REPORT NO. 190410

PAGE NO. 1

TEST DATE: 13-JUL-1994

S T A R

Schlumberger Transient Analysis Report

Based on Model Verified Interpretation Of a Western Testers Well Test

Schlumberger

COMPANY: JACK EXPLORATION, INC.

WELL: DIEL #1-16 - OH-DST #1

TEST IDENTIFICATION

Test Type	OH-DST
Test No.	ONE
Formation	MISSISSIPPI
Test Interval (ft)	4643 to 4700
Depth Reference	KB

WELL LOCATION

Field	WILD CAT
County	BARBER
State	KANSAS
Sec/Twn/Rng	S16/34S/10W
Elevation (ft)	1379

HOLE CONDITIONS

Total Depth (MD/TVD) (ft)	4700/4700
Hole Size (in)	7.875
Tested Interval/Net Pay (ft)	57 / 5

MUD PROPERTIES

Mud Type	CHEMICAL
Mud Weight (lb/gal)	8.7
Filtrate Chlorides (ppm)	4300

INITIAL TEST CONDITIONS

Initial Hydrostatic (psi)	2282
Gas Cushion Type	NONE
Surface Pressure (psi)	--
Liquid Cushion Type	NONE
Cushion Length (ft)	--

TEST STRING CONFIGURATION

Pipe Length (ft)/I.D. (in)	4110 / 3.8
Collar Length (ft)/I.D. (in)	510 / 2.25
Packer Depths (ft)	4643
Bottomhole Choke Size (in)	0.75
Gauge Depth (ft)/Type	-- / 13362

NET PIPE RECOVERY

Volume	Fluid Type	Properties
140 ft	GAS CUT MUD	

NET SAMPLE CHAMBER RECOVERY

Volume	Fluid Type	Properties
NO SAMPLE		
Pressure:	GOR:	GLR:

INTERPRETATION RESULTS

Model of Behavior	2-POROSITY
Fluid Type Used for Analysis	GAS
Reservoir Pressure (psi)	1692
Transmissibility (md.ft/cp)	486.3
Effective Permeability (md)	1.5 (to Gas)
Skin Factor	0.9
Storativity Ratio, Omega	1.8E-03
Interporos.Flow Coef.,Lambdâ	3.3E-04
Radius of Investigation (ft)	45

ROCK/FLUID/WELLBORE PROPERTIES

Gas Gravity	0.65
Liquid/Gas Ratio (STB/MMSCF)	0
Water Cut (%)	0
Viscosity (cp)	0.01538
Total Compressibility (1/psi)	4.951E-04
Porosity (%)	12
Reservoir Temperature (F)	124

PRODUCTION RATE DURING TEST: 385 MSCF/D

COMMENTS:

THIS DRILLSTEM TEST WAS CONDUCTED BY WESTERN TESTERS OF WICHITA, KANSAS AND EVALUATED BY SCHLUMBERGER - GEOQUEST 16-JUL-1994. ANALYSIS OF THE DIAGNOSTIC LOG-LOG PLOTS OF PRESSURE AND DERIVATIVE FOR BOTH SHUT-INS INDICATES THE PRESENCE OF A TWO-POROSITY SYSTEM WITH SKIN AND DECREASING WELLBORE STORAGE AT EARLY TIME AND TRANSITIONAL FLOW REGIME AT MID TO LATE TIMES; THE BUILDUP RESPONSE WAS NEARING THE START OF INFINITE ACTING RADIAL FLOW AT THE END OF THE FINAL BUILDUP. THE FINAL SHUTIN WAS MATCHED USING A TWO-POROSITY (PSS) RESERVOIR MODEL WITH SKIN AND DECREASING WELLBORE STORAGE (SEE ANALYSIS PLOTS, PAGES 2-5). BASED ON THE MATCH, THE BUILDUP RESPONSE WAS IN TRANSITION FROM FISSURES TO TOTAL SYSTEM AT THE END OF THE TEST. EXTRAPOLATED PRESSURE FROM SHUTIN #2 WAS LOWER THAN THE LAST-READ PRESSURE FROM SHUTIN #1. THIS MAY BE DUE TO "SUPERCHARGING" PRIOR TO THE FIRST SHUTIN, INCORRECT FLOWRATE MEASUREMENTS, OR POSSIBLY TO DEPLETION. A LONGER TEST IS RECOMMENDED TO CONFIRM THESE RESULTS. FOR QUESTIONS ABOUT THIS REPORT, PLEASE CONTACT DEBORA HALLFORD AT (303) 843-9090.

CALCULATIONS
GAS WELL
LOG-LOG ANALYSIS

Schlumberger

LOG [DELTA M(P)] VS. LOG (DELTA T) PLOT

TWO-POROSITY SYSTEM WITH PSEUDO STEADY STATE INTERPOROSITY FLOW
SKIN & DECREASING WELLBORE STORAGE
PD VS. TD/CD

DATA IDENTIFICATION

FLOW PERIOD # 4, BUILDUP
M(P)' = 1.163E+06 PSI**2/CP @ DELTA T=0
FLOW RATE CHANGE = 385.00 MSCF/D

TYPE-CURVE MATCH

CURVE MATCH, CD*E(2S) = 280.993
STORATIVITY RATIO, OMEGA = 1.83696E-03
TRANSITION CURVE, LAMBDA*E(-2S) = 5.78095E-05
PRESSURE MATCH, PD/DELTA M(P) = 2.340E-08 1/(PSI**2/CP)
TIME MATCH, (TD/CD)/DELTA T = 81.816 1/HR

CALCULATIONS

KH	7.480 MD.FT
KH/MU	486.34 MD.FT/CP
K	1.496 MD
C	0.001754 BBL/PSI
CD	48.994
LAMBDA	3.316E-04
SKIN, S	0.8733
RADIUS OF INVESTIGATION	45.446 FT (@ 1.5 HR)

COMMENTS

USING TWO-POROSITY (PSS), SKIN AND DECREASING WELLBORE
STORAGE RESERVOIR MODEL; Ca/C=11.92 CoD=7.97

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DIMENSIONLESS MULTI-RATE
PLOT: LOG-LOG MATCH WITH TWO-POROSITY MODEL

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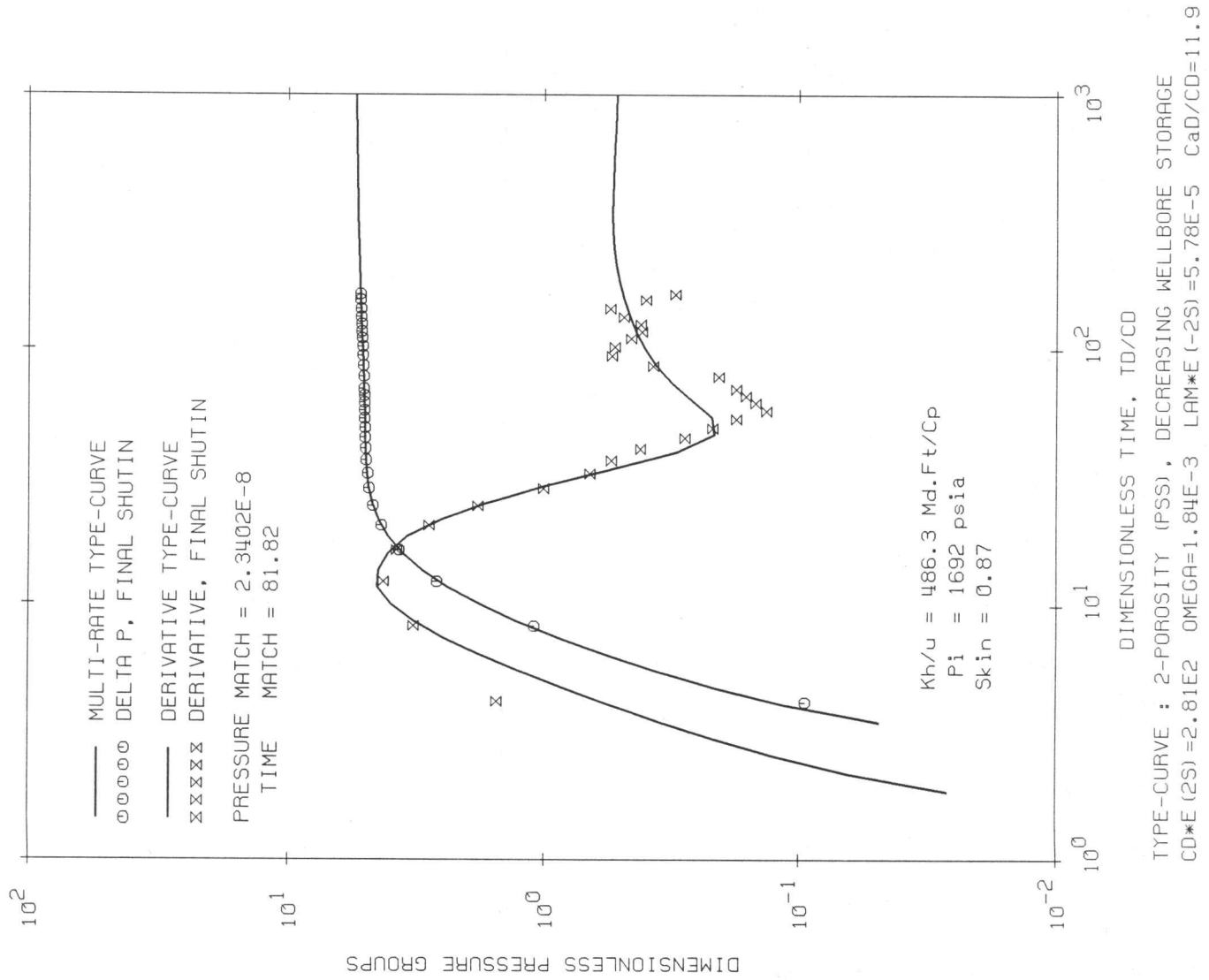

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DIMENSIONLESS SUPERPOSITION PLOT WITH TWO-POROSITY MODEL

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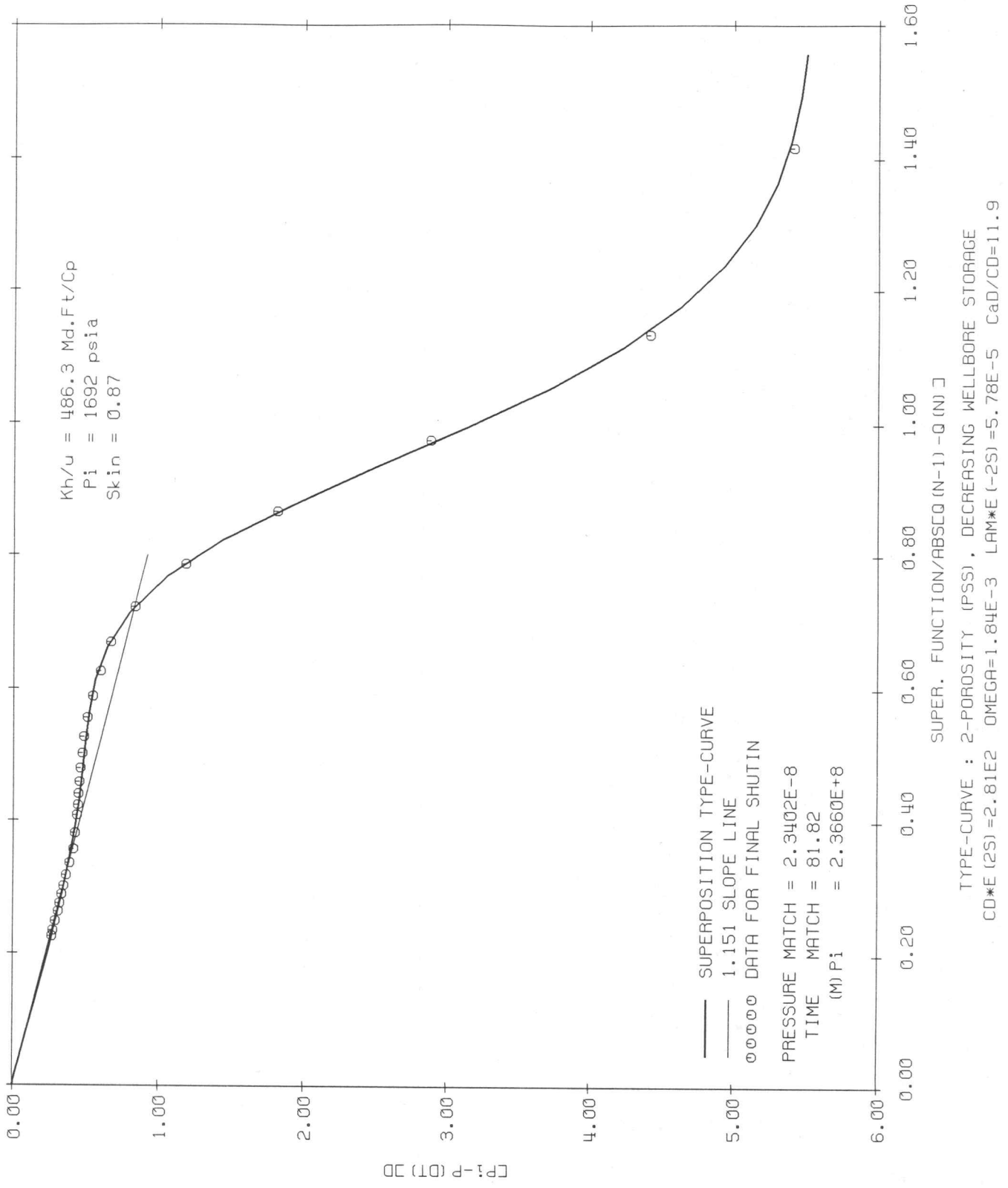

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PRESSURE HISTORY MATCH
WITH 2-POROSITY MODEL

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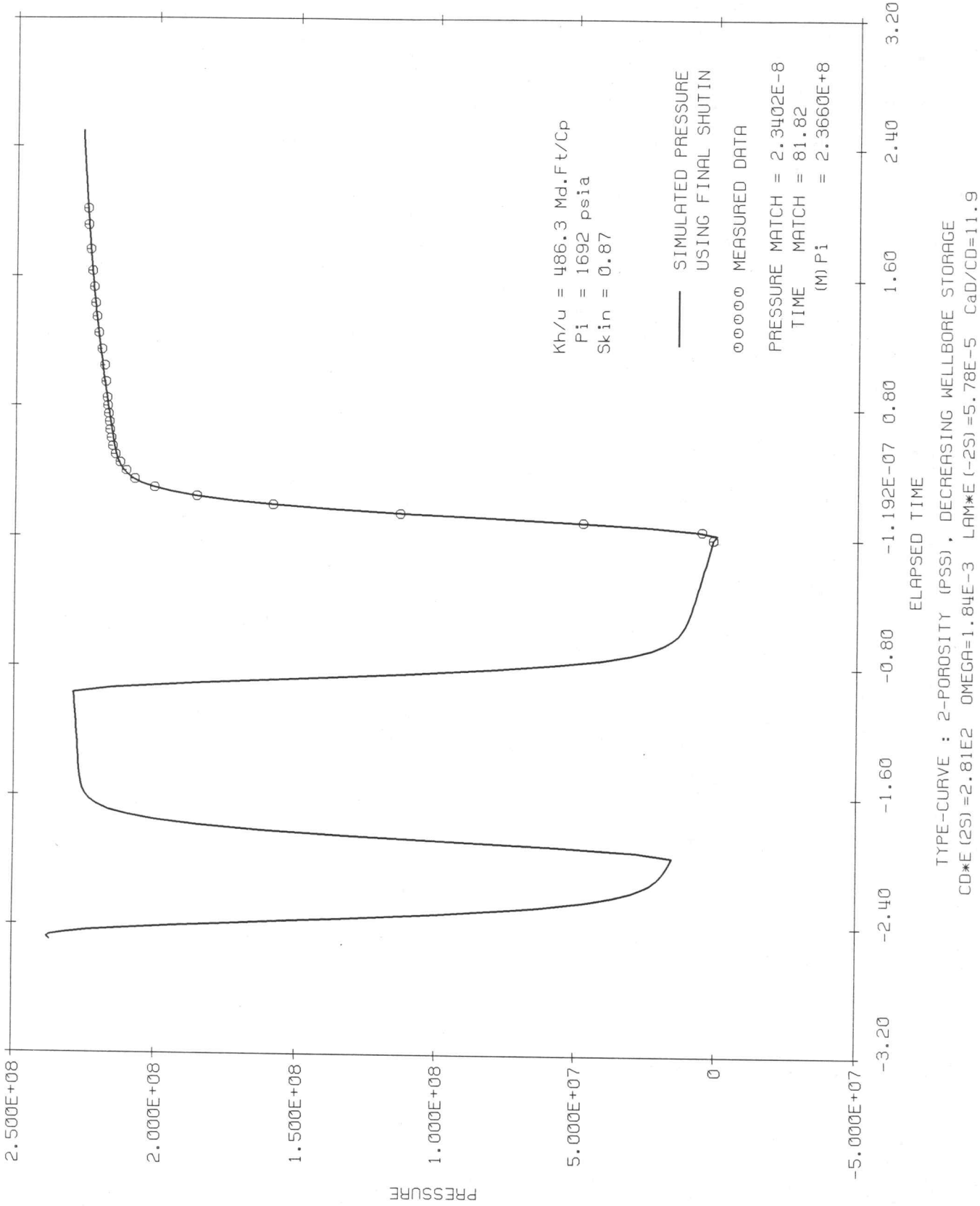

FLOWRATE DATA
USED IN ANALYSIS
DIEL #1-16 - DST #1

Schlumberger

ET VS. FLOWRATE

USING REPORTED GAS FLOWRATES DURING DRILLSTEM TEST CONDUCTED BY
WESTERN TESTERS OF WICHITA, KS - JACK EXPLORATION - DIEL #1-16

	ET (hrs) PRIOR TO FINAL SHUT-IN	GAS FLOWRATE (MSCF/D)
1	-2.5000	385.00
2	-2.0000	0.00000E-01
3	-1.0000	385.00
4	0.00000E-01	0.00000E-01

MODEL-VERIFIED(tm) REPORT

Schlumberger

THIS IS SCHLUMBERGER'S MODEL-VERIFIED(tm) INTERPRETATION REPORT. WITH MODEL-VERIFIED(tm) INTERPRETATION, THE GOAL OF THE SCHLUMBERGER ANALYST IS TO CONSTRUCT A TOTAL SYSTEM RESERVOIR MODEL THAT MATCHES ALL OF YOUR WELL TEST DATA. THIS PROVIDES YOU WITH RELIABLE ANSWERS THAT YOU CAN HAVE CONFIDENCE IN.

FROM THE DIAGNOSTIC LOG-LOG PLOT OF PRESSURE AND PRESSURE DERIVATIVE, THE SCHLUMBERGER ANALYST IDENTIFIES THE FLOW REGIMES GOVERNED BY THE INNER BOUNDARY CONDITIONS, BASIC RESERVOIR BEHAVIOR, AND OUTER BOUNDARY CONDITIONS. A RESERVOIR MODEL IS THEN CONSTRUCTED AND THE TEST DATA ARE MATCHED TO IT. IN ORDER TO VERIFY THE QUALITY OF THE MATCH, THE THEORETICAL MODEL RESPONSE (TYPE CURVE) AND THE TEST DATA ARE PLOTTED TOGETHER. THE PRESENTATION OF THE MATCH CAN BE SHOWN IN ANY OF THREE DIFFERENT FORMS.

1) LOG-LOG PLOT (DELTA PRESSURE AND DERIVATIVE vs. DELTA TIME)
2) SEMI-LOG PLOT (PRESSURE vs. SUPERPOSITION TIME)
3) CARTESIAN PLOT (PRESSURE vs. TIME)

SCHLUMBERGER USES SUPERPOSITION TECHNIQUES (MULTI-RATE ANALYSIS) TO ACCOUNT FOR THE WELL'S PRIOR PRODUCTION HISTORY. ESPECIALLY IN CASES WHERE THE PRIOR PRODUCTION IS ERRATIC OR UNUSUAL, SUPERPOSITION IS THE ONLY MEANS OF PROVIDING AN ACCURATE TYPE CURVE MATCH OF THE WELL TEST DATA. FOR GAS WELLS, THE PSEUDO-PRESSURE TECHNIQUE IS USED TO ACCOUNT FOR THE CHANGE IN GAS PROPERTIES WITH CHANGING PRESSURE.

IN SOME INSTANCES, THE WELL TEST DATA WILL NOT BE UNIQUE, i.e., MORE THAN ONE RESERVOIR MODEL WILL MATCH THE TEST DATA. THE MOST APPROPRIATE MODEL CAN BE DETERMINED AS WE WORK WITH YOU AND DISCUSS THE AREA LITHOLOGY AND GEOLOGY.

THE RESERVOIR ANSWERS DERIVED FROM MODEL-VERIFIED(tm) INTERPRETATION CAN INCLUDE: EFFECTIVE PERMEABILITY (K), SKIN DAMAGE (s), RESERVOIR PRESSURE (P*), FRACTURE HALF-LENGTH (Xf), FRACTURE CAPACITY (Kfw), BOUNDARY CONDITIONS AND DISTANCE TO BOUNDARIES, AS WELL AS THE MODEL OF BASIC RESERVOIR BEHAVIOR.

USING THE RESERVOIR MODEL DETERMINED BY MODEL-VERIFIED(tm) INTERPRETATION, FLOWRATE PREDICTIONS CAN BE MADE FOR THE WELL. ADDITIONALLY, WE CAN HELP YOU OPTIMIZE WELL PERFORMANCE BY USING SCHLUMBERGER'S NODAL ANALYSIS SOFTWARE TO EXAMINE THE WELL'S SENSITIVITY TO DIFFERENT COMPLETION DESIGNS (e.g., FRACTURE HALF-LENGTH, TUBING SIZE, WELLHEAD PRESSURE, SKIN VALUE, SHOT DENSITY). THIS AFFORDS YOU THE OPPORTUNITY TO FORECAST PRODUCTION POTENTIAL FOR THE WELL BEFORE MAKING FINAL COMPLETION/RECOMPLETION DECISIONS.

WELL TEST MODELS

Schlumberger

THE SCHLUMBERGER ANALYST CONSTRUCTS THE TOTAL SYSTEM RESERVOIR MODEL THAT BEST MATCHES YOUR TEST DATA BY CHOOSING THE INNER BOUNDARY CONDITION(S), A BASIC RESERVOIR MODEL, AND THE OUTER BOUNDARY CONDITION(S). THESE COMPONENTS ARE PUT TOGETHER INTO ONE RESERVOIR MODEL AND THE TEST DATA IS MATCHED BY ADJUSTING THE MODEL PARAMETERS (e.g., PERMEABILITY AND SKIN) TO OBTAIN THE BEST FIT. THE FOLLOWING IS A PARTIAL LIST OF THE MODEL COMPONENTS AVAILABLE TO THE SCHLUMBERGER ANALYST FOR MATCHING YOUR WELL TEST DATA.

INNER BOUNDARY CONDITION

- NO WELLBORE STORAGE
- CONSTANT WELLBORE STORAGE
- VARIABLE WELLBORE STORAGE
- FINITE CONDUCTIVITY VERTICAL FRACTURE
- INFINITE CONDUCTIVITY VERTICAL FRACTURE
- UNIFORM FLUX VERTICAL FRACTURE
- HORIZONTAL FRACTURE
- PARTIAL PENETRATION

BASIC RESERVOIR MODEL

- HOMOGENEOUS
- DUAL POROSITY, PSEUDO STEADY STATE INTERPOROSITY FLOW
- DUAL POROSITY, TRANSIENT INTERPOROSITY FLOW
- TRIPLE POROSITY
- DUAL PERMEABILITY
- RADIAL COMPOSITE

OUTER BOUNDARY CONDITION

- INFINITE SYSTEM
- SINGLE SEALING NO FLOW BOUNDARY
- PARTIALLY SEALING BOUNDARY
- SINGLE CONSTANT PRESSURE BOUNDARY
- TWO INTERSECTING NO FLOW BOUNDARIES (WEDGE GEOMETRY)
- PARALLEL NO FLOW BOUNDARIES (CHANNEL)
- GAS CAP/BOTTOM WATER DRIVE
- CLOSED (NO FLOW) CIRCLE
- CONSTANT PRESSURE CIRCLE
- CLOSED (NO FLOW) RECTANGLE
- CONSTANT PRESSURE RECTANGLE
- MIXED BOUNDARY RECTANGLE

FOR SOME APPLICATIONS, SUCH AS HORIZONTAL AND LAYERED RESERVOIR TESTS, ALL OF THE POSSIBLE COMBINATIONS ARE NOT AVAILABLE. REFERENCES ON MOST MODEL COMPONENTS CAN BE FOUND IN SPE PAPERS.

SEQUENCE OF EVENTS

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DATE	TIME (HR:MIN)	DESCRIPTION	ET (MINS)	BHP (PSIA)	WHP (PSIG)
13-JUL	11:59	Hydrostatic Mud	-1	2282	
	12:00	START FLOW GAS TO SURFACE IN 4 MINS.	0	166	
	12:10	385 MSCF/D ON 1" ORIFICE	10		7.0
	12:20		20		7.0
	12:30	END FLOW & START SHUTIN	30	155	7.0
	13:30	END SHUTIN	90	1812	
	13:30	START FLOW	90	161	
	13:40	385 MSCF/D ON 1" ORIFICE	100		7.0
	13:50	385 MSCF/D	110		7.0
	14:00	385 MSCF/D	120		7.0
	14:10	385 MSCF/D	130		7.0
	14:20	385 MSCF/D	140		7.0
	14:30	END FLOW & START SHUTIN	150	118	7.0
	16:30	END SHUTIN	270	1648	
	16:31	Hydrostatic Mud TEST CONDUCTED BY WESTERN TESTERS OF WICHITA, KANSAS	271	2202	

DISTRIBUTION OF REPORTS

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JACK EXPLORATION, INC.
Attn: MR. JACK
(2 copies)

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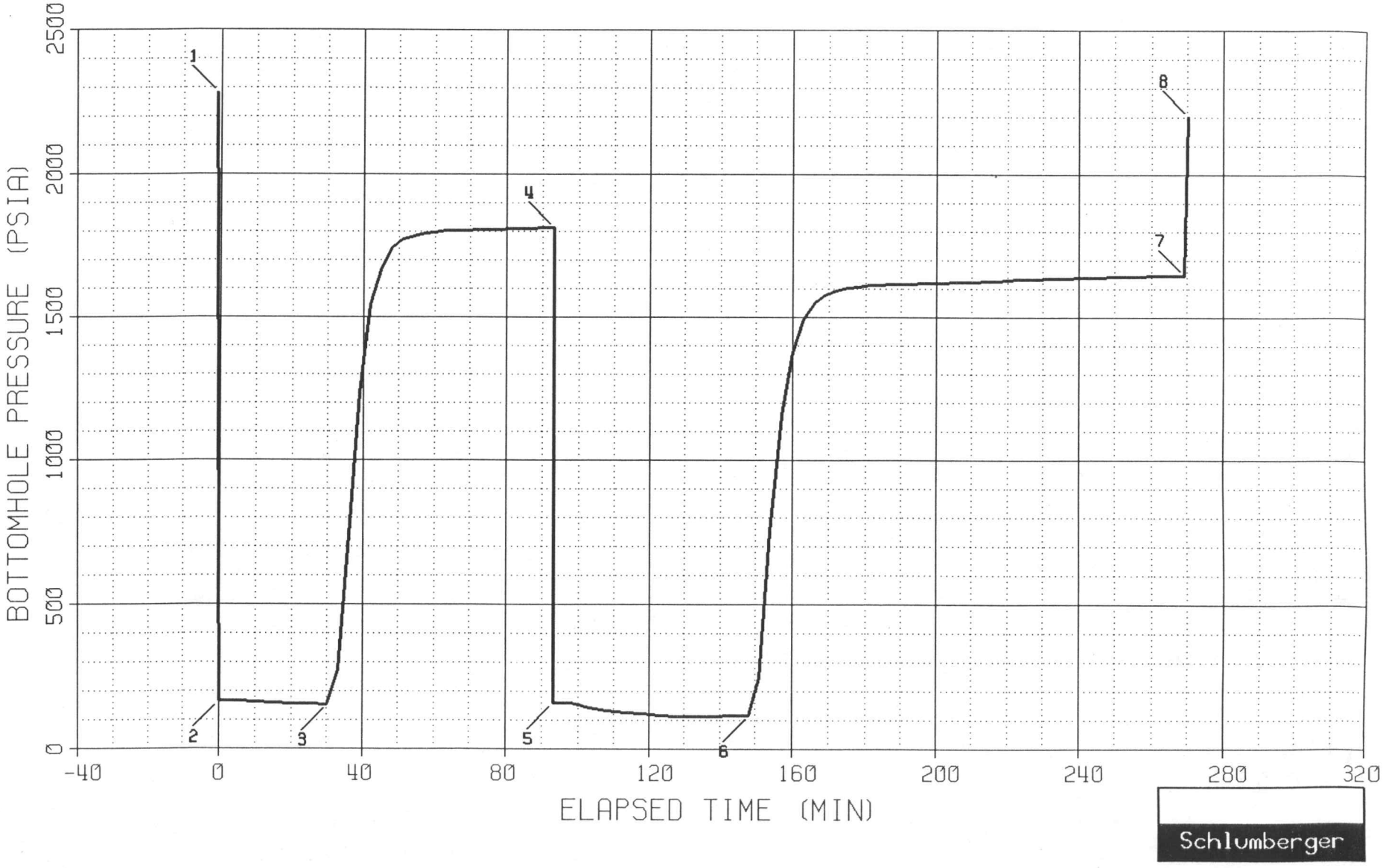
BOTTOMHOLE PRESSURE LOG

FIELD REPORT NO. 190410
INSTRUMENT NO. 13362
DEPTH : 0 FT
CAPACITY : 4450 PSI
PORT OPENING : OUTSIDE

COMPANY : JACK EXPLORATION
WELL : #1-16

Mechanical Recorder Data



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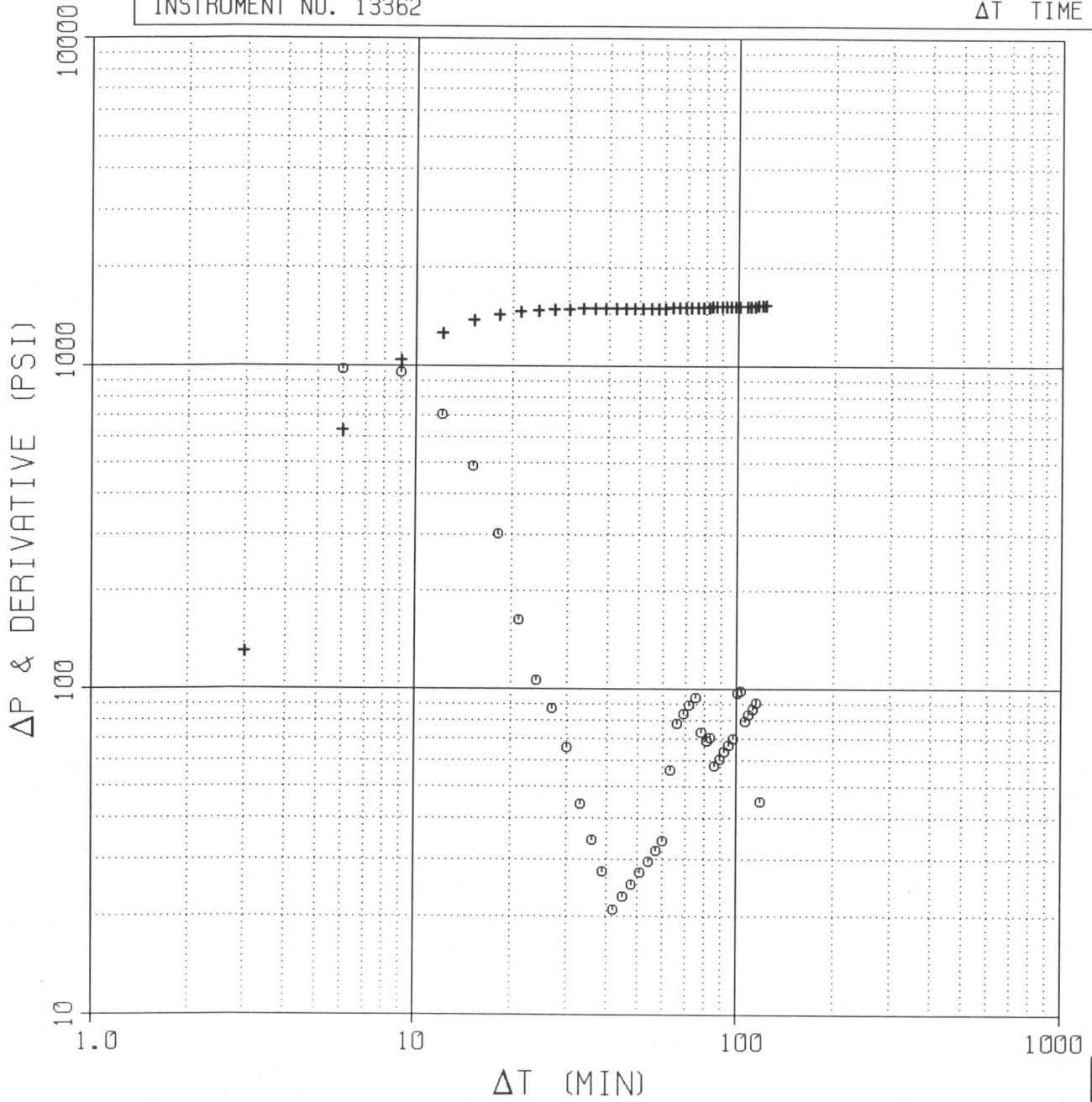
LOG LOG PLOT

COMPANY : JACK EXPLORATION
WELL : #1-16
FIELD REPORT NO. 190410
INSTRUMENT NO. 13362

SHUTIN #2 : PRODUCING TIME (Tp) : 85.0 MIN
FINAL FLOW PRESSURE (Pwf) : 118 PSIA
PLOT ELAPSED TIME RANGE: 151.0 TO 269.0 MIN
ΔT TIME RANGE: 3.0 TO 121.0 MIN



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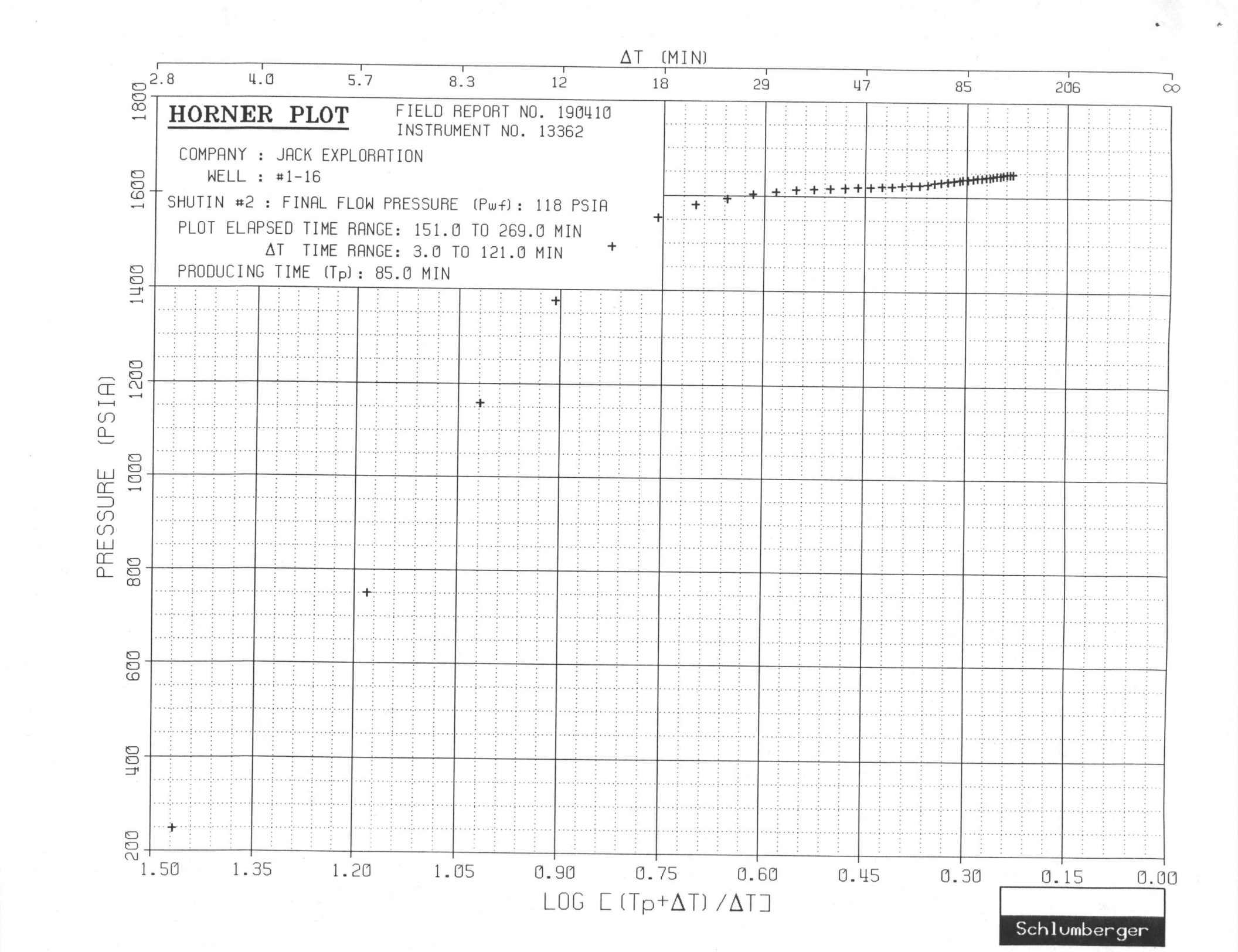
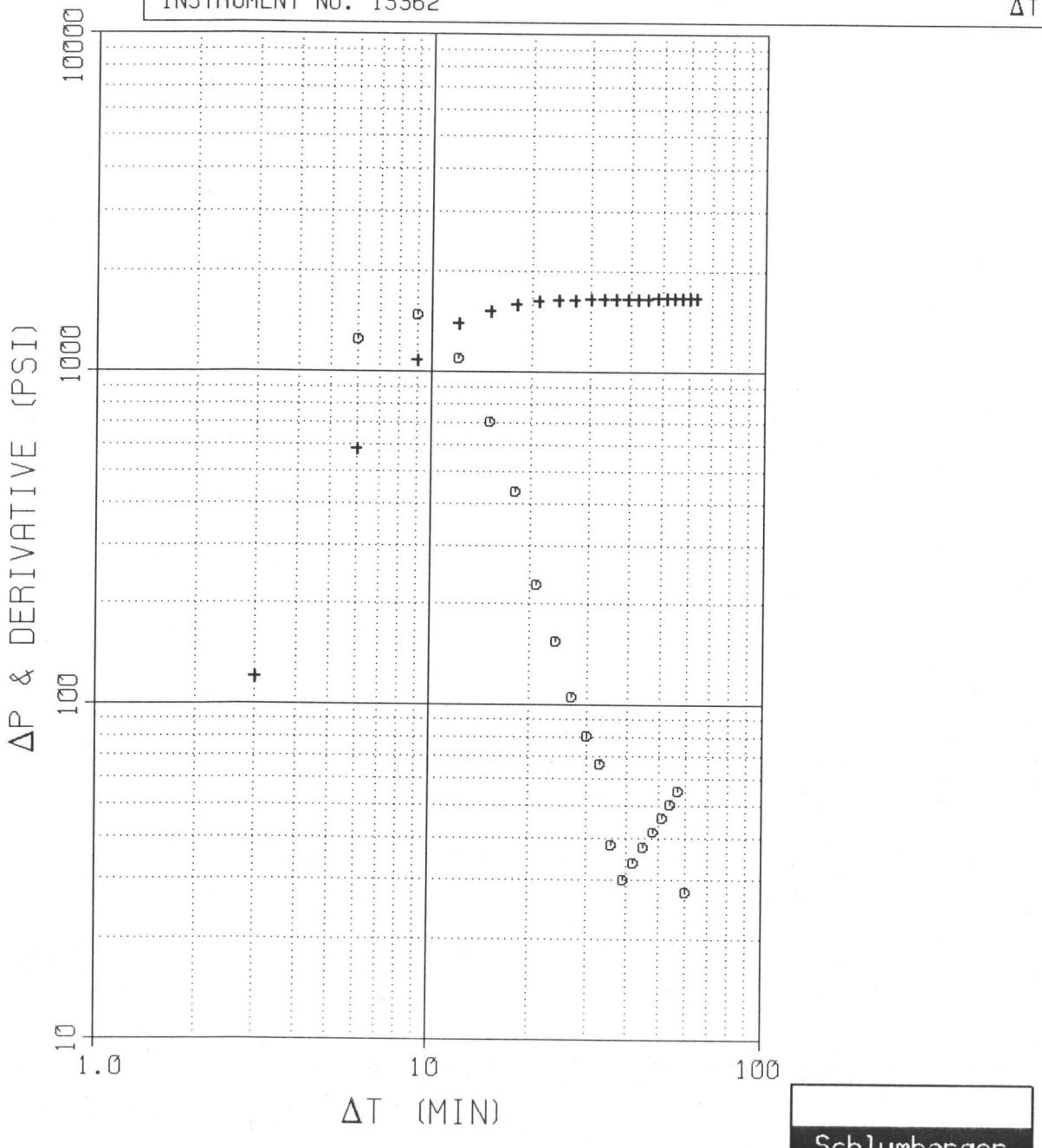
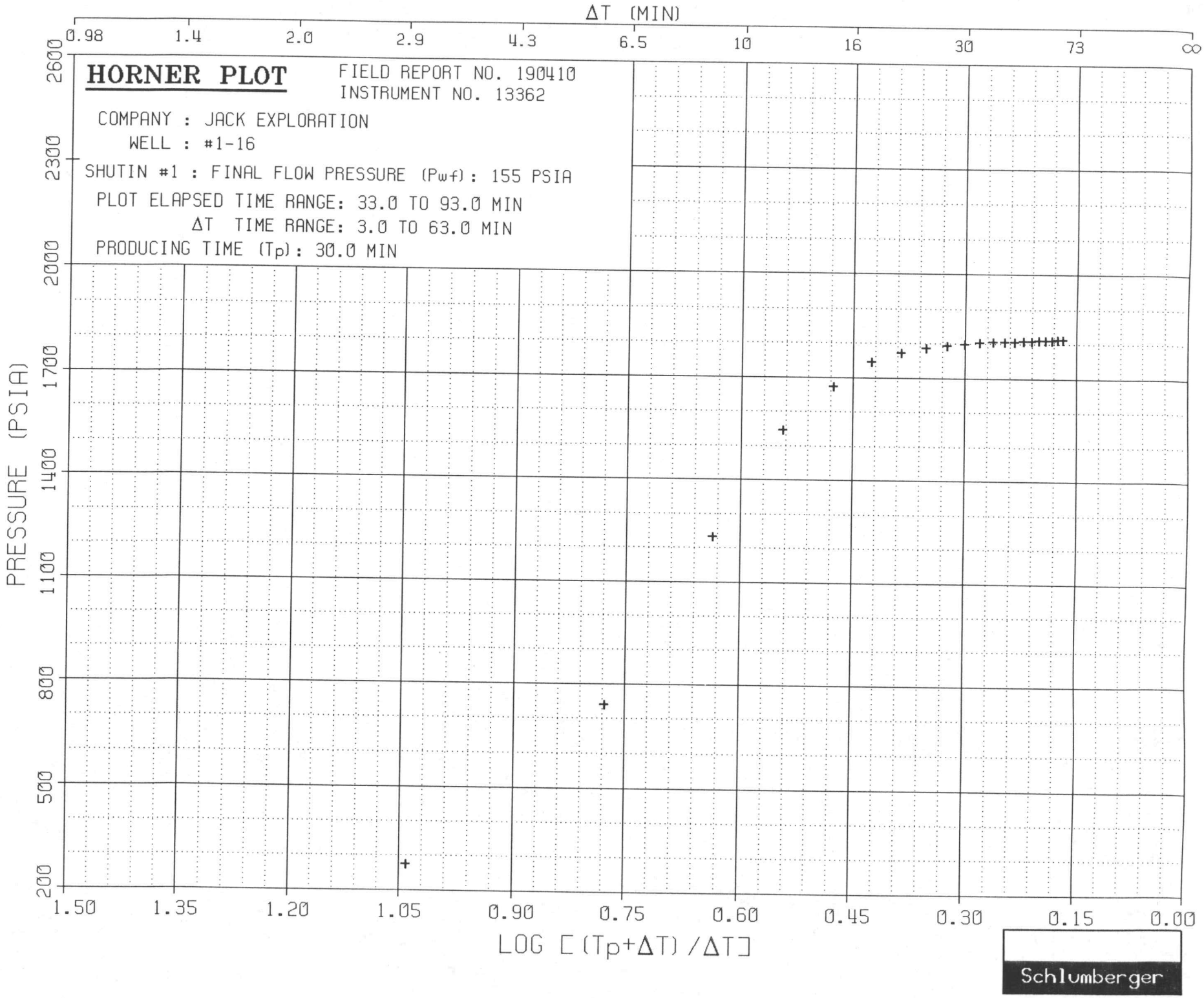

ΔT (MIN)
2.8
4.0
5.7
8.3
12
18
29
47
85
206
∞
HORNER PLOT
FIELD REPORT NO. 190410
INSTRUMENT NO. 13362
COMPANY : JACK EXPLORATION
WELL : #1-16
SHUTIN #2 : FINAL FLOW PRESSURE (Pwf): 118 PSIA
PLOT ELAPSED TIME RANGE: 151.0 TO 269.0 MIN
ΔT TIME RANGE: 3.0 TO 121.0 MIN
PRODUCING TIME (Tp): 85.0 MIN
PRESSURE (PSIA)
1800
1600
1400
1200
1000
800
600
400
200
1.50
1.35
1.20
1.05
0.90
0.75
0.60
0.45
0.30
0.15
0.00
LOG [(Tp+ΔT)/ΔT]
Schlumberger

LOG LOG PLOT

COMPANY : JACK EXPLORATION
WELL : #1-16
FIELD REPORT NO. 190410
INSTRUMENT NO. 13362

SHUTIN #1 : PRODUCING TIME (Tp): 30.0 MIN
FINAL FLOW PRESSURE (Pwf): 155 PSIA
PLOT ELAPSED TIME RANGE: 33.0 TO 93.0 MIN
ΔT TIME RANGE: 3.0 TO 63.0 MIN




ΔT (MIN)
0.98
1.4
2.0
2.9
4.3
6.5
10
16
30
73
∞
HORNER PLOT
FIELD REPORT NO. 190410
INSTRUMENT NO. 13362
COMPANY : JACK EXPLORATION
WELL : #1-16
SHUTIN #1 : FINAL FLOW PRESSURE (Pwf) : 155 PSIA
PLOT ELAPSED TIME RANGE: 33.0 TO 93.0 MIN
ΔT TIME RANGE: 3.0 TO 63.0 MIN
PRODUCING TIME (Tp) : 30.0 MIN
PRESSURE (PSIA)
2600
2300
2000
1700
1400
1100
800
500
200
1.50
1.35
1.20
1.05
0.90
0.75
0.60
0.45
0.30
0.15
0.00
LOG [(Tp+ΔT)/ΔT]
Schlumberger

****
** WELL TEST DATA PRINTOUT **
****

COMPANY: JACK EXPLORATION
WELL: #1-16

FIELD REPORT NO. 190410
INSTRUMENT NO. 13362

RECORDER CAPACITY: 4450 PSI PORT OPENING: OUTSIDE DEPTH: 0 FT
TEMPERATURE: 124 DEG F

LABEL POINT INFORMATION
****

#	TIME OF DAY HH:MM:SS	DATE DD-MMM	EXPLANATION	ELAPSED TIME,MIN	BOT HOLE PRESSURE PSIA
1	11:59:00	13-JUL	HYDROSTATIC MUD	-1.00	2282
2	12:00:00	13-JUL	START FLOW	0.00	166
3	12:30:00	13-JUL	END FLOW & START SHUT-IN	30.00	155
4	13:33:00	13-JUL	END SHUT-IN	93.00	1812
5	13:33:00	13-JUL	START FLOW	93.00	161
6	14:28:00	13-JUL	END FLOW & START SHUT-IN	148.00	118
7	16:29:00	13-JUL	END SHUT-IN	269.00	1648
8	16:30:00	13-JUL	HYDROSTATIC MUD	270.00	2202

SUMMARY OF FLOW PERIODS
****

PERIOD	START ELAPSED TIME,MIN	END ELAPSED TIME,MIN	DURATION MIN	START PRESSURE PSIA	END PRESSURE PSIA	INITIAL PRESSURE PSIA
1	0.00	30.00	30.00	166	155	166
2	93.00	148.00	55.00	161	118	161

SUMMARY OF SHUTIN PERIODS
****

PERIOD	START ELAPSED TIME,MIN	END ELAPSED TIME,MIN	DURATION MIN	START PRESSURE PSIA	END PRESSURE PSIA	FINAL FLOW PRESSURE PSIA	PRODUCING TIME, MIN
1	30.00	93.00	63.00	155	1812	155	30.00
2	148.00	269.00	121.00	118	1648	118	85.00

TEST PHASE: FLOW PERIOD # 1

TIME OF DAY HH:MM:SS	DATE DD-MMM	ELAPSED TIME,MIN	DELTA TIME,MIN	BOT HOLE PRESSURE PSIA
12:00:00	13-JUL	0.00	0.00	166
12:15:00	13-JUL	15.00	15.00	160
12:30:00	13-JUL	30.00	30.00	155

TEST PHASE: SHUTIN PERIOD # 1

FINAL FLOW PRESSURE = 155 PSIA
PRODUCING TIME = 30.00 MIN

TIME OF DAY HH:MM:SS	DATE DD-MMM	ELAPSED TIME,MIN	DELTA TIME,MIN	BOT HOLE PRESSURE PSIA	DELTA P PSI	LOG HORNER TIME
12:30:00	13-JUL	30.00	0.00	155	0	
12:33:00	13-JUL	33.00	3.00	275	120	1.0414
12:36:00	13-JUL	36.00	6.00	740	585	0.7782
12:39:00	13-JUL	39.00	9.00	1232	1077	0.6368
12:42:00	13-JUL	42.00	12.00	1544	1389	0.5441
12:45:00	13-JUL	45.00	15.00	1672	1517	0.4771
12:48:00	13-JUL	48.00	18.00	1744	1589	0.4260
12:51:00	13-JUL	51.00	21.00	1772	1617	0.3854
12:54:00	13-JUL	54.00	24.00	1785	1630	0.3522
12:57:00	13-JUL	57.00	27.00	1794	1639	0.3245
13:00:00	13-JUL	60.00	30.00	1798	1643	0.3010
13:06:00	13-JUL	66.00	36.00	1804	1649	0.2632
13:12:00	13-JUL	72.00	42.00	1806	1651	0.2341
13:18:00	13-JUL	78.00	48.00	1808	1653	0.2109
13:24:00	13-JUL	84.00	54.00	1810	1655	0.1919
13:30:00	13-JUL	90.00	60.00	1812	1657	0.1761
13:33:00	13-JUL	93.00	63.00	1812	1657	0.1691

TEST PHASE: FLOW PERIOD # 2

TIME OF DAY HH:MM:SS	DATE DD-MMM	ELAPSED TIME,MIN	DELTA TIME,MIN	BOT HOLE PRESSURE PSIA
13:33:00	13-JUL	93.00	0.00	161
13:48:00	13-JUL	108.00	15.00	135
14:03:00	13-JUL	123.00	30.00	117
14:18:00	13-JUL	138.00	45.00	114
14:28:00	13-JUL	148.00	55.00	118

TEST PHASE: SHUTIN PERIOD # 2

FINAL FLOW PRESSURE = 118 PSIA
PRODUCING TIME = 85.00 MIN

TIME OF DAY HH:MM:SS	DATE DD-MMM	ELAPSED TIME,MIN	DELTA TIME,MIN	BOT HOLE PRESSURE PSIA	DELTA P PSI	LOG HORNER TIME
14:28:00	13-JUL	148.00	0.00	118	0	
14:31:00	13-JUL	151.00	3.00	248	130	1.4674
14:34:00	13-JUL	154.00	6.00	749	631	1.1809

TEST PHASE: SHUTIN PERIOD # 2 FINAL FLOW PRESSURE = 118 PSIA
PRODUCING TIME = 85.00 MIN

TIME OF DAY HH:MM:SS	DATE DD-MMM	ELAPSED TIME,MIN	DELTA TIME,MIN	BOT HOLE PRESSURE PSIA	DELTA P PSI	LOG HORNER TIME
14:37:00	13-JUL	157.00	9.00	1158	1040	1.0189
14:40:00	13-JUL	160.00	12.00	1376	1258	0.9076
14:43:00	13-JUL	163.00	15.00	1492	1374	0.8239
14:46:00	13-JUL	166.00	18.00	1553	1435	0.7576
14:49:00	13-JUL	169.00	21.00	1581	1463	0.7031
14:52:00	13-JUL	172.00	24.00	1593	1475	0.6572
14:55:00	13-JUL	175.00	27.00	1602	1484	0.6179
14:58:00	13-JUL	178.00	30.00	1608	1490	0.5836
15:04:00	13-JUL	184.00	36.00	1614	1496	0.5265
15:10:00	13-JUL	190.00	42.00	1617	1499	0.4806
15:16:00	13-JUL	196.00	48.00	1619	1501	0.4426
15:22:00	13-JUL	202.00	54.00	1621	1503	0.4106
15:28:00	13-JUL	208.00	60.00	1623	1505	0.3832
15:34:00	13-JUL	214.00	66.00	1626	1508	0.3594
15:40:00	13-JUL	220.00	72.00	1630	1512	0.3386
15:46:00	13-JUL	226.00	78.00	1634	1516	0.3201
15:51:00	13-JUL	231.00	83.00	1636	1518	0.3062
15:57:00	13-JUL	237.00	89.00	1638	1520	0.2912
16:03:00	13-JUL	243.00	95.00	1640	1522	0.2775
16:09:00	13-JUL	249.00	101.00	1642	1524	0.2652
16:14:00	13-JUL	254.00	106.00	1644	1526	0.2557
16:20:00	13-JUL	260.00	112.00	1646	1528	0.2452
16:26:00	13-JUL	266.00	118.00	1648	1530	0.2356
16:29:00	13-JUL	269.00	121.00	1648	1530	0.2311