



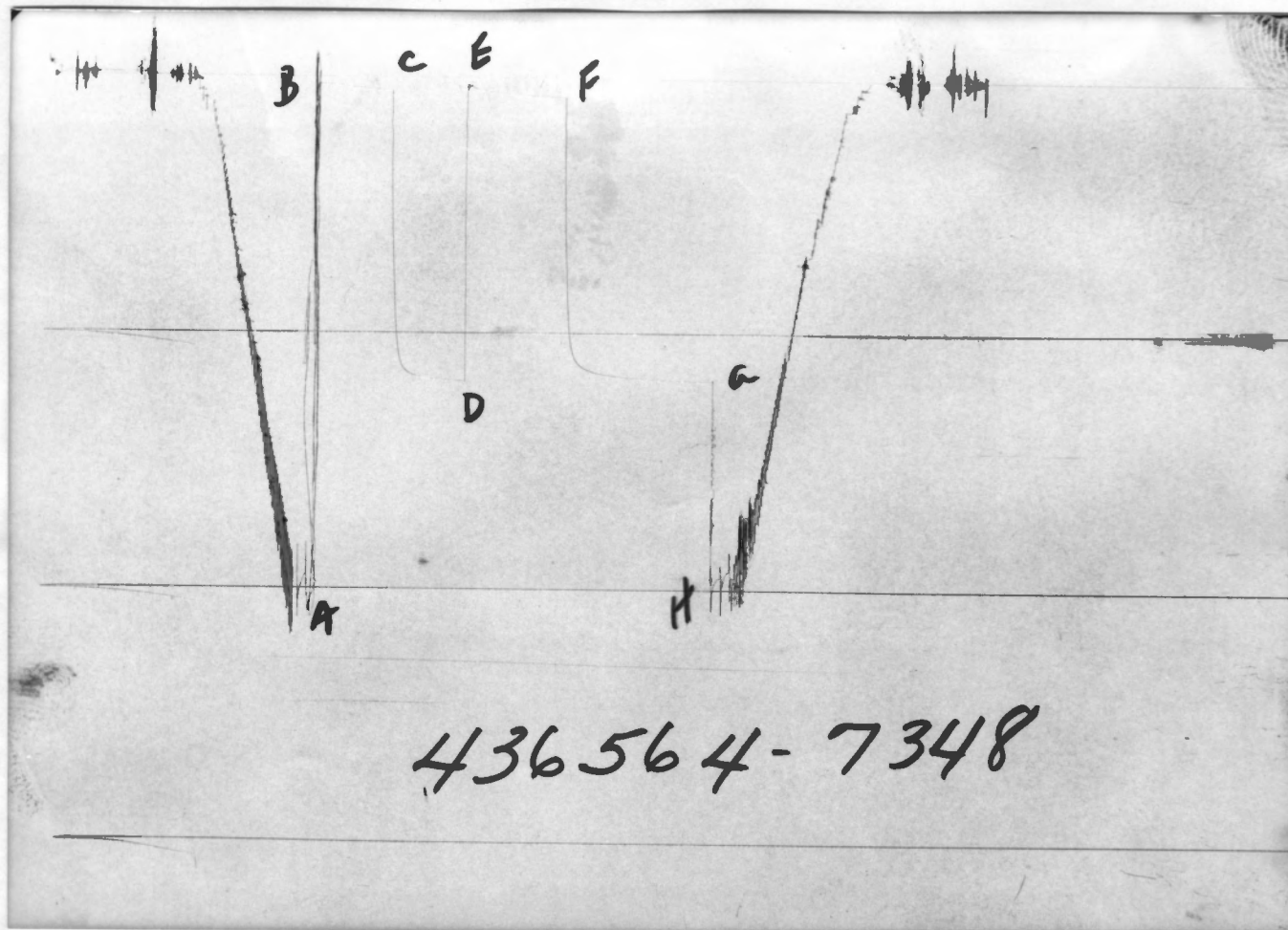
TICKET NO. 43656400

12-SEP-86

PRATT

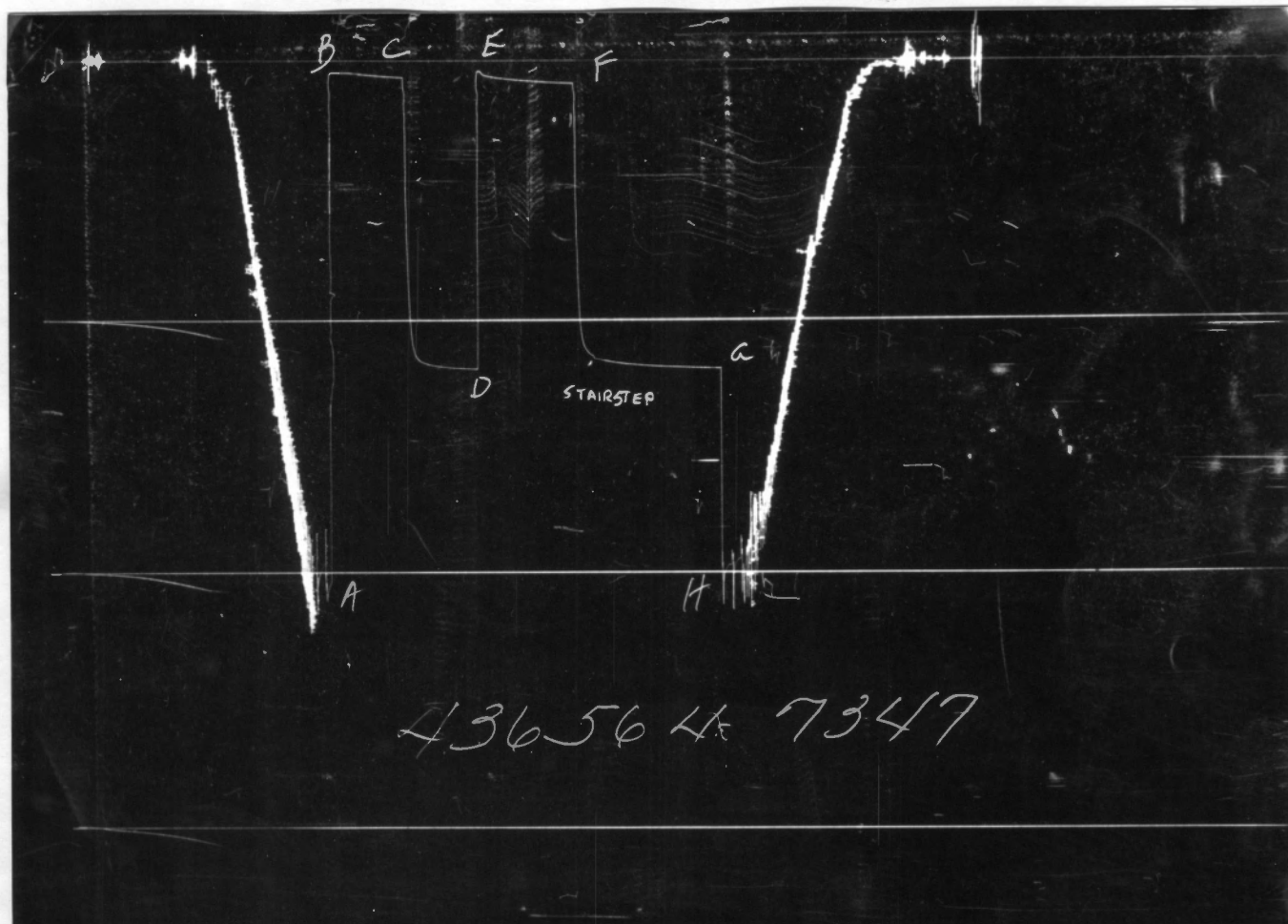
FORMATION TESTING SERVICE REPORT

BRISTON	1	2	4170.0 - 4205.0	MCNEISH OIL OPERATIONS
LEASE NAME	WELL NO.	TEST NO.	TESTED INTERVAL	LEASE OWNER/COMPANY NAME
LEGAL LOCATION 3-265-15W		FIELD PRATT	COUNTY STAFFORD	STATE KANSAS
				SM



GAUGE NO: 7348 DEPTH: 4149.0 BLANKED OFF: NO HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		1956.7			
B	INITIAL FIRST FLOW		27.7			
C	FINAL FIRST FLOW		49.1	45.0	45.4	F
C	INITIAL FIRST CLOSED-IN		49.1			
D	FINAL FIRST CLOSED-IN		1191.6	45.0	45.2	C
E	INITIAL SECOND FLOW		27.4			
F	FINAL SECOND FLOW		73.3	60.0	59.2	F
F	INITIAL SECOND CLOSED-IN		73.3			
G	FINAL SECOND CLOSED-IN		1188.1	90.0	90.2	C
H	FINAL HYDROSTATIC		1962.2			



GAUGE NO: 7347 DEPTH: 4202.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	1968	1973.5			
B	INITIAL FIRST FLOW	39	45.6			
C	FINAL FIRST FLOW	68	63.9	45.0	45.4	F
C	INITIAL FIRST CLOSED-IN	68	63.9			
D	FINAL FIRST CLOSED-IN	1211	1200.8	45.0	45.2	C
E	INITIAL SECOND FLOW	39	41.2			
F	FINAL SECOND FLOW	77	86.3	60.0	59.2	F
F	INITIAL SECOND CLOSED-IN	77	86.3			
G	FINAL SECOND CLOSED-IN	1201	1197.1	90.0	90.2	C
H	FINAL HYDROSTATIC	1968	1980.2			

EQUIPMENT & HOLE DATA

FORMATION TESTED: MISSISSIPPI

NET PAY (ft): 20.0

GROSS TESTED FOOTAGE: 35.0

ALL DEPTHS MEASURED FROM: KELLY BUSHING

CASING PERFS. (ft): _____

HOLE OR CASING SIZE (in): 7.875

ELEVATION (ft): 2040.0

TOTAL DEPTH (ft): 4205.0

PACKER DEPTH(S) (ft): 4164. 4170

FINAL SURFACE CHOKE (in): 0.25000

BOTTOM HOLE CHOKE (in): 0.750

MUD WEIGHT (lb/gal): 9.20

MUD VISCOSITY (sec): 50

ESTIMATED HOLE TEMP. (°F): _____

ACTUAL HOLE TEMP. (°F): 133 @ 4200.0 ft

TICKET NUMBER: 43656400

DATE: 9-9-86 TEST NO: 2

TYPE DST: OPEN HOLE

HALLIBURTON CAMP:
PRATT

TESTER: L.R. PARKER

WITNESS: M. DUBOIS

DRILLING CONTRACTOR:
EAGLE DRILLING COMPANY

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE

RESISTIVITY

CHLORIDES

<u>PIT</u>	<u> </u> @ <u> </u> °F	<u>12000</u> ppm
<u>TOP</u>	<u> </u> @ <u> </u> °F	<u>14000</u> ppm
<u>BOTTOM</u>	<u> </u> @ <u> </u> °F	<u>14500</u> ppm
<u> </u>	<u> </u> @ <u> </u> °F	<u> </u> ppm
<u> </u>	<u> </u> @ <u> </u> °F	<u> </u> ppm
<u> </u>	<u> </u> @ <u> </u> °F	<u> </u> ppm

SAMPLER DATA

Pstg AT SURFACE: _____

cu.ft. OF GAS: _____

cc OF OIL: _____

cc OF WATER: _____

cc OF MUD: _____

TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ @ _____ °F

GAS/OIL RATIO (cu.ft. per bbl): _____

GAS GRAVITY: _____

CUSHION DATA

TYPE AMOUNT WEIGHT

RECOVERED:

90 FEET OF DRILLING MUD

MEASURED FROM
TESTER VALVE

REMARKS:

TICKET NO: 43656400

[illegible]

TICKET NO: 43656400

CLOCK NO: 26864 HOUR: 12



GAUGE NO: 7348

DEPTH: 4149.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	27.7			
2	3.0	27.8	0.2		
3	6.0	29.2	1.4		
4	9.0	29.3	0.1		
5	12.0	30.8	1.5		
6	15.0	33.3	2.5		
7	18.0	35.5	2.2		
8	21.0	37.4	1.9		
9	24.0	39.4	2.1		
10	27.0	41.1	1.7		
11	30.0	42.7	1.6		
12	33.0	44.6	1.9		
13	36.0	45.7	1.1		
14	39.0	47.2	1.5		
15	42.0	48.4	1.3		
C 16	45.4	49.1	0.7		
FIRST CLOSED-IN					
C 1	0.0	49.1			
2	1.0	460.5	411.3	1.0	1.670
3	2.0	732.0	682.8	1.9	1.372
4	3.0	914.2	865.0	2.8	1.205
5	4.0	1013.3	964.2	3.7	1.092
6	5.0	1076.4	1027.3	4.5	1.001
7	6.0	1107.5	1058.4	5.3	0.932
8	7.0	1125.8	1076.6	6.0	0.876
9	8.0	1138.4	1089.2	6.8	0.825
10	9.0	1147.6	1098.5	7.5	0.780
11	10.0	1153.6	1104.5	8.2	0.742
12	12.0	1161.9	1112.8	9.5	0.679
13	14.0	1168.3	1119.2	10.7	0.628
14	16.0	1173.0	1123.9	11.8	0.583
15	18.0	1176.1	1126.9	12.9	0.547
16	20.0	1178.5	1129.4	13.9	0.514
17	22.0	1180.9	1131.8	14.8	0.486
18	24.0	1182.9	1133.8	15.7	0.461
19	26.0	1184.5	1135.3	16.5	0.439
20	28.0	1185.4	1136.3	17.3	0.418
21	30.0	1186.8	1137.7	18.1	0.400
22	35.0	1188.8	1139.6	19.8	0.361
23	40.0	1190.4	1141.3	21.3	0.329
D 24	45.2	1191.6	1142.5	22.7	0.302
SECOND FLOW					
E 1	0.0	27.4			
2	5.0	40.2	12.9		
3	10.0	48.7	8.5		
4	15.0	54.0	5.2		

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
5	20.0	58.4	4.4		
6	25.0	60.9	2.6		
7	30.0	63.6	2.7		
8	35.0	66.3	2.7		
9	40.0	67.7	1.4		
10	45.0	69.4	1.8		
11	50.0	70.8	1.4		
12	55.0	71.8	1.0		
F 13	59.2	73.3	1.5		
SECOND CLOSED-IN					
F 1	0.0	73.3			
2	1.0	498.5	425.2	1.0	2.017
3	2.0	780.0	706.7	2.0	1.720
4	3.0	923.7	850.4	2.9	1.554
5	4.0	1015.0	941.7	3.9	1.432
6	5.0	1057.5	984.2	4.7	1.343
7	6.0	1084.9	1011.6	5.7	1.265
8	7.0	1100.9	1027.6	6.6	1.202
9	8.0	1111.6	1038.3	7.4	1.149
10	9.0	1119.4	1046.1	8.3	1.103
11	10.0	1126.8	1053.5	9.1	1.058
12	12.0	1136.0	1062.7	10.8	0.987
13	14.0	1142.2	1068.9	12.3	0.929
14	16.0	1147.9	1074.6	13.8	0.878
15	18.0	1152.7	1079.4	15.4	0.833
16	20.0	1156.0	1082.7	16.8	0.795
17	22.0	1159.6	1086.3	18.2	0.760
18	24.0	1162.1	1088.8	19.5	0.728
19	26.0	1164.2	1090.9	20.8	0.701
20	28.0	1165.9	1092.6	22.1	0.675
21	30.0	1167.5	1094.2	23.3	0.652
22	35.0	1171.6	1098.3	26.2	0.601
23	40.0	1174.4	1101.1	28.9	0.558
24	45.0	1176.8	1103.5	31.5	0.522
25	50.0	1179.2	1105.9	33.8	0.490
26	55.0	1180.8	1107.4	36.1	0.462
27	60.0	1182.3	1109.0	38.1	0.438
28	70.0	1185.0	1111.7	41.9	0.397
29	80.0	1186.5	1113.2	45.3	0.363
G 30	90.2	1188.1	1114.8	48.4	0.334

REMARKS:

TICKET NO: 43656400

CLOCK NO: 7046 HOUR: 12



HALLIBURTON

 SERVICES

GAUGE NO: 7347

DEPTH: 4202.0
















REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	45.6			
2	3.0	46.0	0.4		
3	6.0	46.1	0.2		
4	9.0	46.1	0.0		
5	12.0	46.7	0.6		
6	15.0	48.4	1.6		
7	18.0	50.3	1.9		
8	21.0	53.1	2.8		
9	24.0	54.8	1.6		
10	27.0	56.0	1.3		
11	30.0	57.5	1.5		
12	33.0	59.3	1.8		
13	36.0	60.4	1.1		
14	39.0	61.8	1.5		
15	42.0	62.8	1.0		
C 16	45.4	63.9	1.2		
FIRST CLOSED-IN					
C 1	0.0	63.9			
2	1.0	476.2	412.3	1.0	1.651
3	2.0	747.5	683.6	1.9	1.369
4	3.0	910.1	846.1	2.8	1.209
5	4.0	1018.9	955.0	3.7	1.092
6	5.0	1085.6	1021.7	4.5	1.002
7	6.0	1120.7	1056.7	5.3	0.932
8	7.0	1141.8	1077.9	6.1	0.871
9	8.0	1153.5	1089.6	6.8	0.826
10	9.0	1161.9	1097.9	7.5	0.780
11	10.0	1168.1	1104.2	8.2	0.742
12	12.0	1174.9	1111.0	9.5	0.679
13	14.0	1179.9	1115.9	10.7	0.627
14	16.0	1183.9	1120.0	11.8	0.584
15	18.0	1186.5	1122.5	12.9	0.546
16	20.0	1188.7	1124.8	13.9	0.515
17	22.0	1190.8	1126.9	14.8	0.486
18	24.0	1192.6	1128.7	15.7	0.461
19	26.0	1193.9	1129.9	16.5	0.439
20	28.0	1195.1	1131.2	17.3	0.418
21	30.0	1196.4	1132.4	18.1	0.400
22	35.0	1198.3	1134.3	19.8	0.361
23	40.0	1199.9	1136.0	21.3	0.329
D 24	45.2	1200.8	1136.8	22.7	0.302
SECOND FLOW					
E 1	0.0	41.2			
2	5.0	57.0	15.9		
3	10.0	64.3	7.3		

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
4	15.0	68.3	4.1		
5	20.0	71.5	3.2		
6	25.0	74.0	2.4		
7	30.0	76.6	2.6		
8	35.0	78.5	1.9		
9	40.0	80.5	2.0		
10	45.0	82.6	2.0		
11	50.0	83.4	0.9		
12	55.0	85.5	2.0		
F 13	59.2	86.3	0.9		
SECOND CLOSED-IN					
F 1	0.0	86.3			
2	1.0	543.9	457.6	1.0	2.021
3	2.0	794.2	707.9	2.0	1.717
4	3.0	955.7	869.4	3.0	1.550
5	4.0	1038.7	952.3	3.9	1.429
6	5.0	1078.6	992.3	4.8	1.337
7	6.0	1104.0	1017.7	5.7	1.264
8	7.0	1115.6	1029.3	6.5	1.205
9	8.0	1125.7	1039.3	7.4	1.149
10	9.0	1134.7	1048.3	8.3	1.100
11	10.0	1139.7	1053.3	9.1	1.060
12	12.0	1147.6	1061.3	10.8	0.986
13	14.0	1158.2	1071.8	12.4	0.927
14	16.0	1160.9	1074.6	13.9	0.876
15	18.0	1164.0	1077.7	15.4	0.832
16	20.0	1166.3	1080.0	16.8	0.794
17	22.0	1168.4	1082.1	18.1	0.761
18	24.0	1171.1	1084.8	19.6	0.728
19	26.0	1173.1	1086.8	20.8	0.701
20	28.0	1174.8	1088.5	22.1	0.675
21	30.0	1176.8	1090.5	23.3	0.652
22	35.0	1180.1	1093.8	26.2	0.601
23	40.0	1183.3	1096.9	28.9	0.558
24	45.0	1185.9	1099.6	31.5	0.522
25	50.0	1187.9	1101.6	33.8	0.490
26	55.0	1189.4	1103.1	36.1	0.462
27	60.0	1190.7	1104.4	38.1	0.438
28	70.0	1192.9	1106.6	41.9	0.397
29	80.0	1195.1	1108.8	45.3	0.363
G 30	90.2	1197.1	1110.8	48.4	0.334

LEGEND:

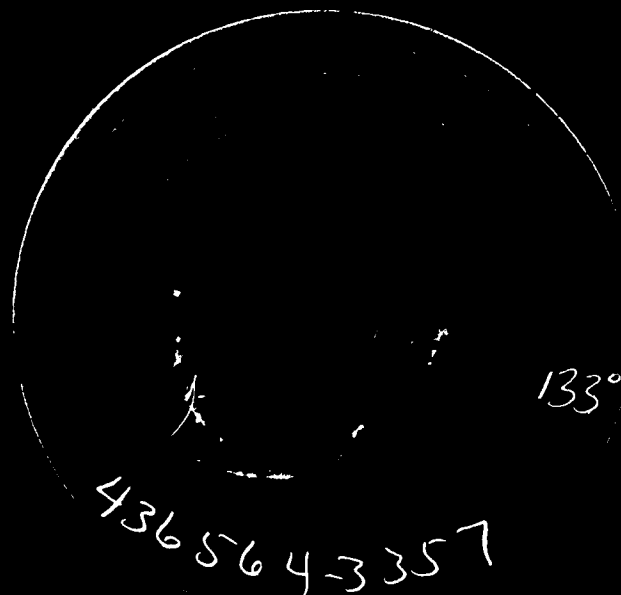
☐ STAIR-STEP

REMARKS:

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	3895.0	
3		DRILL COLLARS.....	6.250	2.250	120.0	
50		IMPACT REVERSING SUB.....	6.000	2.750	1.0	4015.0
3		DRILL COLLARS.....	6.250	2.250	120.0	
5		CROSSOVER.....	6.000	2.250	1.0	
12		DUAL CIP VALVE.....	5.000	0.870	6.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	4147.0
80		AP RUNNING CASE.....	5.000	2.250	4.0	4149.0
15		JAR.....	5.000	1.750	5.0	
16		VR SAFETY JOINT.....	5.000	1.000	3.0	
70		OPEN HOLE PACKER.....	6.750	1.530	6.0	4164.0
70		OPEN HOLE PACKER.....	6.750	1.530	6.0	4170.0
20		FLUSH JOINT ANCHOR.....	5.000	2.370	28.0	
83		HT-500 TEMPERATURE CASE.....	5.000		1.0	4200.0
81		BLANKED-OFF RUNNING CASE.....	5.000		4.0	4202.0
TOTAL DEPTH					4205.0	

EQUIPMENT DATA

TEMPERATURE RECORDER CHART



10° each circle

EQUATIONS FOR DST GAS WELL ANALYSIS

Indicated Flow
Capacity

$$kh = \frac{.001637 Q_g T}{m}$$

md-ft

Average Effective
Permeability

$$k = \frac{kh}{h}$$

md

Skin Factor

$$S = 1.151 \left[\frac{m(P^*) - m(P_i)}{m} - \text{LOG} \left(\frac{k(t/60)}{\phi \mu c_i r_w^2} \right) + 3.23 \right]$$

Damage Ratio

$$DR = \frac{m(P^*) - m(P_i)}{m(P^*) - m(P_i) - 0.87 mS}$$

Indicated Flow
Rate (Maximum)

$$AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_i)}$$

MCFD

Indicated Flow
Rate (Minimum)

$$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_i)}}$$

MCFD

Approx. Radius of
Investigation

$$r_i = 0.032 \sqrt{\frac{k(t/60)}{\phi \mu c_i}}$$

ft