



CORE LABORATORIES

**ANADARKO PETROLEUM CORPORATION
BOEKHAUS TRUST NO. A-1
HUGOTON FIELD
MORTON COUNTY, KANSAS**

**CL FILE NO. 57151-18100
FINAL REPORT**



PETROLEUM SERVICES

December 7, 1994

Anadarko Petroleum Corporation
17001 Northchase
Houston, Texas 77060
Attn: Mr. Warren Winters

Re: Core Analysis Report
Boekhaus Trust No. A-1
Hugoton Field
Morton County, Kansas
CL File No. 57151-18100

Dear Mr. Winters:

Cores from the subject well were retrieved at the wellsite by Core Laboratories' personnel and transported to the Hollister Road facility in Houston. Analysis was performed as directed by representatives of Anadarko Petroleum Corporation.

The following documentation includes: procedures for sample preparation and petrophysical measurements; a list of Houston laboratory personnel involved in this project; and the resultant data reported in tabular and graphical format. The type of equipment used in each procedure is also specified.

We appreciate this opportunity to be of service. If we can be of further assistance, please do not hesitate to contact us.

Sincerely,

CORE LABORATORIES

A handwritten signature in cursive script, reading "Michael R. Long".

Michael R. Long
Laboratory Supervisor

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WELLSITE SERVICES

Personnel from Core Laboratories' Houston facility retrieved the core at the wellsite. The aluminum core barrel liner was wiped to remove drilling mud and marked with orientation lines and depth marks. An electric chop saw was used to cut the liner into 3 foot sections. All core material was then placed in a shipping crate and transported to the Hollister Road facility in Houston, where analysis was performed.

TOTAL CORE GAMMA

The core was removed from the aluminum liner, fitted together and depth labels were placed at one foot intervals. Orientation lines were also marked on the core surface. The natural total gamma radiation count of the core was then recorded as a function of depth. The instrument was calibrated against API standards and adjusted for background radiation.

SAMPLE PREPARATION

PLUG DRILLING and TRIMMING: Three (3) one-inch diameter plugs were drilled per foot in the interval from 2178.0 to 2196.0 feet. A plug was taken in each foot at 4 inch increments, starting at the foot mark. The remainder of the core, including shale sections, was sampled at a density of one plug per foot. All plugs were drilled in the same plane, parallel to maximum dip. The plugs were drilled and clipped using a 2% KCl solution as the drilling and trimming lubricant. The plugs were faced with a diamond facing tool to provide right circular cylinders. Plugs that appeared unstable or brittle were placed in lead sleeves with 60 mesh and 120 mesh stainless steel screens on each end. Trimmed ends for all plugs were catalogued and stored.

PLUG LEACHING: Samples were extracted of salts in a soxhlet extractor. Methanol was used as the leaching solvent. Extraction was continued until a test of the returning solvent with AgNO_3 solution yielded no precipitate. The methanol was maintained at approximately 150 degrees F. during the extraction process.

PLUG DRYING: Cleaned plugs were dried in a humidity oven at 140 degrees F. and 40% relative humidity until weight stabilization was achieved.

PETROPHYSICAL MEASUREMENTS

GRAIN VOLUME: Direct grain volume measurements were made using a small volume porosimeter. This instrument utilizes the principle of gas expansion as described by Boyle's law. Helium was used as the test gas. The instrument was calibrated daily and test standards were run.

GRAIN DENSITY: Calculated grain densities were obtained utilizing direct grain volume measurement and sample weight. Grain densities were checked against lithology standards.

PLUG DIMENSIONS: Sample lengths and diameters were measured using digital metric calipers.

CMS-300 ANALYSIS:

- A. **PERMEABILITY "k":** Permeability was measured by flowing helium from a reference cell at the selected pressure through the core. The size of the reference cell used is optimized during a pre-test flow through. The chambers available are approximately 2, 9, 56 and 315 cc's. The actual size of each cell is calculated during calibration procedures. The cell combination used varies with each sample. The downstream end of the core was maintained at atmospheric pressure. The upstream pressure decline was monitored in real time and recorded digitally. The difference between the confining stress and the mean pore pressure during flow is the net confining stress. The net confining stress used for this project was 800 psig.
 - 1. **K-air:** Permeability to air at 800 psig net confining stress was calculated from time pressure data.
 - 2. **K-Klinkenberg:** Unsteady state equations were used with time/pressure data to calculate the Klinkenberg slip corrected permeability at 800 psig net confining stress.
- B. **POROSITY:** Pore volume was determined by expansion of helium into the core sample from a known volume source at approximately 240 psig. At pressure equilibrium, Boyle's Law was used to compute pore volume. Porosity was then calculated by using the pore volume from the CMS-300 and the grain volume from the Small Volume Porosimeter.

OTHER SERVICES

CORE SLABBING: An automatic slab saw was used to cut the cores vertically into 1/3 - 2/3 sections. The core was oriented so that the slab face would expose the maximum bedding angle. Water was used as the blade coolant/lubricant.

CORE PHOTOGRAPHY: The 1/3 section of the slabbed core was photographed under white light conditions. A "box" format, which displays an entire slab box in an 8 x 10 photo, was used. Two sets of the completed photographs were delivered to Mr. Warren Winters.

THIN SECTION PREPARATION: Sixteen (16) standard 27mm x 46mm blue epoxy thin sections were prepared and delivered to Mr. Warren Winters.

The plugs and trim ends for samples 19, 20, 35, 48, 53 and 57 were shipped to Halliburton Research Center in Duncan, Oklahoma.



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 County : Morton County, Kansas

CL File No : 57151-18100

Date : 02-Nov-1994

Analyst : MJK/MRL

CMS - 300 ANALYSIS

Sample Number	Depth ft	NOB Pressure psig	Pore Volume cc	Porosity %	Kinf md	Kair(est) md	b(He) psi	BETA ft(-1)	ALPHA microns
Core Number One 2160.3 through 2222.35 feet									
1	2160.30		0.294 #	9.2 #	.51 *	0.78 *			
2	2162.30		1.933 #	9.1 #	.96 *	1.36 *			
3	2164.35		1.319 #	17.3 #	<.001 *	<.001 *			
4	2166.25		1.536 #	9.4 #	<.01 *	.01 *			
5	2168.50		1.385 #	7.1 #	1.18 *	1.63 *			
6	2170.35	800	1.85	7.9	0.010	0.022	115.09	2.93E+13	9.01E+02
7	2174.40	800	2.42	11.0	0.004	0.008	121.12	5.57E+16	6.38E+05
8	2176.80		1.172 #	14.1 #	<.001	<.001			
9	2178.00	800	3.36	15.3	0.081	0.138	51.96	2.79E+13	7.31E+03
10	2178.45	800	2.86	13.6	0.434	0.542	16.50	2.48E+11	3.49E+02
11	2178.70	800	3.11	13.7	0.038	0.077	78.68	1.41E+13	1.73E+03
12	2179.00	800	2.01	12.9	0.164	0.210	19.49	1.21E+11	6.46E+01
13	2179.50		2.870 #	7.3 #	.24 *	.40 *			
14	2179.70	800	4.54	22.9	1.876	2.641	24.56	4.57E+10	2.78E+02
15	2180.00	800	4.27	19.3	2.179	2.819	17.55	2.68E+10	1.89E+02
16	2180.35	800	3.39	15.0	0.094	0.161	52.70	6.41E+12	1.95E+03
17	2180.65	800	3.51	16.1	0.058	0.112	68.43	4.86E+13	9.20E+03
18	2181.00	800	3.94	17.9	2.123	2.719	16.79	2.22E+10	1.53E+02
19	2181.35	800	4.96	21.8	11.853	13.501	7.51	5.89E+08	2.26E+01
20	2181.70	800	4.34	19.5	18.808	20.815	5.62	2.24E+08	1.36E+01
21	2182.00	800	3.97	17.6	5.378	6.204	8.69	4.68E+09	8.15E+01
22	2182.35	800	3.29	14.9	0.716	0.914	17.73	4.43E+11	1.03E+03



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CMS - 300 ANALYSIS

Sample Number	Depth ft	NOB Pressure psig	Pore Volume cc	Porosity %	Kinf md	Kair(est) md	b(He) psi	BETA ft(-1)	ALPHA microns
23	2182.65	800	4.41	19.5	3.747	4.712	14.89	5.31E+09	6.44E+01
24	2183.10	800	4.71	21.6	3.775	4.696	14.05	5.23E+09	6.40E+01
25	2183.35	800	4.13	20.9	4.087	4.944	12.03	6.42E+09	8.49E+01
26	2183.70	800	3.11	14.5	0.283	0.359	18.11	1.54E+11	141.5424
27	2184.00	800	3.66	16.5	0.336	0.500	32.88	2.26E+11	2.46E+02
28	2184.35	800	3.25	14.8	0.355	0.501	27.44	1.12E+11	1.29E+02
29	2184.65	800	4.25	20.3	0.594	0.858	28.72	2.71E+11	5.21E+02
30	2185.00		.460 #	8.9 #	4.58 *	5.71 *			
31	2185.35		2.336 #	8.6 #	.05 *	.11 *			
32	2185.70	800	3.45	16.0	0.116	0.200	52.67	2.97E+12	1.11E+03
33	2186.00	800	3.21	14.3	0.073	0.130	58.04	1.28E+13	3.03E+03
34	2186.35	800	3.88	17.6	2.402	3.012	15.04	1.16E+10	9.02E+01
35	2186.65	800	3.66	16.4	1.527	1.870	13.73	6.46E+10	3.19E+02
36	2187.00	800	3.55	15.8	1.740	2.122	13.28	3.03E+10	1.71E+02
37	2187.35	800	4.23	19.4	9.331	10.677	7.89	6.97E+08	2.10E+01
38	2187.65	800	3.27	15.6	1.805	2.113	10.31	3.91E+10	2.29E+02
39	2188.00	800	3.20	14.6	0.039	0.073	69.35	5.73E+13	7.17E+03
40	2188.25	800	3.43	15.7	0.742	0.864	10.53	2.87E+11	6.90E+02
41	2188.65	800	3.84	17.3	0.130	0.227	53.81	5.47E+12	2.30E+03
42	2189.00	800	4.32	18.6	8.403	9.499	7.17	7.15E+08	1.95E+01
43	2189.35	800	3.21	14.2	0.113	0.173	38.84	1.14E+12	4.17E+02
44	2189.65	800	2.83	12.8	0.232	0.293	18.18	7.52E+09	5.64E+00
45	2190.00	800	4.56	20.5	1.028	1.424	24.10	1.62E+11	5.40E+02
46	2190.35	800	4.84	21.8	6.115	7.255	10.45	1.03E+09	2.05E+01



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47	2190.65	800	4.97	23.0	7.606	8.959	9.83	8.83E+08	2.17E+01
48	2191.00	800	4.70	21.1	10.296	11.557	6.66	4.71E+08	1.57E+01
49	2191.35	800	4.38	23.6	19.466	21.973	6.76	1.69E+08	1.06E+01
50	2191.65	800	5.04	23.7	12.651	14.632	8.41	3.41E+08	1.40E+01
51	2192.05	800	4.35	20.8	1.131	1.548	22.95	1.01E+11	3.69E+02
52	2192.35	800	5.36	24.1	28.095	31.008	5.33	1.26E+08	1.14E+01
53	2192.65	800	4.44	22.5	26.558	28.982	4.71	1.24E+08	1.07E+01
54	2193.00	800	3.38	20.6	3.940	4.721	11.40	1.29E+10	1.65E+02
55	2193.35	800	4.93	22.7	19.502	21.725	5.98	2.46E+08	1.55E+01
56	2193.85		3.718 #	4.1 #	.03 *	.08 *			
57	2194.00	800	4.72	23.6	25.589	28.503	5.89	1.19E+08	9.83E+00
58	2194.35		4.367 #	4.8 #	22.5 *	25.5 *			
59	2194.65	800	3.75	16.9	6.718	7.737	8.45	1.37E+09	2.99E+01
60	2195.00		3.993 #	4.1 #	16.8 *	19.4 *			
61	2195.35	800	2.81	18.7	1.889	2.380	15.63	5.39E+10	3.30E+02
62	2195.65	800	4.82	22.8	22.086	24.381	5.42	1.95E+08	1.40E+01
63	2196.00	800	3.24	16.2	2.107	2.452	9.77	3.54E+10	2.42E+02
64	2198.35	800	0.87	3.9	0.001	0.003	167.64	9.15E+15	3.46E+04
65	2200.35	800	1.66	7.6	0.010	0.015	49.44	1.02E+16	3.14E+05
66	2202.35	800	1.29	5.8	0.003	0.006	107.88	5.96E+16	5.18E+05
67	2204.35	800	1.75	7.7	0.013	0.023	64.24	1.26E+15	5.27E+04
68	2206.35	800	1.65	7.5	0.005	0.012	99.13	2.12E+16	3.77E+05
69	2208.35	800	2.06	9.4	0.011	0.015	29.72	4.63E+16	1.64E+06
70	2210.45	800	1.09	9.2	0.037	0.042	11.01	3.54E+12	4.19E+02



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Sample Number	Depth ft	NOB Pressure psig	Pore Volume cc	Porosity %	Kinf md	Kair(est) md	b(He) psi	BETA ft(-1)	ALPHA microns
71	2212.35	800	1.85	8.3	0.033	0.057	57.10	0.00E+00	0.00E+00
72	2214.35	800	1.43	6.4	0.602	0.758	16.70	0.00E+00	0.00E+00
73	2216.35	800	2.05	9.1	0.003	0.006	124.01	3.14E+16	2.66E+05
74	2218.35	800	1.44	6.5	0.001	0.003	112.78	2.00E+16	8.89E+04
75	2220.35	800	1.09	4.9	0.001	0.002	137.09	1.84E+17	6.06E+05
76	2222.35	800	0.91	7.2	0.124	0.182	33.53	0.00E+00	0.00E+00

Irregular sample. Ambient porosity reported.

* Permeability measured using Profile Permeameter.



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Core Number One 2160.3 through 2222.35 feet						
1	2160.30		0.78 *	9.2 #	2.69	Sh rd slty calc
2	2162.30		1.36 *	9.1 #	2.71	Sh rd slty calc
3	2164.35		<.001 *	17.3 #	2.75	Sltst rd gry sh slily calc
4	2166.25		.01 *	9.4 #	2.73	Sh rd slty calc
5	2168.50		1.63 *	7.1 #	2.75	Sh rd slty slily calc
6	2170.35	800	0.010	7.9	2.72	Sltst rd gry sh lam calc
7	2174.40	800	0.004	11.0	2.74	Sh rd
8	2176.80		<.001	14.1 #	2.82	Dol lt gry wh micro xln slily lmy
9	2178.00	800	0.081	15.3	2.72	Sst rd gry vf gr sh lam slty
10	2178.45	800	0.434	13.6	2.72	Sst rd gry vf gr sh lam slty
11	2178.70	800	0.038	13.7	2.74	Sst rd gry vf gr sh lam slty
12	2179.00	800	0.164	12.9	2.73	Sst rd gry vf gr sh lam slty
13	2179.50		.40 *	7.3 #	2.70	Sst rd gry vf gr v sh lam slty
14	2179.70	800	1.876	22.9	2.65	Sst lt gry wh vf gr slty
15	2180.00	800	2.179	19.3	2.69	Sst lt gry wh vf gr slty
16	2180.35	800	0.094	15.0	2.73	Sst rd vf gr v sh slty slily calc
17	2180.65	800	0.058	16.1	2.76	Sst rd vf gr v sh slty slily calc
18	2181.00	800	2.123	17.9	2.62	Sst lt gry wh vf gr slily sh lam slty
19	2181.35	800	11.853	21.8	2.66	Sst lt gry wh vf gr slily sh lam slty
20	2181.70	800	18.808	19.5	2.68	Sst lt gry wh vf gr slily sh lam slty
21	2182.00	800	5.378	17.6	2.70	Sst lt gry wh vf gr slily sh lam slty
22	2182.35	800	0.716	14.9	2.72	Sst rd gry vf gr slily sh lam slty



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23	2182.65	800	3.747	19.5	2.68	Sst lt gry wh vf gr slty
24	2183.10	800	3.775	21.6	2.67	Sst lt gry wh vf gr slily sh lam slty
25	2183.35	800	4.087	20.9	2.67	Sst lt gry wh vf gr slily sh lam slty
26	2183.70	800	0.283	14.5	2.70	Sst rd gry vf gr v sh slty
27	2184.00	800	0.336	16.5	2.69	Sst rd gry vf gr sh lam slty
28	2184.35	800	0.355	14.8	2.72	Sst rd gry vf gr sh lam slty
29	2184.65	800	0.594	20.3	2.67	Sst rd gry vf gr sh lam slty
30	2185.00		5.71 *	8.9 #	2.68	Sh rd slty
31	2185.35		.11 *	8.6 #	2.68	Sh rd slty
32	2185.70	800	0.116	16.0	2.69	Sh rd slty slily sdy
33	2186.00	800	0.073	14.3	2.73	Sh rd slty slily sdy
34	2186.35	800	2.402	17.6	2.71	Sst rd gry vf gr sl lam slty
35	2186.65	800	1.527	16.4	2.78	Sst rd gry vf gr sl lam slty
36	2187.00	800	1.740	15.8	2.71	Sst rd gry vf gr sl lam slty
37	2187.35	800	9.331	19.4	2.69	Sst rd gry vf gr sl lam slty
38	2187.65	800	1.805	15.6	2.71	Sst rd gry vf gr sl lam slty
39	2188.00	800	0.039	14.6	2.70	Sh rd slty slily sdy
40	2188.25	800	0.742	15.7	2.71	Sh rd slty slily sdy lam
41	2188.65	800	0.130	17.3	2.70	Sst rd gry vf gr v sh lam slty
42	2189.00	800	8.403	18.6	2.70	Sst rd gry vf gr v sh lam slty
43	2189.35	800	0.113	14.2	2.74	Sst rd vf gr v sh lam slty
44	2189.65	800	0.232	12.8	2.74	Sst rd vf gr v sh lam slty
45	2190.00	800	1.028	20.5	2.68	Sst rd brn vf gr sh lam slty
46	2190.35	800	6.115	21.8	2.68	Sst rd brn vf gr sh lam slty



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47	2190.65	800	7.606	23.0	2.66	Sst rd brn vf gr sh lam slty
48	2191.00	800	10.296	21.1	2.67	Sst rd brn vf gr sh lam slty
49	2191.35	800	19.466	23.6	2.66	Sst rd brn vf gr slily sh lam slty
50	2191.65	800	12.651	23.7	2.66	Sst rd brn vf gr slily sh lam slty
51	2192.05	800	1.131	20.8	2.65	Sst rd brn vf gr slily sh lam slty
52	2192.35	800	28.095	24.1	2.67	Sst rd brn vf gr slily sh lam slty
53	2192.65	800	26.558	22.5	2.66	Sst rd brn vf gr slily sh lam slty
54	2193.00	800	3.940	20.6	2.67	Sst rd brn vf gr slily sh lam slty
55	2193.35	800	19.502	22.7	2.68	Sst rd brn vf gr slily sh lam slty
56	2193.85		.08 *	4.1 #	2.66	Sst rd brn vf gr slily sh lam slty
57	2194.00	800	25.589	23.6	2.66	Sst rd brn vf gr slily sh lam slty
58	2194.35		25.5 *	4.8 #	2.67	Sst rd brn vf gr slily sh lam slty
59	2194.65	800	6.718	16.9	2.61	Sst rd brn vf gr slily sh lam slty
60	2195.00		19.4 *	4.1 #	2.66	Sst rd brn vf gr slily sh lam slty
61	2195.35	800	1.889	18.7	2.67	Sst rd brn vf gr slily sh lam slty
62	2195.65	800	22.086	22.8	2.67	Sst lt rd brn vf gr slily sh lam slty
63	2196.00	800	2.107	16.2	2.66	Sst gry vf gr sh lam slty
64	2198.35	800	0.001	3.9	2.83	Dol gry vf xln foss
65	2200.35	800	0.010	7.6	2.87	Dol gry vf xln foss
66	2202.35	800	0.003	5.8	2.82	Dol gry vf xln foss
67	2204.35	800	0.013	7.7	2.83	Dol gry vf xln foss
68	2206.35	800	0.005	7.5	2.78	Dol gry vf xln foss
69	2208.35	800	0.011	9.4	2.77	Dol lt gry micro xln slily lmy
70	2210.45	800	0.037	9.2	2.73	Sh rd slty calc



CORE LABORATORIES

Company : ANADARKO PETROLEUM CORPORATION
Well : Boekhaus Trust A-1
Field : Hugoton Field
County : Morton County, Kansas

CL File No : 57151-18100

Date : 02-Nov-1994

Analyst : MJK/MRL

CMS - 300 ANALYSIS

Sample Number	Depth ft	NOB Pressure psig	Kinf md	Porosity %	Grain Den. g/cm3	Description
71	2212.35	800	0.033	8.3	2.75	Sh rd gry slty calc
72	2214.35	800	0.602	6.4	2.74	Sh rd gry slty v calc
73	2216.35	800	0.003	9.1	2.73	Sh rd gry
74	2218.35	800	0.001	6.5	2.71	Sh rd gry v calc
75	2220.35	800	0.001	4.9	2.80	Sh rd anhy calc
76	2222.35	800	0.124	7.2	2.70	Sh rd anhy calc

Irregular sample. Ambient porosity reported.

* Permeability measured using Profile Permeameter.

CORRELATION COREGRAPH

ANADARKO PETROLEUM CORPORATION

Boekhaus Trust A-1

Hugoton Field

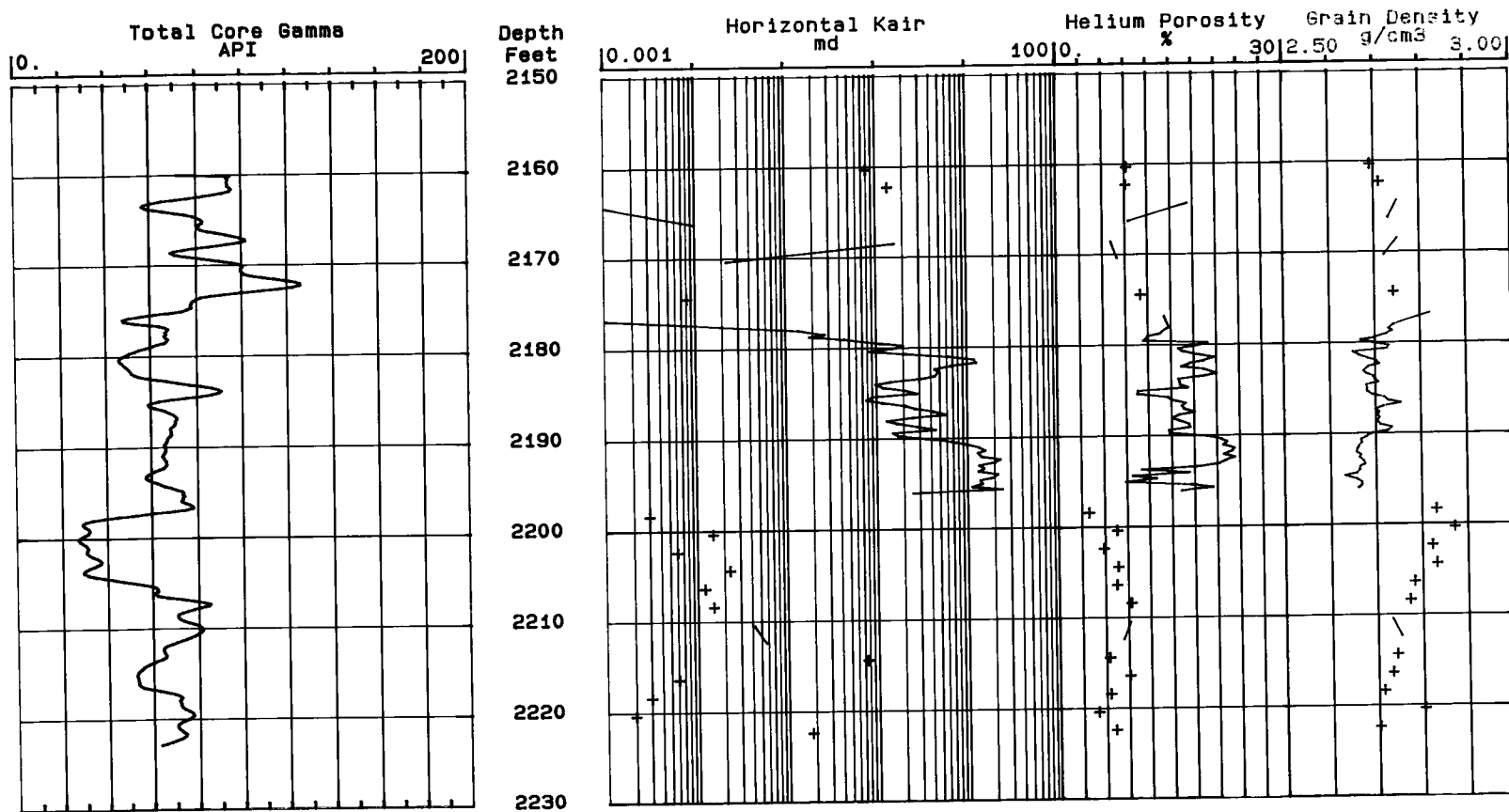
Morton County, Kansas

2160.0 - 2222.35 ft

Core Laboratories File No. 57151-18100

08-Dec-1994

Vertical Scale
5.00 in = 100.0 ft



APPENDIX A: LIST OF PROJECT ANALYSTS and PERSONNEL

PETROLEUM SERVICES MANAGER	FEDERICA M. CURBY
LABORATORY SUPERVISOR	MICHAEL R. LONG
SENIOR PROJECT ANALYST	JOSEPH A. WEIR
PHOTOGRAPHY	THOMAS MURPHY
TECHNICAL SALES REPRESENTATIVE	DOUGLAS McELROY
CORE ANALYST	MIKE KOSTER
SECRETARIAL	JANET PUFFER

APPENDIX B: REPORT DISTRIBUTION

ANADARKO PETROLEUM CORPORATION
Boekhaus Trust NO. A-1
Hugoton Field
Morton County, Kansas
CL File No. 57151-18100

4 cc Anadarko Petroleum Corporation
17001 Northchase
Houston, Texas 77060

Attn: Mr. Warren Winters