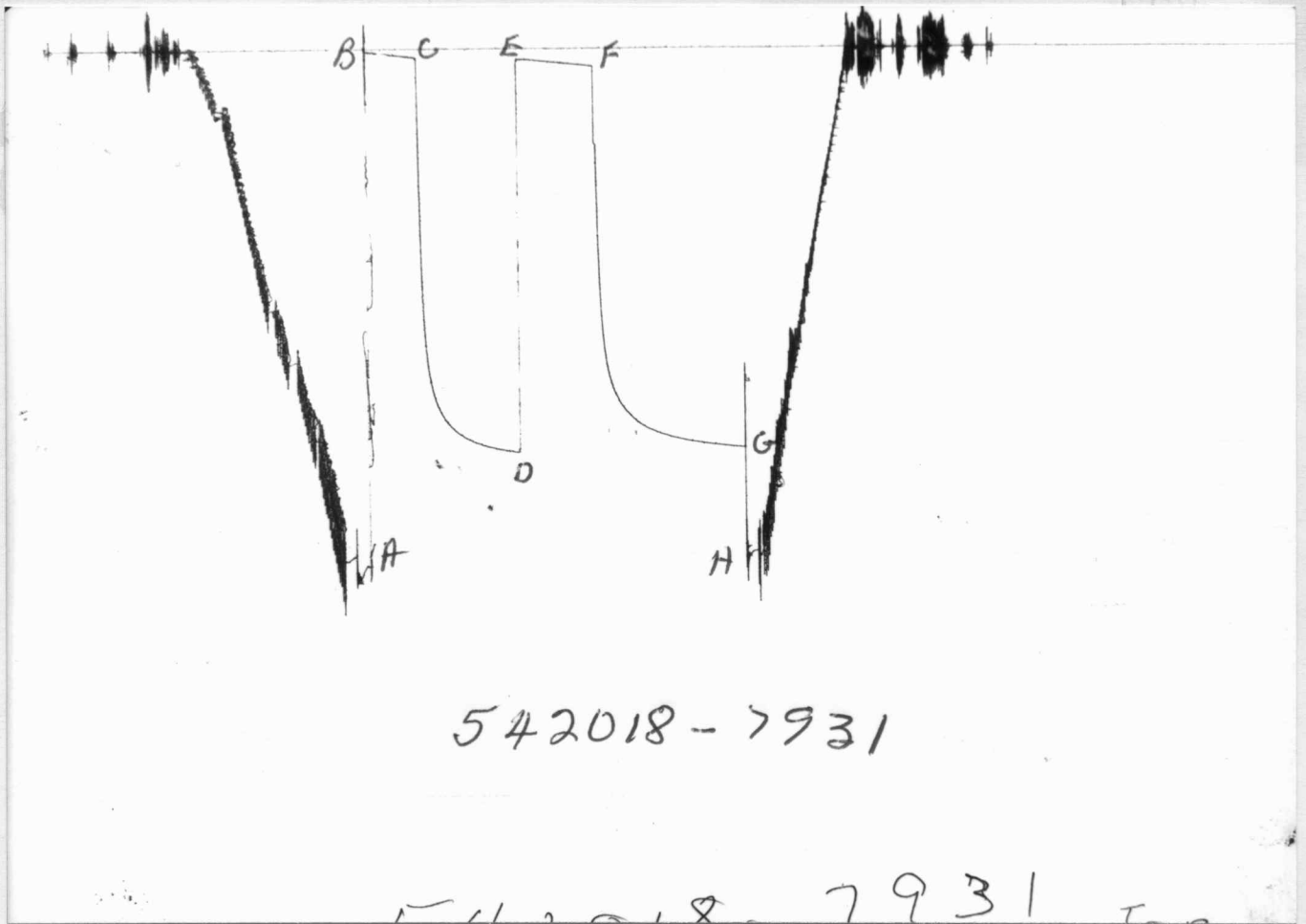




TICKET NO. 54201800
 29-DEC-82
 PRATT

FORMATION TESTING SERVICE REPORT

LEGAL LOCATION SEC. - TWP. - RNG.	11-32-21	WELL NO.	1	TEST NO.	1	TESTED INTERVAL	4209.1 - 4253.1	WELLS ENERGY CORPORATION LEASE OWNER/COMPANY NAME
				FIELD AREA		COUNTY	CLARK	STATE KANSAS DRBC

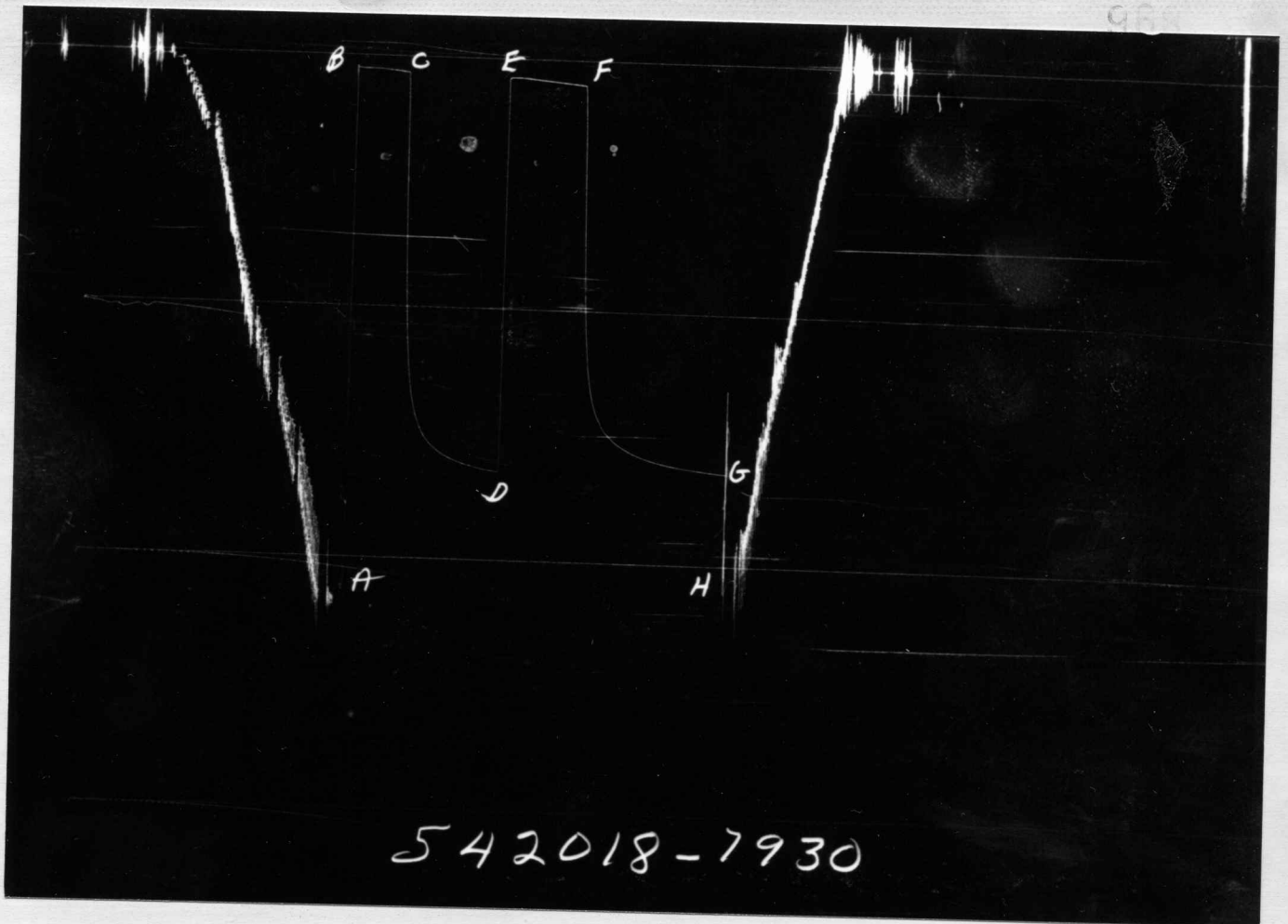


542018-7931

542018-7931

GAUGE NO: 7931 DEPTH: 4188.0 BLANKED OFF: NO HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		2037.3			
B	INITIAL FIRST FLOW		12.3			
C	FINAL FIRST FLOW		35.7	30.0	30.9	F
C	INITIAL FIRST CLOSED-IN		35.7			
D	FINAL FIRST CLOSED-IN		1625.7	60.0	58.8	C
E	INITIAL SECOND FLOW		49.1			
F	FINAL SECOND FLOW		72.2	45.0	46.4	F
F	INITIAL SECOND CLOSED-IN		72.2			
G	FINAL SECOND CLOSED-IN		1609.9	90.0	88.9	C
H	FINAL HYDROSTATIC		2025.1			



GAUGE NO: 7930 DEPTH: 4250.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	2044	2059.8			
B	INITIAL FIRST FLOW	40	49.5			
C	FINAL FIRST FLOW	70	65.4	30.0	30.9	F
C	INITIAL FIRST CLOSED-IN	70	65.4			
D	FINAL FIRST CLOSED-IN	1638	1649.1	60.0	58.8	C
E	INITIAL SECOND FLOW	80	81.6			
F	FINAL SECOND FLOW	100	100.1	45.0	46.4	F
F	INITIAL SECOND CLOSED-IN	100	100.1			
G	FINAL SECOND CLOSED-IN	1628	1634.1	90.0	88.9	C
H	FINAL HYDROSTATIC	2044	2051.4			

EQUIPMENT & HOLE DATA

FORMATION TESTED: TORONTO

NET PAY (ft): 10.0

GROSS TESTED FOOTAGE: 44.0

ALL DEPTHS MEASURED FROM: KB

CASING PERFS. (ft): _____

HOLE OR CASING SIZE (in): 7.875

ELEVATION (ft): 1941

TOTAL DEPTH (ft): 4253.0

PACKER DEPTH(S) (ft): 4203, 4209

FINAL SURFACE CHOKE (in): 1.000

BOTTOM HOLE CHOKE (in): 0.750

MUD WEIGHT (lb/gal): 9.20

MUD VISCOSITY (sec): 45

ESTIMATED HOLE TEMP. (°F): _____

ACTUAL HOLE TEMP. (°F): 98 @ 4248.0 ft

TICKET NUMBER: 54201800

DATE: 12-22-82 TEST NO: 1

TYPE DST: OPEN HOLE

HALLIBURTON CAMP: PRATT

TESTER: PARKER

WITNESS: MOORE

DRILLING CONTRACTOR: ALDEBARAN DRILLING COMPANY

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES
<u>TOP RECOVERY</u>	<u> </u> @ <u> </u> °F	<u>22000</u> ppm
<u>BOTTOM RECOVERY</u>	<u> </u> @ <u> </u> °F	<u>35500</u> ppm
<u>PIT SAMPLE</u>	<u> </u> @ <u> </u> °F	<u>23000</u> ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

SAMPLER DATA

Pstg AT SURFACE: _____

cu.ft. OF GAS: _____

cc OF OIL: _____

cc OF WATER: _____

cc OF MUD: _____

TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ @ _____ °F

GAS/OIL RATIO (cu.ft. per bbl): _____

GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____

RECOVERED:

125' OF DRILLING MUD

MEASURED FROM TESTER VALVE

REMARKS:

TIGHT HOLE INFORMATION.....

TICKET NO: 54201800
 CLOCK NO: 26864 HOUR: 12



GAUGE NO: 7931
 DEPTH: 4188.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	12.3			
2	5.0	14.3	2.0		
3	10.0	18.4	4.0		
4	15.0	23.4	5.1		
5	20.0	27.0	3.5		
6	25.0	31.0	4.0		
C 7	30.9	35.7	4.6		
FIRST CLOSED-IN					
C 1	0.0	35.7			
2	4.0	1237.2	1201.5	3.5	0.941
3	8.0	1391.5	1355.8	6.4	0.686
4	12.0	1465.4	1429.7	8.6	0.554
5	16.0	1507.3	1471.6	10.5	0.468
6	20.0	1536.2	1500.5	12.1	0.406
7	24.0	1556.7	1521.0	13.5	0.360
8	28.0	1573.5	1537.8	14.7	0.324
9	32.0	1584.3	1548.6	15.7	0.294
10	36.0	1594.0	1558.4	16.6	0.270
11	40.0	1602.4	1566.7	17.4	0.249
12	44.0	1609.2	1573.6	18.2	0.231
13	48.0	1614.8	1579.2	18.8	0.216
14	52.0	1619.4	1583.7	19.4	0.203
15	56.0	1625.0	1589.3	19.9	0.191
D 16	58.8	1625.7	1590.1	20.3	0.184
SECOND FLOW					
E 1	0.0	49.1			
2	9.0	46.8	-2.3		
3	18.0	53.0	6.3		
4	27.0	59.4	6.4		
5	36.0	65.8	6.4		
6	45.0	70.5	4.7		
F 7	46.4	72.2	1.7		
SECOND CLOSED-IN					
F 1	0.0	72.2			
2	6.0	1263.7	1191.5	5.6	1.143
3	12.0	1403.2	1331.0	10.4	0.871
4	18.0	1466.7	1394.5	14.6	0.725
5	24.0	1505.0	1432.7	18.3	0.625
6	30.0	1531.4	1459.2	21.6	0.553
7	36.0	1548.6	1476.4	24.6	0.498
8	42.0	1560.7	1488.5	27.2	0.454
9	48.0	1570.9	1498.7	29.6	0.417
10	54.0	1580.3	1508.1	31.8	0.386

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
11	60.0	1587.5	1515.3	33.8	0.360
12	66.0	1594.0	1521.8	35.6	0.337
13	72.0	1597.6	1525.4	37.3	0.317
14	78.0	1602.2	1530.0	38.8	0.299
15	84.0	1607.2	1534.9	40.3	0.283
G 16	88.9	1609.9	1537.7	41.4	0.272

REMARKS:

TICKET NO: 54201800
 CLOCK NO: 26754 HOUR: 12



















GAUGE NO: 7930
 DEPTH: 4250.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B	1	0.0	49.5		
	2	5.0	53.8	4.3	
	3	10.0	53.8	0.0	
	4	15.0	54.7	0.9	
	5	20.0	57.7	3.0	
	6	25.0	60.9	3.2	
C	7	30.9	65.4	4.5	
FIRST CLOSED-IN					
C	1	0.0	65.4		
	2	4.0	1260.9	1195.5	3.5 0.941
	3	8.0	1429.0	1363.6	6.4 0.686
	4	12.0	1497.7	1432.4	8.7 0.553
	5	16.0	1538.2	1472.9	10.5 0.468
	6	20.0	1561.9	1496.5	12.1 0.406
	7	24.0	1582.6	1517.2	13.5 0.359
	8	28.0	1597.4	1532.1	14.7 0.323
	9	32.0	1608.8	1543.4	15.7 0.294
	10	36.0	1618.5	1553.1	16.6 0.269
	11	40.0	1626.7	1561.3	17.5 0.249
	12	44.0	1633.2	1567.8	18.2 0.231
	13	48.0	1638.3	1573.0	18.8 0.216
	14	52.0	1643.3	1577.9	19.4 0.203
	15	56.0	1647.5	1582.2	19.9 0.191
D	16	58.8	1649.1	1583.7	20.3 0.184
SECOND FLOW					
E	1	0.0	81.6		
	2	9.0	75.2	-6.4	
	3	18.0	80.9	5.7	
	4	27.0	85.9	5.0	
	5	36.0	91.9	6.0	
	6	45.0	98.9	7.0	
F	7	46.4	100.1	1.2	
SECOND CLOSED-IN					
F	1	0.0	100.1		
	2	6.0	1284.3	1184.2	5.6 1.142
	3	12.0	1433.1	1333.0	10.4 0.873
	4	18.0	1493.7	1393.6	14.6 0.725
	5	24.0	1530.0	1429.9	18.3 0.626
	6	30.0	1553.0	1452.9	21.6 0.554
	7	36.0	1571.7	1471.6	24.6 0.498
	8	42.0	1584.8	1484.7	27.2 0.453
	9	48.0	1596.8	1496.7	29.6 0.417
	10	54.0	1605.6	1505.5	31.8 0.386

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
	11	60.0	1612.5	1512.4	33.8 0.360
	12	66.0	1618.5	1518.4	35.6 0.337
	13	72.0	1623.3	1523.2	37.3 0.317
	14	78.0	1627.1	1527.0	38.8 0.299
	15	84.0	1631.1	1531.0	40.3 0.283
G	16	88.9	1634.1	1534.0	41.4 0.272

REMARKS:

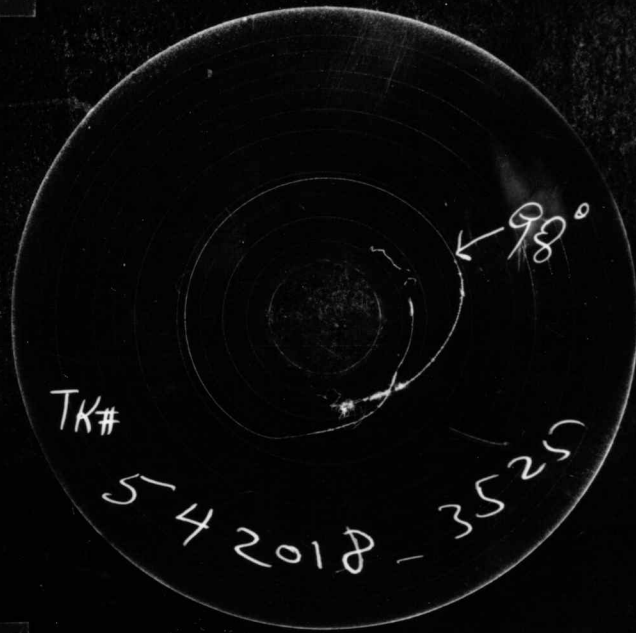
		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	3609.0	
3		DRILL COLLARS.....	6.250	2.250	436.0	
50		IMPACT REVERSING SUB.....	6.000	2.750	1.0	4045.0
3		DRILL COLLARS.....	6.250	2.250	125.0	
5		CROSSOVER.....	6.000	2.250	1.0	
11		HANDLING SUB & CHOKE ASSEMBLY...	5.750	3.750	5.0	
12		DUAL CIP VALVE.....	5.000	0.870	5.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	4186.0
80		AP RUNNING CASE.....	5.000	3.060	4.0	4188.0
15		JAR.....	5.000	1.750	5.0	
16		VR SAFETY JOINT.....	5.000	1.000	3.0	
70		OPEN HOLE PACKER.....	6.750	1.530	6.0	4203.0
70		OPEN HOLE PACKER.....	6.750	1.530	6.0	4209.0
20		FLUSH JOINT ANCHOR.....	5.000	2.370	36.0	
83		HT-500 TEMPERATURE CASE.....	5.000	2.440	2.0	4248.0
81		BLANKED-OFF RUNNING CASE.....	5.000	2.440	4.0	4250.0
TOTAL DEPTH					4253.0	

EQUIPMENT DATA

TEMPERATURE

RECORDER

CHART



10° each circle

Indicated Flow Capacity

$$kh = \frac{1637 Q_g T}{m}$$

md-ft

Average Effective Permeability

$$k = \frac{kh}{h}$$

md

Skin Factor

$$S = 1.151 \left[\frac{m(P^*) - m(P_f)}{m} - \text{LOG} \frac{kt}{\phi \mu c_t r_w^2} + 3.23 \right]$$

—

Damage Ratio

$$DR = \frac{m(P^*) - m(P_f)}{m(P^*) - m(P_f) - 0.87 mS}$$

—

Indicated Flow Rate (Maximum)

$$AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_f)}$$

MCFD

Indicated Flow Rate (Minimum)

$$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_f)}}$$

MCFD

Approx. Radius of Investigation

$$r_i = 0.032 \sqrt{\frac{kt}{\phi \mu c_t}}$$

ft