





### Pressure Breakdown Data

Date 12-19-63

Field Report No. 12312 A

Recorder No. T-864 Capacity 5000#

Recorder Depth 4426'

Recorder Run INSIDE Clock Travel 0.02095 inches per min.

Well Temperature 125 °F.

| Point                     | Pressure | Time Given | Time Computed |
|---------------------------|----------|------------|---------------|
| A Initial Hydrostatic Mud | 2365     |            |               |
| B Initial Shut-in         | 1508     |            |               |
| C Initial Flow            | 74       |            |               |
| D Final Flow              | 192      |            |               |
| E Final Shut-in           | 1453     |            |               |
| F Final Hydrostatic Mud   | 2359     |            |               |

|                 |          |    |       |
|-----------------|----------|----|-------|
| Opened Tool     | 0202     |    |       |
| Initial Flow    | 10 Mins. | 10 | Mins. |
| Initial Shut-in | 30 Mins. | 31 | Mins. |
| Final Flow      | 30 Mins. | 29 | Mins. |
| Final Shut-in   | 30 Mins. | 30 | Mins. |

C-1 105  
C-2 113

Remarks:

#### PRESSURE INCREMENTS

##### INITIAL SHUT-IN

##### FINAL SHUT-IN

Breakdown: \_\_\_\_\_ increments of \_\_\_\_\_ mins. and a final increment of \_\_\_\_\_ mins.

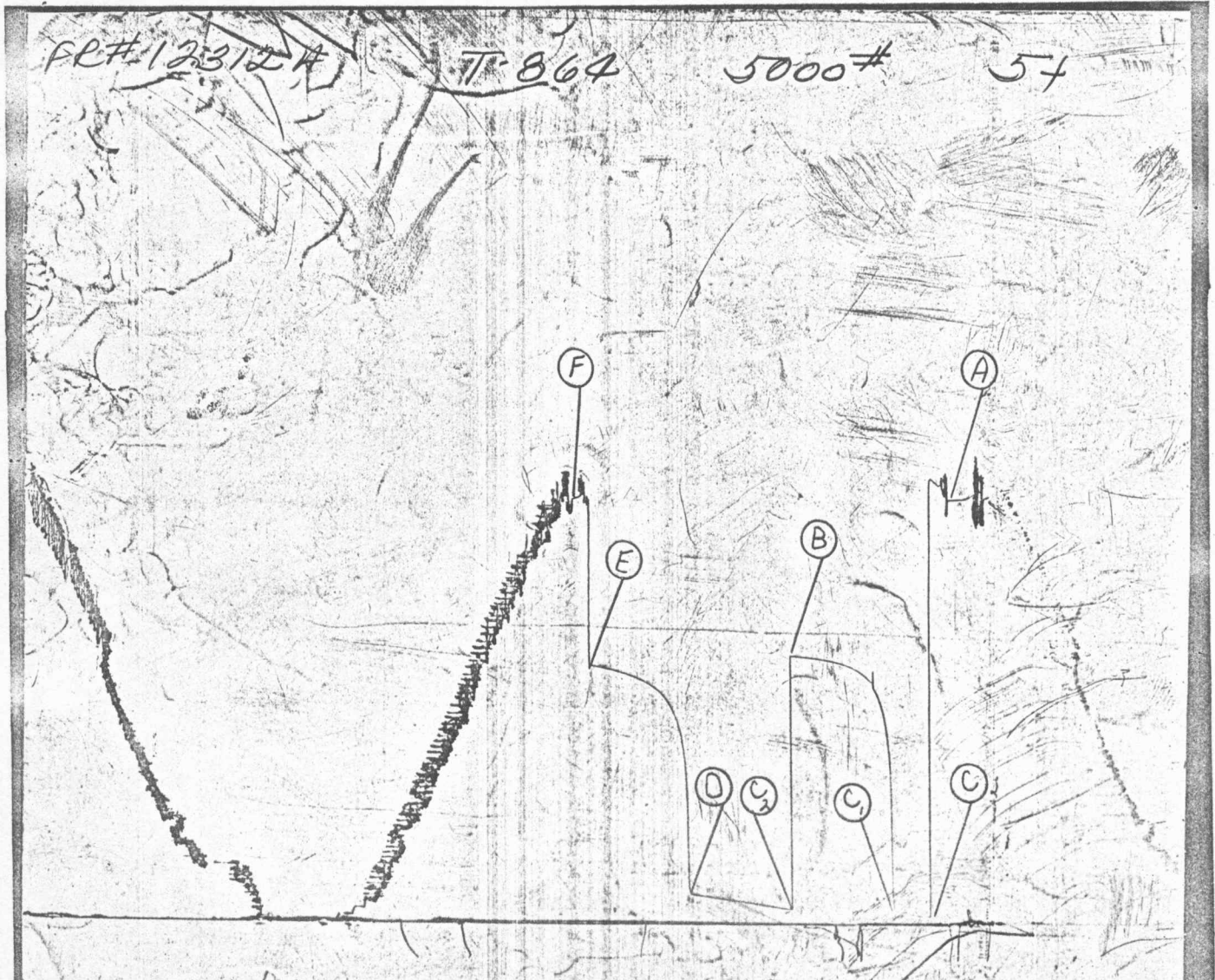
Breakdown: 10 increments of 3 mins. and a final increment of 1 mins.

Breakdown: 10 increments of 3 mins. and a final increment of - mins.

| Point Minutes | Pressure | $\frac{T + \Delta t}{\Delta t}$ | Point Minutes | Pressure | $\frac{T + \Delta t}{\Delta t}$ | Point Minutes | Pressure | $\frac{T + \Delta t}{\Delta t}$ |
|---------------|----------|---------------------------------|---------------|----------|---------------------------------|---------------|----------|---------------------------------|
|               |          |                                 | C-1 0         | 105      |                                 | D 0           | 192      |                                 |
|               |          |                                 | 3             | 1062     |                                 | 3             | 1023     |                                 |
|               |          |                                 | 6             | 1294     |                                 | 6             | 1209     |                                 |
|               |          |                                 | 9             | 1393     |                                 | 9             | 1297     |                                 |
|               |          |                                 | 12            | 1432     |                                 | 12            | 1344     |                                 |
|               |          |                                 | 15            | 1459     |                                 | 15            | 1376     |                                 |
|               |          |                                 | 18            | 1477     |                                 | 18            | 1400     |                                 |
|               |          |                                 | 21            | 1488     |                                 | 21            | 1417     |                                 |
|               |          |                                 | 24            | 1495     |                                 | 24            | 1432     |                                 |
|               |          |                                 | 27            | 1502     |                                 | 27            | 1444     |                                 |
|               |          |                                 | 30            | 1506     |                                 | E 30          | 1453     |                                 |
|               |          |                                 | B 31          | 1508     |                                 |               |          |                                 |

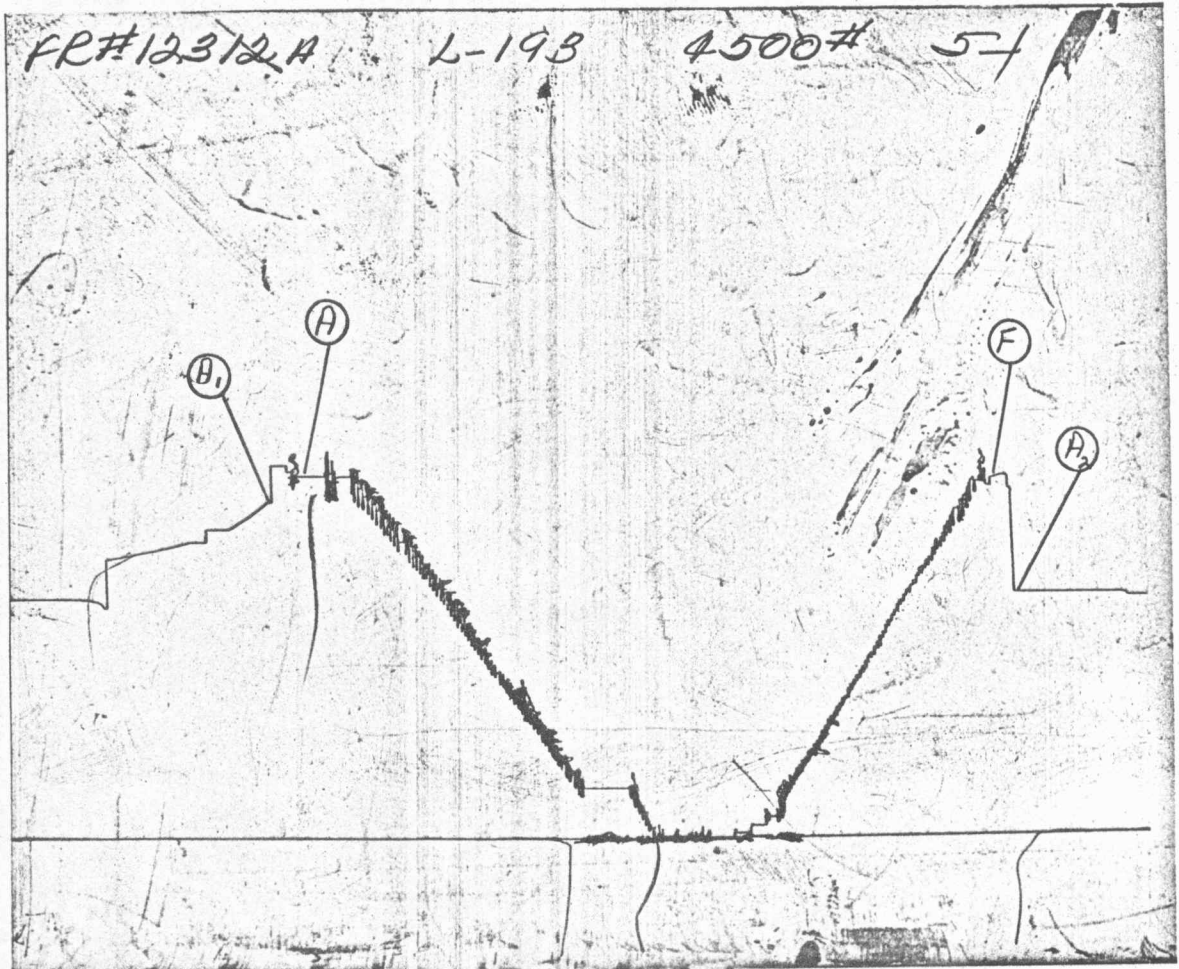
|                              |         |        |  |  |
|------------------------------|---------|--------|--|--|
| Recorder No.                 | T-864   | INSIDE |  |  |
| Capacity (P.S.I.G.)          | 5000    |        |  |  |
| Recorder Depth               | 4426'   |        |  |  |
| Pressure Gradient P.S.I./Ft. |         |        |  |  |
| Well Temperature °F.         | 125     |        |  |  |
| A Initial Hydrostatic Mud    | 2365    |        |  |  |
| B Initial Shut-in            | *1508   |        |  |  |
| C Initial Flow               | 74      |        |  |  |
| D Final Flow                 | 192     |        |  |  |
| E Final Shut-in              | *1453   |        |  |  |
| F Final Hydrostatic Mud      | 2359    |        |  |  |
| Remarks:                     | C-1 105 |        |  |  |
|                              | C-2 113 |        |  |  |

\*Shut in pressure did not reach static reservoir pressure.



|                                  |                 |         |  |  |
|----------------------------------|-----------------|---------|--|--|
| Recorder No.                     | L-193           | OUTSIDE |  |  |
| Capacity (P.S.I.G.)              | 4500            |         |  |  |
| Recorder Depth                   | 4440'           |         |  |  |
| Pressure Gradient P.S.I./Ft.     |                 |         |  |  |
| Well Temperature °F.             | 125             |         |  |  |
| <b>A Initial Hydrostatic Mud</b> | <b>2508</b>     |         |  |  |
| B Initial Shut-in                | -               |         |  |  |
| C Initial Flow                   | -               |         |  |  |
| D Final Flow                     | -               |         |  |  |
| E Final Shut-in                  | -               |         |  |  |
| F Final Hydrostatic Mud          | 2481            |         |  |  |
| Remarks:                         | A-1 2327        |         |  |  |
|                                  | A-2 1687        |         |  |  |
|                                  | BELOW STRADDLE. |         |  |  |

\*Shut in pressure did not reach static reservoir pressure.



1 HOUR

FINAL HYDROSTATIC

2359 #

FINAL SHUT IN

1453 #

FINAL FLOW

192 #

INITIAL HYDROSTATIC

2365 #

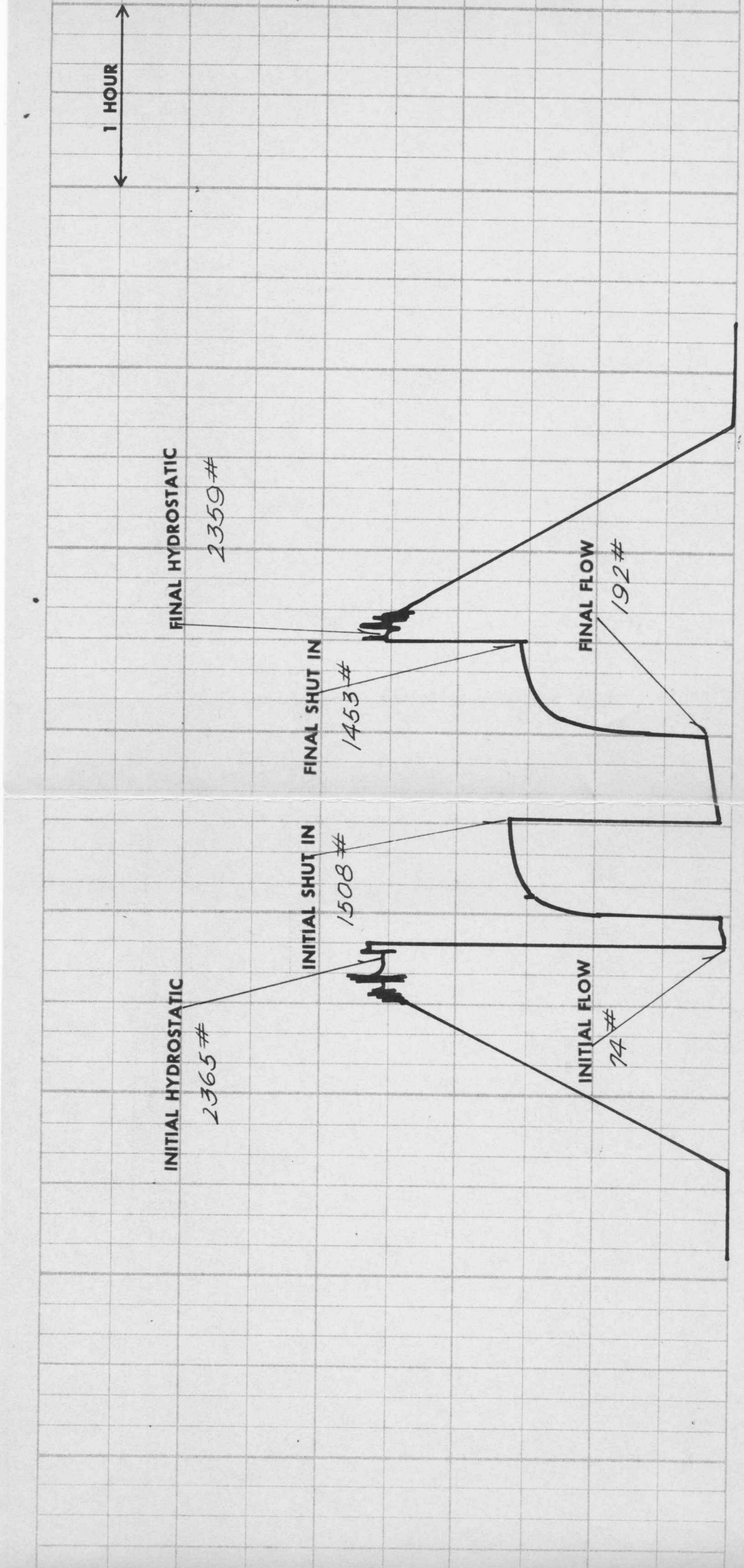
INITIAL SHUT IN

1508 #

INITIAL FLOW

74 #

TIME







### Pressure Breakdown Data

Date 12-19-63

Field Report No. 12313 A

Recorder No. T-864 Capacity 5000#

Recorder Depth 4326'

Recorder Run INSIDE Clock Travel 0.02034 inches per min.

Well Temperature 128 °F.

| Point                     | Pressure | Time Given | Time Computed |
|---------------------------|----------|------------|---------------|
| A Initial Hydrostatic Mud | 2319     |            |               |
| B Initial Shut-in         | 964      |            |               |
| C Initial Flow            | 433      |            |               |
| D Final Flow              | 945      |            |               |
| E Final Shut-in           | 958      |            |               |
| F Final Hydrostatic Mud   | 2307     |            |               |

|                 |          |    |       |
|-----------------|----------|----|-------|
| Opened Tool     | 0830     |    |       |
| Initial Flow    | 10 Mins. | 10 | Mins. |
| Initial Shut-in | 30 Mins. | 30 | Mins. |
| Final Flow      | 60 Mins. | 60 | Mins. |
| Final Shut-in   | 60 Mins. | 60 | Mins. |

C-1 569

C-2 611

Remarks: \_\_\_\_\_

#### PRESSURE INCREMENTS

##### INITIAL SHUT-IN

##### FINAL SHUT-IN

Breakdown: \_\_\_\_\_ increments of \_\_\_\_\_ mins. and a final increment of \_\_\_\_\_ mins.

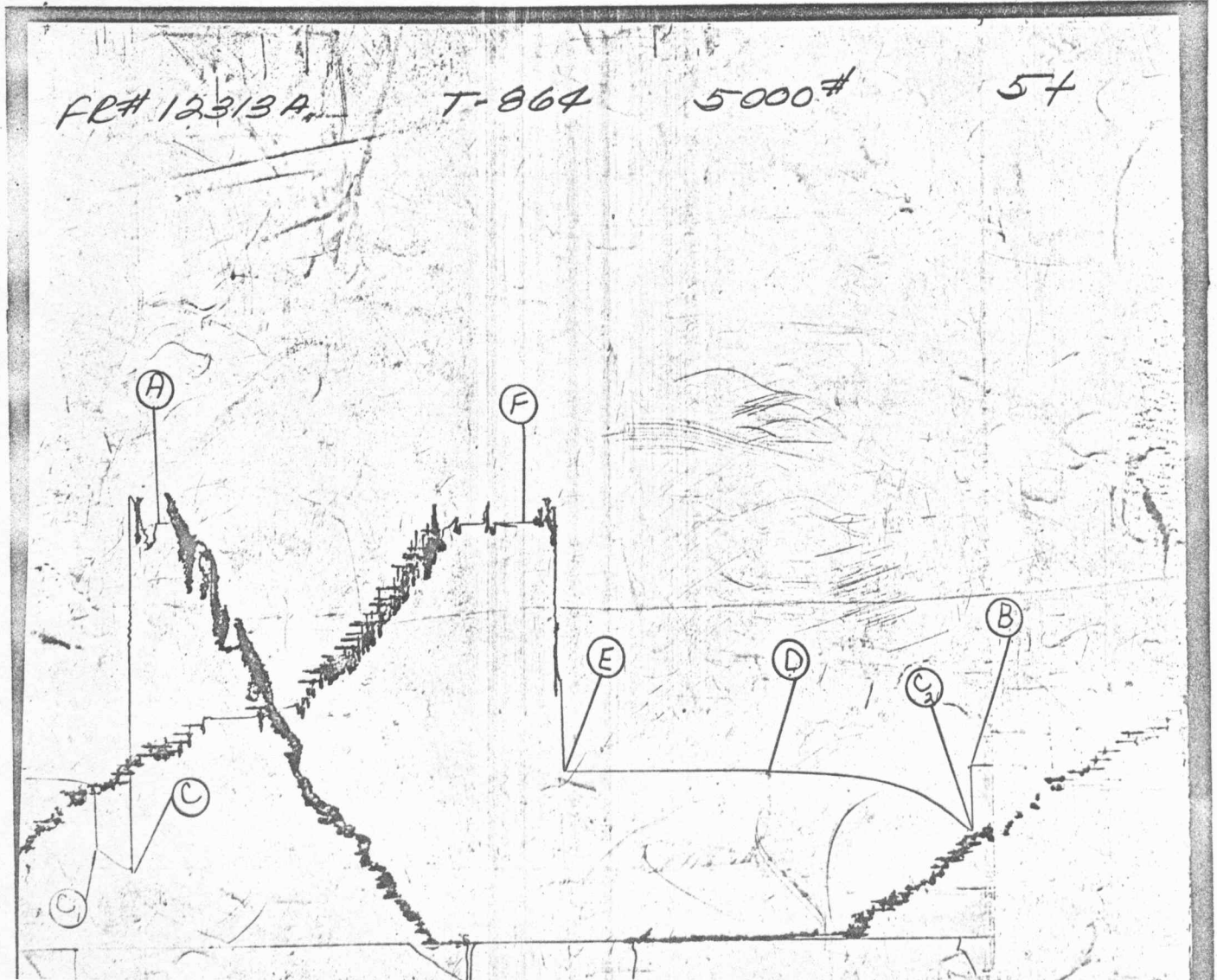
Breakdown: 10 increments of 3 mins. and a final increment of - mins.

Breakdown: 12 increments of 5 mins. and a final increment of - mins.

| Point Minutes | Pressure | $\frac{T + \Delta t}{\Delta t}$ | Point Minutes | Pressure | $\frac{T + \Delta t}{\Delta t}$ | Point Minutes | Pressure | $\frac{T + \Delta t}{\Delta t}$ |
|---------------|----------|---------------------------------|---------------|----------|---------------------------------|---------------|----------|---------------------------------|
|               |          |                                 | C-1 0         | 569      |                                 | D 0           | 945      |                                 |
|               |          |                                 | 3             | 927      | 4.333                           | 5             | 951      | 15.000                          |
|               |          |                                 | 6             | 937      | 2.666                           | 10            | 953      | 8.000                           |
|               |          |                                 | 9             | 944      | 2.111                           | 15            | 954      | 5.667                           |
|               |          |                                 | 12            | 951      | 1.834                           | 20            | 954      | 4.500                           |
|               |          |                                 | 15            | 954      | 1.667                           | 25            | 955      | 3.800                           |
|               |          |                                 | 18            | 956      | 1.555                           | 30            | 956      | 3.333                           |
|               |          |                                 | 21            | 958      | 1.476                           | 35            | 956      | 3.000                           |
|               |          |                                 | 24            | 961      | 1.417                           | 40            | 956      | 2.750                           |
|               |          |                                 | 27            | 963      | 1.370                           | 45            | 956      | 2.556                           |
|               |          |                                 | B 30          | 964      | 1.333                           | 50            | 957      | 2.400                           |
|               |          |                                 |               |          |                                 | 55            | 957      | 2.273                           |
|               |          |                                 |               |          |                                 | E 60          | 958      | 2.167                           |

|                              |       |        |  |  |
|------------------------------|-------|--------|--|--|
| Recorder No.                 | T-864 | INSIDE |  |  |
| Capacity (P.S.I.G.)          | 5000  |        |  |  |
| Recorder Depth               | 4326' |        |  |  |
| Pressure Gradient P.S.I./Ft. |       |        |  |  |
| Well Temperature °F.         | 128   |        |  |  |
| A Initial Hydrostatic Mud    | 2319  |        |  |  |
| B Initial Shut-in            | * 964 |        |  |  |
| C Initial Flow               | 433   |        |  |  |
| D Final Flow                 | 945   |        |  |  |
| E Final Shut-in              | * 958 |        |  |  |
| F Final Hydrostatic Mud      | 2307  |        |  |  |
| Remarks:                     | C-1   | 569    |  |  |
|                              | C-2   | 611    |  |  |

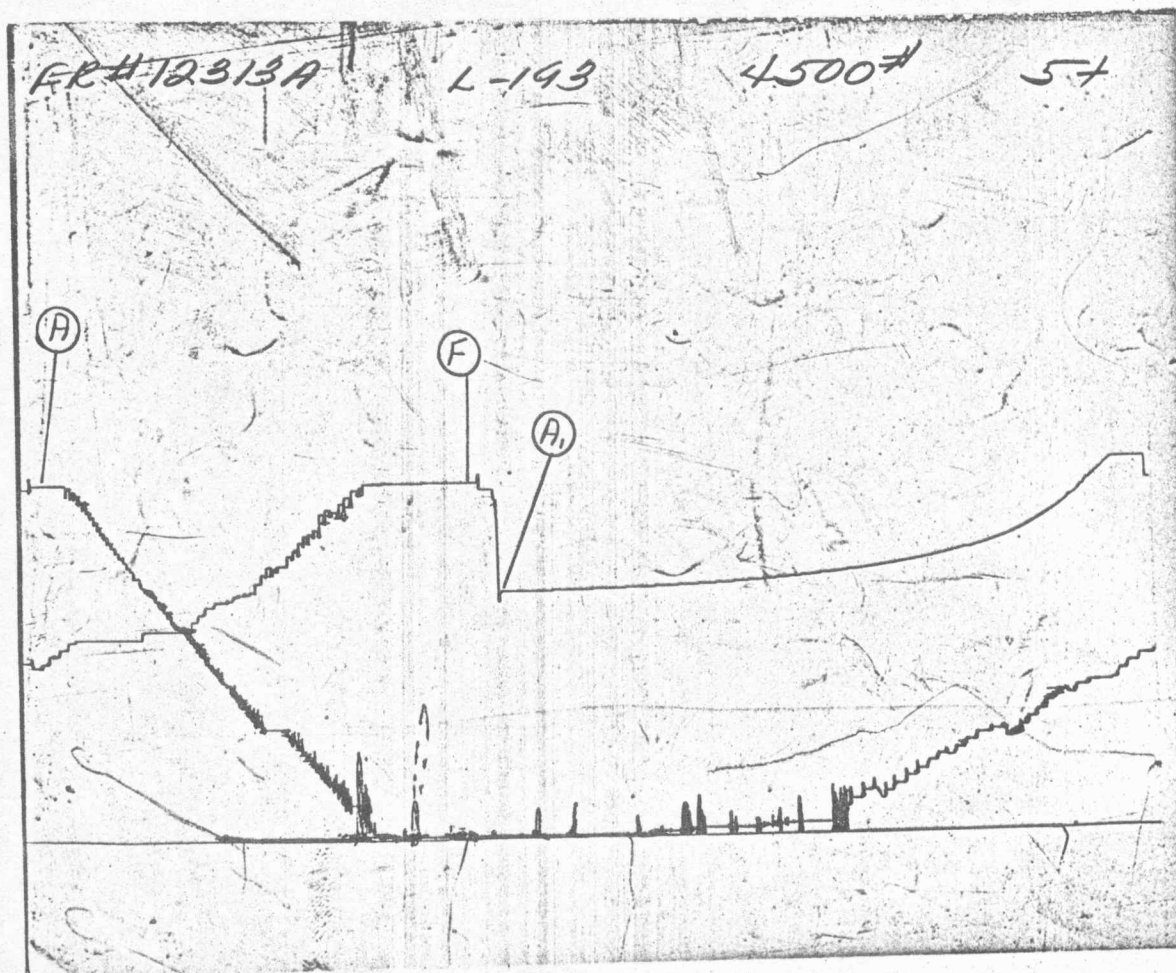
\*Shut in pressure did not reach static reservoir pressure.



|                                  |             |         |  |  |
|----------------------------------|-------------|---------|--|--|
| Recorder No.                     | L-193       | OUTSIDE |  |  |
| Capacity (P.S.I.G.)              | 4500        |         |  |  |
| Recorder Depth                   | 4342'       |         |  |  |
| Pressure Gradient P.S.I./Ft.     |             |         |  |  |
| Well Temperature °F.             | 128         |         |  |  |
| <b>A</b> Initial Hydrostatic Mud | <b>2444</b> |         |  |  |
| B Initial Shut-in                | -           |         |  |  |
| C Initial Flow                   | -           |         |  |  |
| D Final Flow                     | -           |         |  |  |
| E Final Shut-in                  | -           |         |  |  |
| F Final Hydrostatic Mud          | 2439        |         |  |  |
| Remarks:                         | A-1         | 1686    |  |  |

BELOW STRADDLE.

\*Shut in pressure did not reach static reservoir pressure.



## Assumptions made for Calculations for Liquid Recoveries

1. Q is taken as steady state flow.
2.  $P_f$  is formation flowing pressure at steady state flow.
3. Formation flow is taken as single phase flow.  
If gas is produced at surface, phase separation is assumed to have occurred in drill pipe.
4. Radial flow is assumed.
5. For the purpose of calculating EDR where specific reservoir parameters are not available it is assumed that:

|  |                                      |
|--|--------------------------------------|
| Effective permeability, K, will fall between .....   | 1 to 200 md                          |
| Formation porosity, $\phi$ , will fall between ..... | 0.1 to 0.3                           |
| Fluid compressibility, $c$ , will fall between ..... | $10^{-6}$ to $10^{-4}$               |
| Fluid viscosity, $\mu$ , will fall between .....     | 0.05 to 50 cp.                       |
| Well bore radius, $r_w$ , will fall between .....    | $3\frac{7}{8}$ " to $4\frac{3}{8}$ " |

Which gives an average value for the function  $\log \frac{K}{\phi \mu c r_w^2}$  of ..... 5.5

6. Other standard radial flow, steady state assumptions.

### Empirical Equations:

$$1. \text{ EDR} = \frac{P_o - P_f}{M(\log T + 2.65)}$$

$$2. \text{ Transmissibility } \frac{Kh}{\mu B} = \frac{162.6Q}{M}$$

$$3. \text{ P.I.} = \frac{Q}{P_o - P_f}$$

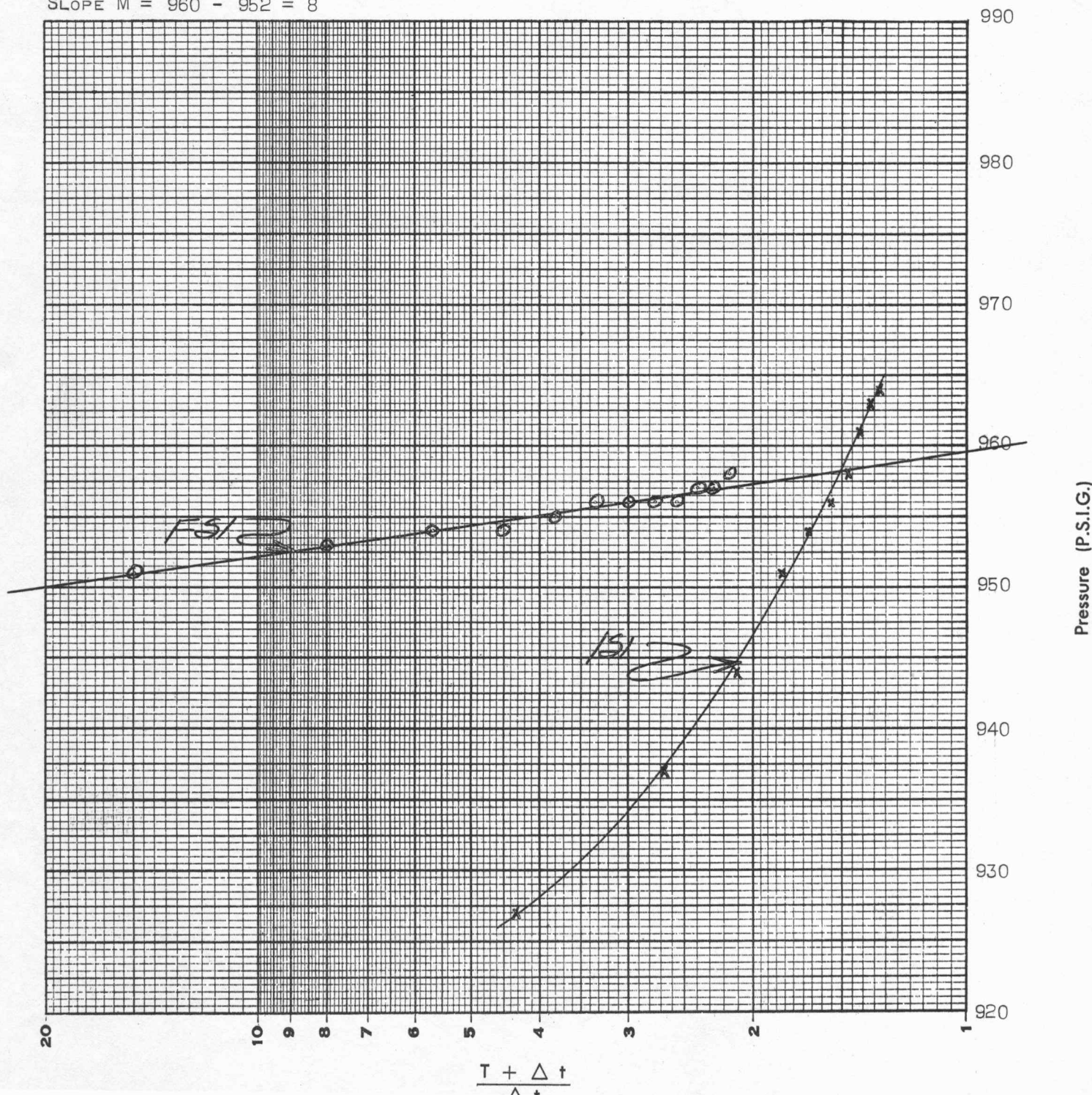
$$4. \text{ P.S.} = \left[ P_o \times 2.309 \text{ ft./PSI} \right] - \left[ \text{Recorder depth to sea level.} \right]$$

| Symbols      | Dimensions                                | Symbols                                | Dimensions                                    |
|--------------|---|--|---|
| B            | Formation volume factor                   | Q                                      | Rate of flow during test                      |
| c            | Fluid compressibility                     | Q <sub>o</sub>                         | Rate of oil flow during test                  |
| EDR          | Estimated damage ratio                    | Q <sub>w</sub>                         | Rate of water flow during test                |
| $\phi$       | Formation porosity                        | Q <sub>g</sub>                         | Rate of gas flow during test                  |
| h            | Net producing interval                    | $r_w$                                  | Well bore radius                              |
| J            | Productivity index                        | t                                      | Shut-in time period                           |
| K            | Permeability                              | $\Delta t$                             | Increment time of shut-in                     |
| M            | Slope of shut-in build up                 |  | period  |
| $P_f$        | Final flowing pressure                    | T                                      | Open flow time period                         |
| $P_{f_{si}}$ | Final shut-in pressure at time t          | $^{\circ}T_f$                          | Formation temperature                         |
| $P_{isi}$    | Initial shut-in pressure                  | $\mu$                                  | Fluid viscosity                               |
| $P_o$        | Maximum reservoir pressure                |  | (Reservoir Conditions)                        |
| $P_1$        | Final shut-in buildup plot intercept @ 1  | Z                                      | Gas deviation factor (Compressibility factor) |
| $P_{10}$     | Final shut-in buildup plot intercept @ 10 | $\frac{Kh}{\mu B}$ or $\frac{Kh}{\mu}$ | Transmissibility factor                       |
| P.S.         | Potentiometric surface                    |  | $\frac{\text{Md.} - \text{ft.}}{\text{Cp.}}$  |

In making any interpretation, our employees will give Customer the benefit of their best judgment as to the correct interpretation. Nevertheless, since all interpretations are opinions based on inferences from electrical, mechanical or other measurements, we cannot, and do not guarantee the accuracy or correctness of any interpretations, and we shall not be liable or responsible, except in the case of gross or wilful negligence on our part, for any loss, costs, damages or expenses incurred or sustained by Customer resulting from any interpretation made by any of our agents or employees.

|   |       |       |               |                            |                    |       |                      |
|---|-------|-------|---------------|----------------------------|--------------------|-------|----------------------|
| Estimated Damage Ratio                          | EDR   | 0.42  |               | Effective Transmissibility | $\frac{Kh}{\mu B}$ | 15154 | $\frac{Md-ft.}{Cp.}$ |
| Maximum Reservoir Pressure                      | $P_o$ | 960   | P.S.I.G.      | Effective Transmissibility | $\frac{Kh}{\mu B}$ |       | $\frac{Md-ft.}{Cp.}$ |
| Slope of Shut-in Curve                          | M     | 8     | PSI/log cycle | Flow Rate                  | OIL                | Q     | 745.66 Bbl./day      |
| Potentiometric Surface (Datum Plane, Sea Level) | PS    | -200  | ft.           | Flow Rate                  |                    | Q     | Bbl./day             |
| Productivity Index                              | PI    | 49.71 | Bbl./day/PSI  | Gas Oil Ratio              |                    | GOR   | CF/Bbl.              |
| Radius of Investigation                         |       | -     | ft.           | K (Effective to OIL )      |                    | 2020  | Md.                  |

SLOPE M = 960 - 952 = 8



## SPECIAL DATA ANALYSIS

DECEMBER 26, 1963

THIS APPEARS TO BE A POOR MECHANICAL DRILL STEM TEST DURING WHICH THE TOOLS MAY NOT HAVE FUNCTIONED PROPERLY. WELL CONDITIONS WERE SATISFACTORY AND THE FORMATION WITHIN THE TEST INTERVAL DID PRODUCE ENOUGH RESERVOIR FLUID FOR PROPER IDENTIFICATION. SUFFICIENT RESERVOIR PRESSURE DRAWDOWN DID OCCUR FOR ADEQUATE SHUT-IN BUILD-UPS FOR RELIABLE SPECIAL DATA ANALYSIS. THE LENGTHS OF TIME OF THE FLOW PERIODS AND SHUT-IN PERIODS OF THIS TEST ARE SUFFICIENT. THE DATA OBTAINED SHOULD BE ADEQUATE FOR RELIABLE SPECIAL DATA ANALYSIS. BOTH THE INITIAL AND FINAL SHUT-IN BUILD-UPS MAY BE EFFECTED BY A SMALL LEAK AROUND THE BOTTOM PACKER.

1. RESERVOIR PRESSURE: EXTRAPOLATION OF THE FINAL SHUT-IN PRESSURE BUILD-UP PLOT INDICATES A MAXIMUM RESERVOIR PRESSURE OF 960 P.S.I.G. AT RECORDER DEPTH.
2. PERMEABILITY: THE CALCULATED TRANSMISSIBILITY FACTOR OF 15154 MD.-FT./CP. INDICATES AN AVERAGE EFFECTIVE PERMEABILITY TO OIL OF 2020 MD. FOR THE REPORTED 7.5 FOOT POROUS INTERVAL. THIS VALUE WAS CALCULATED ASSUMING THE PRODUCT OF THE OIL VISCOSITY AND FORMATION VOLUME FACTOR TO BE 1.0.
3. WELL BORE DAMAGE: THE CALCULATED ESTIMATED DAMAGE RATIO OF 0.42 INDICATES THAT NO WELL BORE DAMAGE IS PRESENT AT THE TIME AND CONDITIONS OF THIS TEST.
4. GENERAL COMMENTS: THIS APPEARS TO BE A TEST OF AN EXCELLENT PERMEABILITY OIL ZONE WHICH ALSO CONTAINS SOME WATER. THE WELL WILL NOT FLOW, BUT A PUMPER CAPABLE OF MAKING ITS ALLOWABLE SHOULD BE POSSIBLE IF THE WATER PRODUCTION CAN BE TOLERATED.

THE INITIAL PRESSURES ARE BEING EFFECTED BY A BOTTOM PACKER LEAK. THE FINAL PRESSURE MAY ALSO BE EFFECTED BY THIS LEAK.



JAMES D. HILLHOUSE  
EVALUATION ENGINEER

1 HOUR

FINAL HYDROSTATIC  
2307#

2307#

FINAL FLOW  
945#

945#

FINAL SHUT IN  
958#

958#

INITIAL HYDROSTATIC  
2319#

2319#

INITIAL SHUT IN  
964#

964#

INITIAL FLOW  
433#

433#

TIME

