4	34.5	0.550
14	52.0	1304.4	867.5	36.5	0.526
15	56.0	1311.0	874.1	38.4	0.503
G 16	57.5	1313.2	876.4	39.1	0.495

REMARKS:

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	3974.0	
50		IMPACT REVERSING SUB.....	5.750	2.750	1.0	3958.6
1		DRILL PIPE.....	4.500	3.826	31.0	
3		DRILL COLLARS.....	6.250	2.250	265.0	
5		CROSSOVER.....	5.750	2.750	0.8	
12		DUAL CIP VALVE.....	5.750	0.870	6.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	4266.4
80		AP RUNNING CASE.....	5.000	2.250	4.1	4267.2
15		JAR.....	5.030	1.750	5.0	
16		VR SAFETY JOINT.....	5.000	1.000	2.8	
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	4282.4
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	4288.2
5		CROSSOVER.....	5.750	2.750	1.5	
3		DRILL COLLARS.....	6.250	2.250	29.5	
5		CROSSOVER.....	5.750	2.750	1.5	
20		FLUSH JOINT ANCHOR.....	5.000	2.370	31.0	
82		TEMPERATURE RUNNING CASE.....	5.000		1.5	4354.0
81		BLANKED-OFF RUNNING CASE.....	5.000		4.1	4356.0
TOTAL DEPTH						4359.0

EQUIPMENT DATA

TEMPERATURE

RECORDER

CHART



10° each circle

EQUATIONS FOR DESIGN

Indicated Flow Capacity

$$kh = \frac{1637 Q_g T}{m}$$

md-ft

Average Effective Permeability

$$k = \frac{kh}{h}$$

md

Skin Factor

$$S = 1.151 \left[\frac{m(P^*) - m(P_f)}{m} - \text{LOG} \frac{kt}{\phi \mu c_t r_w^2} + 3.23 \right]$$

—

Damage Ratio

$$DR = \frac{m(P^*) - m(P_f)}{m(P^*) - m(P_f) - 0.87 mS}$$

—

Indicated Flow Rate (Maximum)

$$AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_f)}$$

MCFD

Indicated Flow Rate (Minimum)

$$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_f)}}$$

MCFD

Approx. Radius of Investigation

$$r_i = 0.032 \sqrt{\frac{kt}{\phi \mu c_t}}$$

ft