

JOHNSON "B"
LEASE NAME

1
WELL NO.

1
TEST NO.

3401.0 - 3425.0
TESTED INTERVAL

← WELL FILE

K & E PETROLEUM INCORPORATED
LEASE OWNER/COMPANY NAME

LEGAL LOCATION
SEC. - TWP. - RNG.

33-6-21

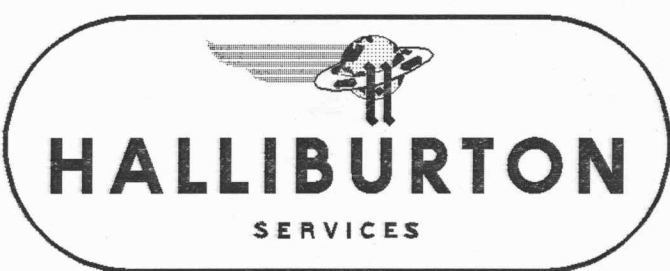
FIELD
AREA

COUNTY

GRAHAM

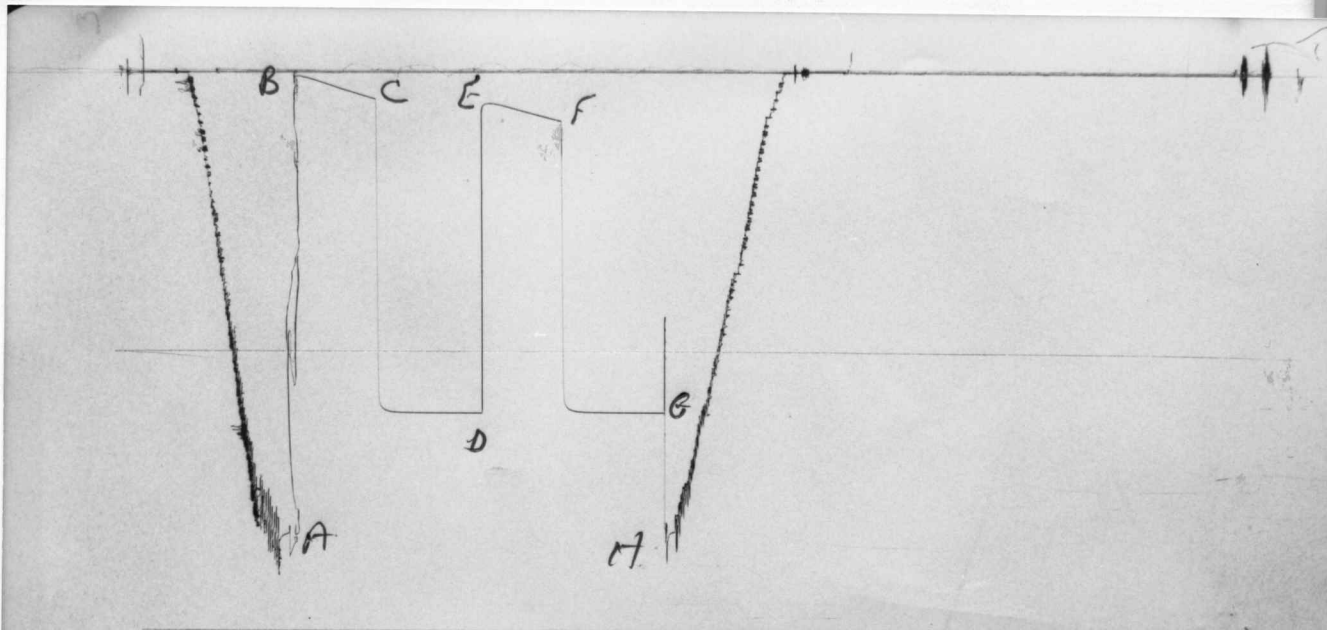
STATE

KANSAS OR



TICKET NO. 41953300
06-OCT-86
HAYS

FORMATION TESTING SERVICE REPORT

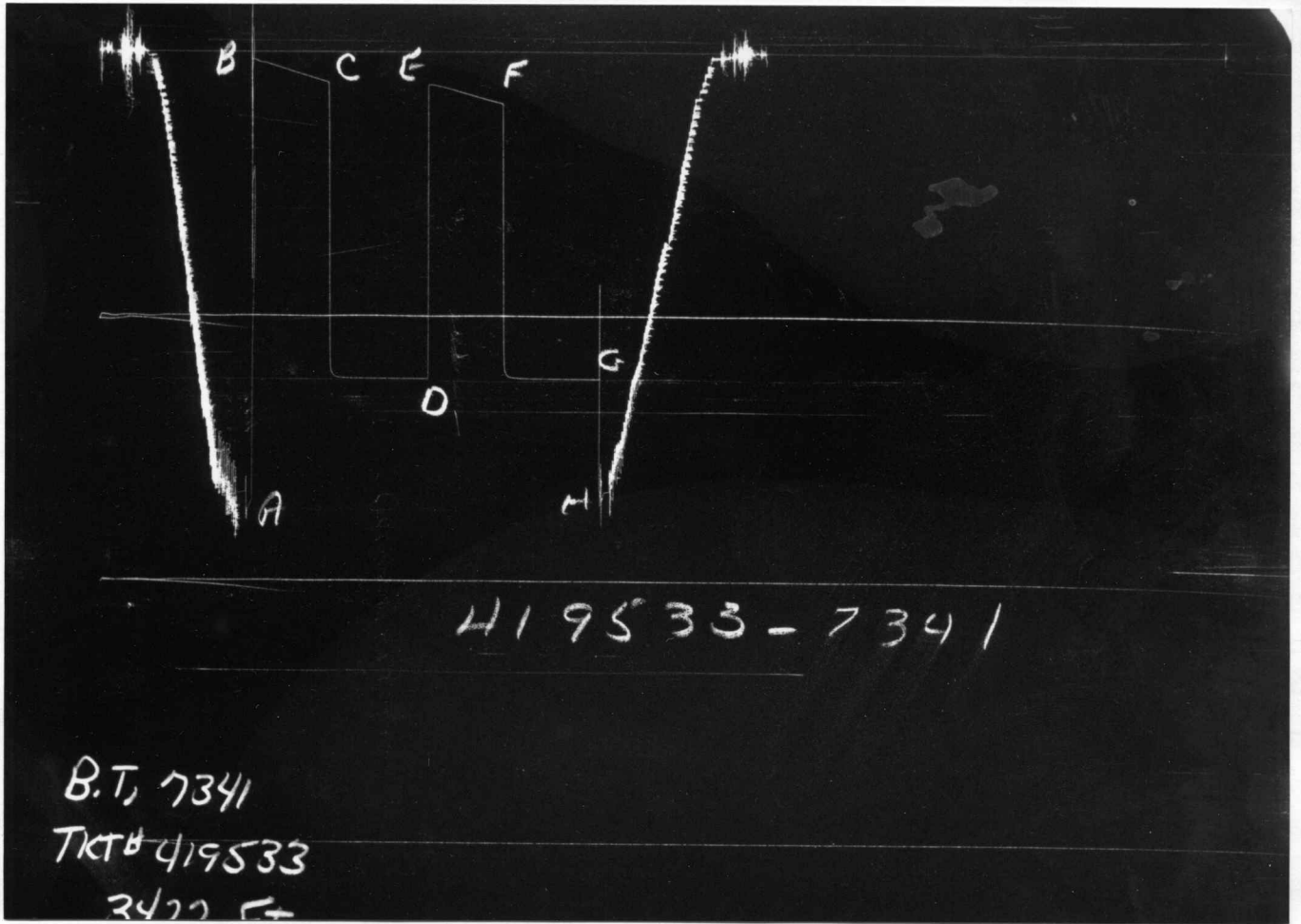


419533 - 7342

BT. 7342
TKT# 419533

GAUGE NO: 7342 DEPTH: 3388.0 BLANKED OFF: NO HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		1651.5			
B	INITIAL FIRST FLOW		18.4			
C	FINAL FIRST FLOW		97.5	45.0	46.4	F
C	INITIAL FIRST CLOSED-IN		97.5			
D	FINAL FIRST CLOSED-IN		1219.2	60.0	59.8	C
E	INITIAL SECOND FLOW		141.1			
F	FINAL SECOND FLOW		176.3	45.0	45.5	F
F	INITIAL SECOND CLOSED-IN		176.3			
G	FINAL SECOND CLOSED-IN		1217.7	60.0	58.3	C
H	FINAL HYDROSTATIC		1644.5			



GAUGE NO: 7341 DEPTH: 3422.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	1658	1662.8			
B	INITIAL FIRST FLOW	19	27.1			
C	FINAL FIRST FLOW	112	115.4	45.0	46.4	F
C	INITIAL FIRST CLOSED-IN	112	115.4			
D	FINAL FIRST CLOSED-IN	1230	1234.1	60.0	59.8	C
E	INITIAL SECOND FLOW	112	127.1			
F	FINAL SECOND FLOW	187	195.3	45.0	45.5	F
F	INITIAL SECOND CLOSED-IN	187	195.3			
G	FINAL SECOND CLOSED-IN	1230	1233.7	60.0	58.3	C
H	FINAL HYDROSTATIC	1658	1659.8			

EQUIPMENT & HOLE DATA

FORMATION TESTED: TOPEKA
 NET PAY (ft): 6.0
 GROSS TESTED FOOTAGE: 24.0
 ALL DEPTHS MEASURED FROM: KELLY BUSHING
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.875
 ELEVATION (ft): 2235.0
 TOTAL DEPTH (ft): 3425.0
 PACKER DEPTH(S) (ft): 3395, 3401
 FINAL SURFACE CHOKE (in): _____
 BOTTOM HOLE CHOKE (in): 0.750
 MUD WEIGHT (lb/gal): 9.30
 MUD VISCOSITY (sec): 46
 ESTIMATED HOLE TEMP. (°F): _____
 ACTUAL HOLE TEMP. (°F): 94 @ 3420.0 ft

TICKET NUMBER: 41953300

DATE: 9-30-86 TEST NO: 1

TYPE DST: OPEN HOLE

HALLIBURTON CAMP:
HAYS

TESTER: MEL CHILDERS

WITNESS: TIM PRIEST

DRILLING CONTRACTOR:
ABERCROMBIE #4

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES
SAMPLE OF DST	_____ @ _____ °F	<u>58480</u> ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

SAMPLER DATA

Psig AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ @ _____ °F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE AMOUNT WEIGHT

RECOVERED:

347' OF SLIGHTLY OIL CUT WATERY MUD
 160' OF (5% OIL, 5% WATER, 88% MUD AND 2% SOLIDS)
 64' OF (5% OIL, 50% WATER, 43% MUD AND 2% SOLIDS)
 123' OF (1% OIL, 96% WATER AND 3% SOLIDS)

MEASURED FROM
TESTER VALVE

REMARKS:

TICKET NO: 41953300

CLOCK NO: 4205 HOUR: 12



GAUGE NO: 7342

DEPTH: 3388.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	18.4			
2	5.0	19.8	1.4		
3	10.0	27.6	7.8		
4	15.0	37.6	10.0		
5	20.0	47.4	9.8		
6	25.0	58.3	10.8		
7	30.0	68.1	9.8		
8	35.0	77.3	9.3		
9	40.0	87.6	10.3		
10	45.0	96.2	8.6		
C 11	46.4	97.5	1.3		
FIRST CLOSED-IN					
C 1	0.0	97.5			
2	1.0	1183.2	1085.7	1.0	1.680
3	2.0	1198.1	1100.6	1.9	1.382
4	3.0	1204.8	1107.3	2.9	1.211
5	4.0	1208.7	1111.1	3.7	1.101
6	5.0	1211.3	1113.8	4.5	1.009
7	6.0	1213.1	1115.6	5.3	0.942
8	7.0	1214.9	1117.4	6.1	0.881
9	8.0	1215.7	1118.2	6.8	0.833
10	9.0	1216.5	1119.0	7.5	0.789
11	10.0	1217.2	1119.7	8.2	0.751
12	12.0	1217.9	1120.4	9.5	0.686
13	14.0	1218.3	1120.8	10.7	0.635
14	16.0	1218.6	1121.1	11.9	0.591
15	18.0	1218.6	1121.1	13.0	0.553
16	20.0	1218.6	1121.1	14.0	0.521
17	22.0	1218.6	1121.1	14.9	0.492
18	24.0	1219.3	1121.8	15.8	0.467
19	26.0	1219.3	1121.8	16.7	0.444
20	28.0	1219.2	1121.7	17.5	0.424
21	30.0	1219.1	1121.6	18.2	0.405
22	35.0	1219.1	1121.6	19.9	0.367
23	40.0	1219.2	1121.7	21.5	0.334
24	45.0	1219.2	1121.7	22.8	0.308
25	50.0	1219.2	1121.7	24.1	0.285
26	55.0	1219.2	1121.7	25.1	0.266
D 27	59.8	1219.2	1121.7	26.1	0.249
SECOND FLOW					
E 1	0.0	141.1			
2	5.0	113.8	-27.3		
3	10.0	117.5	3.6		
4	15.0	125.5	8.0		
5	20.0	133.8	8.3		
6	25.0	142.5	8.7		

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
7	30.0	151.5	9.0		
8	35.0	160.0	8.5		
9	40.0	167.9	7.9		
F 10	45.5	176.3	8.4		
SECOND CLOSED-IN					
F 1	0.0	176.3			
2	1.0	1179.8	1003.6	1.0	1.980
3	2.0	1196.0	1019.7	1.9	1.674
4	3.0	1203.0	1026.7	2.9	1.499
5	4.0	1207.0	1030.7	3.8	1.382
6	5.0	1209.3	1033.0	4.8	1.286
7	6.0	1211.2	1034.9	5.6	1.212
8	7.0	1212.8	1036.5	6.5	1.147
9	8.0	1214.0	1037.7	7.3	1.097
10	9.0	1214.5	1038.3	8.2	1.048
11	10.0	1214.9	1038.6	9.0	1.007
12	12.0	1215.7	1039.5	10.6	0.938
13	14.0	1216.3	1040.0	12.1	0.879
14	16.0	1217.0	1040.7	13.6	0.829
15	18.0	1217.3	1041.1	15.1	0.785
16	20.0	1217.7	1041.4	16.4	0.748
17	22.0	1217.7	1041.4	17.7	0.714
18	24.0	1217.7	1041.4	19.0	0.684
19	26.0	1217.7	1041.4	20.2	0.657
20	28.0	1217.7	1041.4	21.5	0.631
21	30.0	1217.7	1041.4	22.6	0.609
22	35.0	1217.7	1041.4	25.4	0.559
23	40.0	1217.7	1041.4	27.9	0.518
24	45.0	1217.7	1041.4	30.2	0.483
25	50.0	1217.7	1041.4	32.4	0.453
26	55.0	1217.7	1041.4	34.4	0.427
G 27	58.3	1217.7	1041.4	35.7	0.411

REMARKS:

TICKET NO: 41953300

CLOCK NO: 3930 HOUR: 12



GAUGE NO: 7341














DEPTH: 3422.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	27.1			
2	5.0	38.6	11.4		
3	10.0	44.4	5.8		
4	15.0	54.3	9.9		
5	20.0	64.4	10.1		
6	25.0	74.9	10.5		
7	30.0	84.2	9.3		
8	35.0	94.2	10.0		
9	40.0	103.4	9.2		
10	45.0	112.7	9.4		
C 11	46.4	115.4	2.7		
FIRST CLOSED-IN					
C 1	0.0	115.4			
2	1.0	1201.2	1085.7	1.0	1.674
3	2.0	1217.4	1101.9	1.9	1.385
4	3.0	1223.9	1108.4	2.8	1.219
5	4.0	1227.2	1111.8	3.7	1.103
6	5.0	1229.4	1114.0	4.5	1.015
7	6.0	1230.2	1114.7	5.4	0.938
8	7.0	1230.6	1115.2	6.1	0.881
9	8.0	1231.1	1115.7	6.8	0.832
10	9.0	1231.1	1115.7	7.5	0.790
11	10.0	1231.7	1116.2	8.2	0.751
12	12.0	1232.4	1117.0	9.5	0.688
13	14.0	1232.4	1117.0	10.7	0.636
14	16.0	1232.9	1117.4	11.9	0.591
15	18.0	1232.9	1117.4	13.0	0.553
16	20.0	1232.9	1117.4	14.0	0.521
17	22.0	1233.2	1117.7	14.9	0.492
18	24.0	1233.2	1117.7	15.8	0.467
19	26.0	1233.2	1117.7	16.7	0.444
20	28.0	1233.2	1117.7	17.5	0.424
21	30.0	1233.3	1117.9	18.2	0.406
22	35.0	1233.7	1118.3	19.9	0.366
23	40.0	1233.7	1118.3	21.5	0.334
24	45.0	1233.7	1118.3	22.8	0.308
25	50.0	1233.7	1118.3	24.1	0.285
26	55.0	1233.7	1118.3	25.2	0.265
D 27	59.8	1234.1	1118.6	26.1	0.249
SECOND FLOW					
E 1	0.0	127.1			
2	5.0	127.0	-0.1		
3	10.0	134.0	7.0		
4	15.0	142.4	8.4		
5	20.0	150.9	8.4		
6	25.0	160.3	9.5		

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
7	30.0	170.0	9.6		
8	35.0	178.2	8.2		
9	40.0	186.5	8.2		
F 10	45.5	195.3	8.8		
SECOND CLOSED-IN					
F 1	0.0	195.3			
2	1.0	1205.0	1009.7	1.0	1.967
3	2.0	1219.5	1024.2	2.0	1.664
4	3.0	1224.4	1029.1	2.9	1.497
5	4.0	1227.3	1032.0	3.9	1.375
6	5.0	1228.1	1032.9	4.7	1.290
7	6.0	1229.2	1034.0	5.6	1.212
8	7.0	1230.0	1034.7	6.5	1.149
9	8.0	1230.4	1035.1	7.3	1.098
10	9.0	1230.9	1035.7	8.2	1.052
11	10.0	1231.2	1035.9	9.0	1.010
12	12.0	1231.7	1036.4	10.6	0.937
13	14.0	1232.2	1037.0	12.1	0.880
14	16.0	1232.2	1037.0	13.6	0.829
15	18.0	1232.6	1037.3	15.0	0.786
16	20.0	1232.9	1037.6	16.4	0.748
17	22.0	1232.9	1037.6	17.8	0.714
18	24.0	1233.2	1038.0	19.0	0.684
19	26.0	1233.3	1038.1	20.3	0.656
20	28.0	1233.4	1038.2	21.4	0.632
21	30.0	1233.6	1038.4	22.6	0.609
22	35.0	1233.6	1038.4	25.3	0.560
23	40.0	1233.7	1038.4	27.9	0.518
24	45.0	1233.7	1038.4	30.2	0.483
25	50.0	1233.7	1038.4	32.4	0.453
26	55.0	1233.7	1038.4	34.4	0.427
G 27	58.3	1233.7	1038.4	35.7	0.411

REMARKS:

TICKET NO. 41953300

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	2774.5	
4		FLEX WEIGHT.....	4.500	2.950	346.7	
50		IMPACT REVERSING SUB.....	5.750	2.750	1.0	3122.0
4		FLEX WEIGHT.....	4.500	2.950	252.9	
5		CROSSOVER.....	5.000	2.950	1.0	
12		DUAL CIP VALVE.....	5.000	0.870	6.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	3386.0
80		AP RUNNING CASE.....	5.000	2.250	4.1	3388.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3395.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3401.0
20		FLUSH JOINT ANCHOR.....	5.000	2.370	16.4	
83		HT-500 TEMPERATURE CASE.....	5.000		1.5	3420.0
81		BLANKED-OFF RUNNING CASE.....	5.000		4.3	3422.0
TOTAL DEPTH					3425.0	

EQUIPMENT DATA

TEMPERATURE

RECORDER

CHART



10° each circle

EQUATIONS FOR DST GAS WELL ANALYSIS

Indicated Flow Capacity	$kh = \frac{.001637 Q_g T}{m}$	md-ft
Average Effective Permeability	$k = \frac{kh}{h}$	md
Skin Factor	$S = 1.151 \left[\frac{m(P^*) - m(P_i)}{m} - \text{LOG} \left(\frac{k (t/60)}{\phi \mu c_i r_w^2} \right) + 3.23 \right]$	
Damage Ratio	$DR = \frac{m(P^*) - m(P_i)}{m(P^*) - m(P_i) - 0.87 mS}$	
Indicated Flow Rate (Maximum)	$AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_i)}$	MCFD
Indicated Flow Rate (Minimum)	$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_i)}}$	MCFD
Approx. Radius of Investigation	$r_i = 0.032 \sqrt{\frac{k (t/60)}{\phi \mu c_i}}$	ft

JOHNSON "B"

LEASE NAME

WELL NO. 1

TEST NO. 2

3447.0 - 3490.0

TESTED INTERVAL

WELL K & E PETROLEUM, INCORPORATED

LEGAL LOCATION

SEC. - TWP. - RNG. 33 - 6 - 21

FIELD AREA

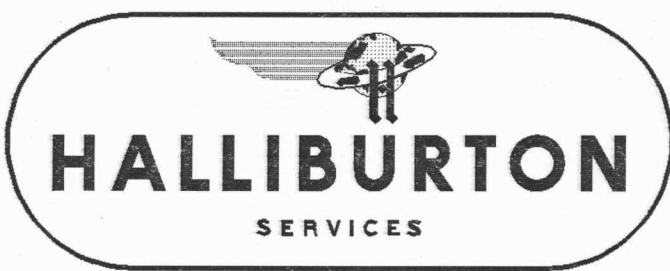
COUNTY

GRAHAM

STATE

KANSAS

PW

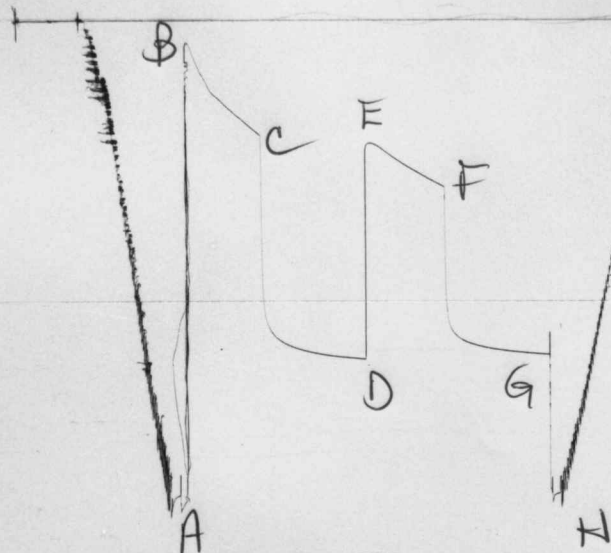


TICKET NO. 41953200

06-OCT-86

HAYS

FORMATION TESTING SERVICE REPORT

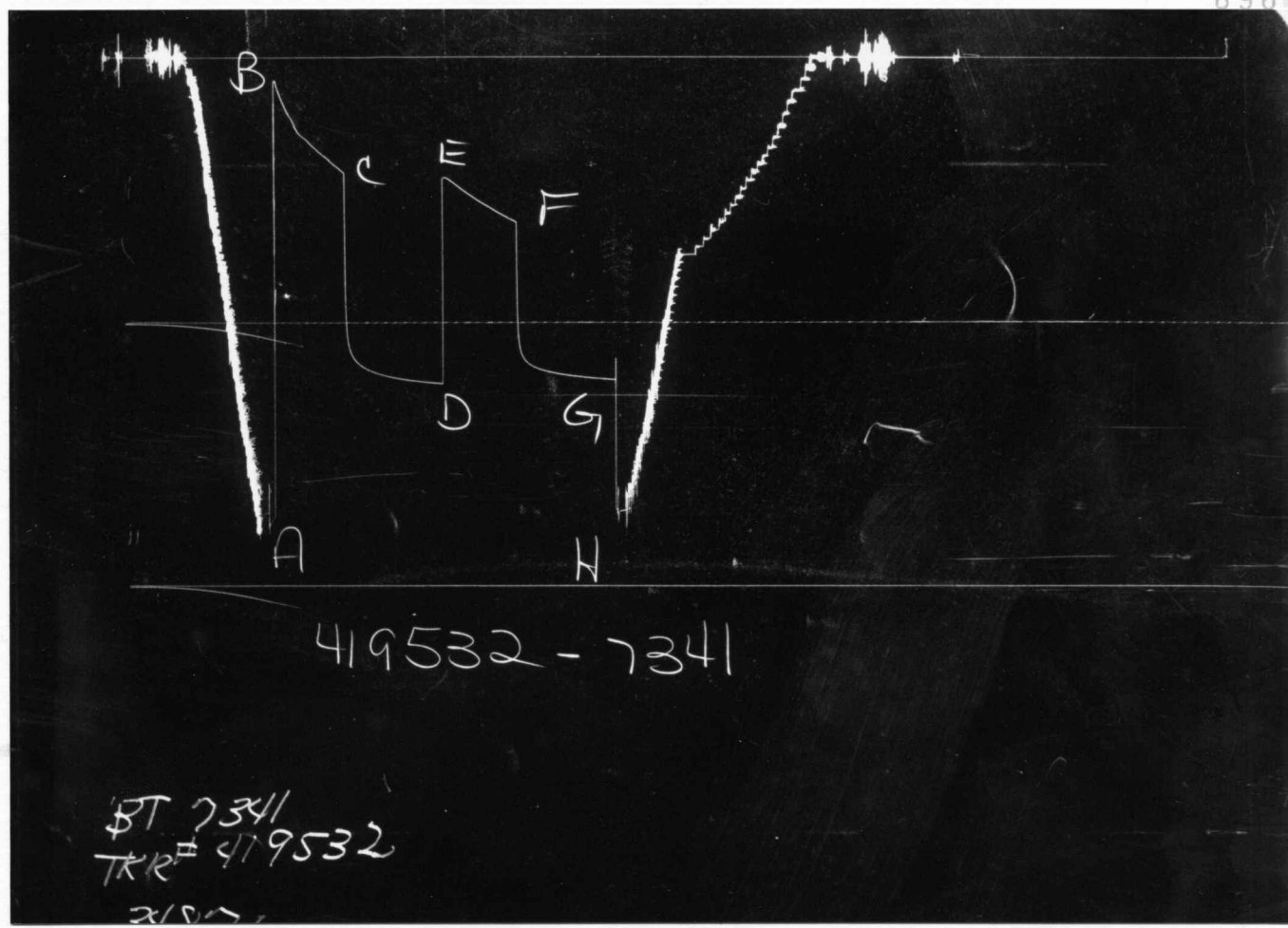


419532 - 7342

BT# 7342
TKT# 419532
3434 FT

GAUGE NO: 7342 DEPTH: 3434.0 BLANKED OFF: NO HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		1700.7			
B	INITIAL FIRST FLOW		81.1			
C	FINAL FIRST FLOW		410.1	44.0	43.2	F
C	INITIAL FIRST CLOSED-IN		410.1			
D	FINAL FIRST CLOSED-IN		1209.3	60.0	60.2	C
E	INITIAL SECOND FLOW		438.7			
F	FINAL SECOND FLOW		595.3	45.0	45.2	F
F	INITIAL SECOND CLOSED-IN		595.3			
G	FINAL SECOND CLOSED-IN		1193.1	60.0	60.4	C
H	FINAL HYDROSTATIC		1691.5			



419532-7341

BT 7341
TRR# 419532
2/18/7

GAUGE NO: 7341 DEPTH: 3487.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	1714	1723.8			
B	INITIAL FIRST FLOW	75	86.5			
C	FINAL FIRST FLOW	431	439.0	44.0	43.2	F
C	INITIAL FIRST CLOSED-IN	431	439.0			
D	FINAL FIRST CLOSED-IN	1230	1233.5	60.0	60.2	C
E	INITIAL SECOND FLOW	449	455.5			
F	FINAL SECOND FLOW	617	624.6	45.0	45.2	F
F	INITIAL SECOND CLOSED-IN	617	624.6			
G	FINAL SECOND CLOSED-IN	1211	1218.8	60.0	60.4	C
H	FINAL HYDROSTATIC	1714	1715.0			

EQUIPMENT & HOLE DATA

FORMATION TESTED: TORONTO
 NET PAY (ft): 4.0
 GROSS TESTED FOOTAGE: 43.0
 ALL DEPTHS MEASURED FROM: KB
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.875
 ELEVATION (ft): 2235.0
 TOTAL DEPTH (ft): 3490.0
 PACKER DEPTH(S) (ft): 3441, 3447
 FINAL SURFACE CHOKE (in): _____
 BOTTOM HOLE CHOKE (in): 0.750
 MUD WEIGHT (lb/gal): 9.50
 MUD VISCOSITY (sec): 45
 ESTIMATED HOLE TEMP. (°F): _____
 ACTUAL HOLE TEMP. (°F): 96 @ 3485.0 ft

TICKET NUMBER: 41953200

DATE: 9-30-86 TEST NO: 2

TYPE DST: OPEN HOLE

HALLIBURTON CAMP:
HAYS

TESTER: MEL CHILDERS

WITNESS: TIM PRIEST

DRILLING CONTRACTOR:
ABERCROMBIE #4

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES
DST SAMPLE	_____ @ _____ °F	<u>60200</u> ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

SAMPLER DATA

Pstg AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): 38.0 @ 70°F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____

RECOVERED:

527 FEET OF CLEAN GASSY OIL
 589 FEET OF MUD CUT OIL OF WHICH 322' = 22% MUD -
 3% WATER - 75% OIL; 267' = 35% MUD - 8% WATER -
 57% OIL
 129 FEET OF MUDDY WATER (5% OIL/10% MUD/85% WATER)

MEASURED FROM
TESTER VALVE

REMARKS:

RECOVERY CONTINUED:
 248 FEET OF WATER
 1488 FEET OF TOTAL FLUID RECOVERED

TICKET NO: 41953200

CLOCK NO: 4205 HOUR: 12



GAUGE NO: 7342

DEPTH: 3434.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	81.1			
2	3.0	100.8	19.7		
3	6.0	148.3	47.5		
4	9.0	190.9	42.6		
5	12.0	222.3	31.4		
6	15.0	257.8	35.4		
7	18.0	274.3	16.5		
8	21.0	291.9	17.6		
9	24.0	310.7	18.8		
10	27.0	327.4	16.7		
11	30.0	342.7	15.3		
12	33.0	357.8	15.0		
13	36.0	375.1	17.3		
14	39.0	389.9	14.8		
15	42.0	405.1	15.2		
C 16	43.2	410.1	5.0		
FIRST CLOSED-IN					
C 1	0.0	410.1			
2	1.0	980.9	570.8	1.0	1.628
3	2.0	1040.9	630.8	1.9	1.347
4	3.0	1071.1	660.9	2.8	1.183
5	4.0	1088.7	678.6	3.7	1.068
6	5.0	1102.5	692.4	4.5	0.983
7	6.0	1112.8	702.6	5.3	0.911
8	7.0	1120.4	710.3	6.0	0.855
9	8.0	1127.9	717.7	6.8	0.805
10	9.0	1133.1	723.0	7.5	0.761
11	10.0	1138.5	728.4	8.1	0.726
12	12.0	1146.5	736.4	9.4	0.663
13	14.0	1153.7	743.6	10.6	0.612
14	16.0	1159.7	749.6	11.7	0.568
15	18.0	1165.9	755.7	12.7	0.532
16	20.0	1170.0	759.8	13.7	0.500
17	22.0	1173.9	763.7	14.6	0.471
18	24.0	1177.2	767.1	15.4	0.447
19	26.0	1180.6	770.5	16.2	0.425
20	28.0	1183.7	773.5	17.0	0.405
21	30.0	1186.3	776.1	17.7	0.387
22	35.0	1192.2	782.0	19.3	0.349
23	40.0	1196.8	786.7	20.8	0.318
24	45.0	1200.6	790.4	22.0	0.292
25	50.0	1203.5	793.3	23.2	0.270
26	55.0	1206.3	796.2	24.2	0.252
D 27	60.2	1209.3	799.2	25.1	0.235
SECOND FLOW					
E 1	0.0	438.7			

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
2	3.0	438.4	-0.3		
3	6.0	444.0	5.6		
4	9.0	455.7	11.7		
5	12.0	469.8	14.1		
6	15.0	483.4	13.6		
7	18.0	497.0	13.6		
8	21.0	509.9	12.9		
9	24.0	521.2	11.3		
10	27.0	531.9	10.7		
11	30.0	542.7	10.8		
12	33.0	553.5	10.9		
13	36.0	564.5	11.0		
14	39.0	574.2	9.7		
15	42.0	583.9	9.7		
F 16	45.2	595.3	11.4		
SECOND CLOSED-IN					
F 1	0.0	595.3			
2	1.0	1008.8	413.4	1.0	1.946
3	2.0	1067.3	472.0	2.0	1.653
4	3.0	1089.9	494.6	2.9	1.487
5	4.0	1103.8	508.5	3.8	1.363
6	5.0	1112.8	517.5	4.7	1.273
7	6.0	1120.4	525.1	5.7	1.194
8	7.0	1125.8	530.4	6.5	1.135
9	8.0	1131.1	535.8	7.3	1.081
10	9.0	1135.7	540.3	8.2	1.033
11	10.0	1139.4	544.1	9.0	0.994
12	12.0	1146.6	551.3	10.6	0.922
13	14.0	1151.1	555.7	12.1	0.865
14	16.0	1154.8	559.5	13.5	0.815
15	18.0	1159.0	563.7	15.0	0.771
16	20.0	1163.0	567.7	16.3	0.734
17	22.0	1166.0	570.7	17.6	0.700
18	24.0	1168.6	573.3	18.9	0.670
19	26.0	1171.0	575.6	20.1	0.643
20	28.0	1173.1	577.8	21.3	0.619
21	30.0	1174.9	579.6	22.4	0.596
22	35.0	1179.6	584.3	25.1	0.547
23	40.0	1183.0	587.7	27.5	0.506
24	45.0	1186.3	590.9	29.8	0.472
25	50.0	1188.9	593.6	31.9	0.442
26	55.0	1191.7	596.4	33.9	0.416
G 27	60.4	1193.1	597.8	35.9	0.391

REMARKS:

TICKET NO: 41953200
 CLOCK NO: 3930 HOUR: 12
















GAUGE NO: 7341
 DEPTH: 3487.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B	1	0.0	86.5		
	2	3.0	129.3	42.9	
	3	6.0	176.0	46.6	
	4	9.0	214.7	38.7	
	5	12.0	246.6	31.9	
	6	15.0	285.4	38.8	
	7	18.0	302.2	16.9	
	8	21.0	318.6	16.4	
	9	24.0	337.4	18.7	
	10	27.0	354.7	17.3	
	11	30.0	370.4	15.7	
	12	33.0	384.9	14.5	
	13	36.0	402.7	17.8	
	14	39.0	418.1	15.4	
	15	42.0	434.1	16.0	
C	16	43.2	439.0	4.9	
FIRST CLOSED-IN					
C	1	0.0	439.0		
	2	1.0	967.9	529.0	1.0 1.652
	3	2.0	1064.1	625.1	1.9 1.348
	4	3.0	1097.4	658.4	2.8 1.190
	5	4.0	1118.3	679.3	3.7 1.069
	6	5.0	1130.2	691.2	4.4 0.987
	7	6.0	1140.7	701.7	5.3 0.914
	8	7.0	1148.6	709.6	6.1 0.853
	9	8.0	1155.5	716.5	6.8 0.804
	10	9.0	1160.4	721.4	7.4 0.763
	11	10.0	1165.4	726.4	8.1 0.727
	12	12.0	1173.8	734.8	9.4 0.662
	13	14.0	1180.7	741.8	10.6 0.611
	14	16.0	1185.8	746.8	11.7 0.568
	15	18.0	1191.0	752.0	12.7 0.532
	16	20.0	1195.1	756.2	13.7 0.500
	17	22.0	1199.1	760.2	14.6 0.471
	18	24.0	1202.5	763.5	15.4 0.447
	19	26.0	1205.7	766.8	16.2 0.424
	20	28.0	1208.3	769.4	17.0 0.405
	21	30.0	1210.7	771.7	17.7 0.387
	22	35.0	1216.4	777.5	19.3 0.349
	23	40.0	1220.9	781.9	20.8 0.318
	24	45.0	1224.4	785.5	22.0 0.292
	25	50.0	1228.1	789.2	23.2 0.270
	26	55.0	1230.4	791.4	24.2 0.252
D	27	60.2	1233.5	794.6	25.1 0.235
SECOND FLOW					
E	1	0.0	455.5		

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
	2	3.0	459.3	3.8	
	3	6.0	472.8	13.5	
	4	9.0	486.5	13.7	
	5	12.0	500.6	14.0	
	6	15.0	513.9	13.3	
	7	18.0	527.0	13.1	
	8	21.0	539.0	12.1	
	9	24.0	551.2	12.2	
	10	27.0	560.9	9.8	
	11	30.0	571.8	10.9	
	12	33.0	583.2	11.4	
	13	36.0	593.8	10.6	
	14	39.0	604.6	10.8	
	15	42.0	613.9	9.3	
F	16	45.2	624.6	10.8	
SECOND CLOSED-IN					
F	1	0.0	624.6		
	2	1.0	1035.6	410.9	1.0 1.952
	3	2.0	1095.7	471.0	1.9 1.663
	4	3.0	1120.2	495.6	2.9 1.481
	5	4.0	1133.2	508.6	3.8 1.363
	6	5.0	1143.0	518.4	4.7 1.272
	7	6.0	1150.0	525.3	5.6 1.199
	8	7.0	1155.7	531.0	6.5 1.136
	9	8.0	1161.3	536.7	7.3 1.081
	10	9.0	1165.2	540.6	8.2 1.035
	11	10.0	1168.8	544.1	9.0 0.994
	12	12.0	1174.6	549.9	10.5 0.923
	13	14.0	1179.8	555.1	12.1 0.865
	14	16.0	1183.5	558.8	13.5 0.815
	15	18.0	1186.4	561.7	15.0 0.771
	16	20.0	1189.5	564.9	16.3 0.734
	17	22.0	1192.1	567.5	17.6 0.700
	18	24.0	1195.1	570.5	18.9 0.671
	19	26.0	1196.9	572.2	20.1 0.644
	20	28.0	1199.3	574.7	21.3 0.619
	21	30.0	1201.2	576.5	22.4 0.596
	22	35.0	1204.9	580.2	25.1 0.547
	23	40.0	1208.1	583.5	27.5 0.507
	24	45.0	1211.1	586.5	29.8 0.472
	25	50.0	1213.7	589.1	31.9 0.442
	26	55.0	1216.6	592.0	33.9 0.416
G	27	60.4	1218.8	594.2	35.9 0.391

REMARKS:

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	2820.8	
4		FLEX WEIGHT.....	4.500	2.950	346.7	
50		IMPACT REVERSING SUB.....	5.750	2.750	1.0	3167.2
4		FLEX WEIGHT.....	4.500	2.950	252.9	
5		CROSSOVER.....	5.000	2.950	1.0	
12		DUAL CIP VALVE.....	5.000	0.870	6.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	3432.0
80		AP RUNNING CASE.....	5.000	2.250	4.1	3434.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3441.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3447.0
20		FLUSH JOINT ANCHOR.....	5.000	2.370	35.4	
83		HT-500 TEMPERATURE CASE.....	5.000		1.5	3485.0
81		BLANKED-OFF RUNNING CASE.....	5.000		4.3	3487.0
TOTAL DEPTH					3490.0	

EQUIPMENT DATA

TEMPERATURE

RECORDER

CHART



10° each circle

EQUATIONS FOR DST GAS WELL ANALYSIS

Indicated Flow Capacity $kh = \frac{.001637 Q_g T}{m}$ md-ft

Average Effective Permeability $k = \frac{kh}{h}$ md

Skin Factor $S = 1.151 \left[\frac{m(P^*) - m(P_i)}{m} - \text{LOG} \left(\frac{k (t/60)}{\phi \mu c_i r_w^2} \right) + 3.23 \right]$

Damage Ratio $DR = \frac{m(P^*) - m(P_i)}{m(P^*) - m(P_i) - 0.87 mS}$

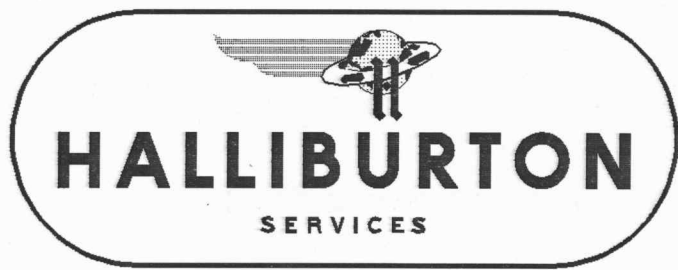
Indicated Flow Rate (Maximum) $AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_i)}$ MCFD

Indicated Flow Rate (Minimum) $AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_i)}}$ MCFD

Approx. Radius of Investigation $r_i = 0.032 \sqrt{\frac{k (t/60)}{\phi \mu c_i}}$ ft

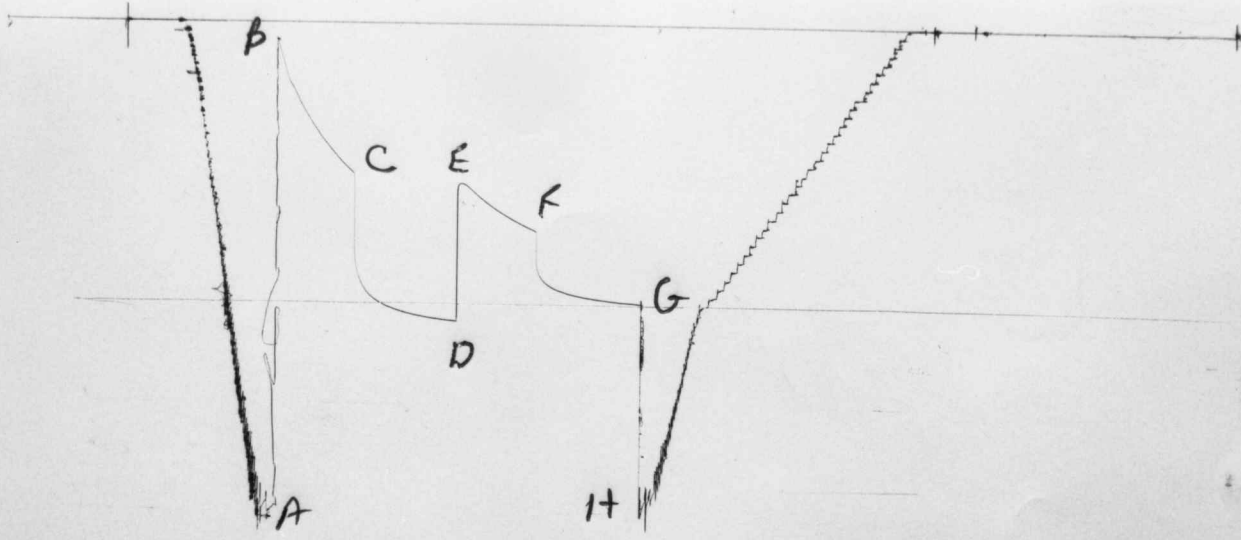
JOHNSON "B"
LEASE NAME
WELL NO. 1
TEST NO. 3
3487.0 - 3515.0
TESTED INTERVAL
WELL FILE
LEASE OWNER/COMPANY NAME
PETROLEUM INCORPORATED

LEGAL LOCATION
SEC. - TWP. - RNG. 33-6-21
FIELD AREA
COUNTY GRAHAM
STATE KANSAS OR



TICKET NO. 41953400
07-OCT-86
HAYS

FORMATION TESTING SERVICE REPORT

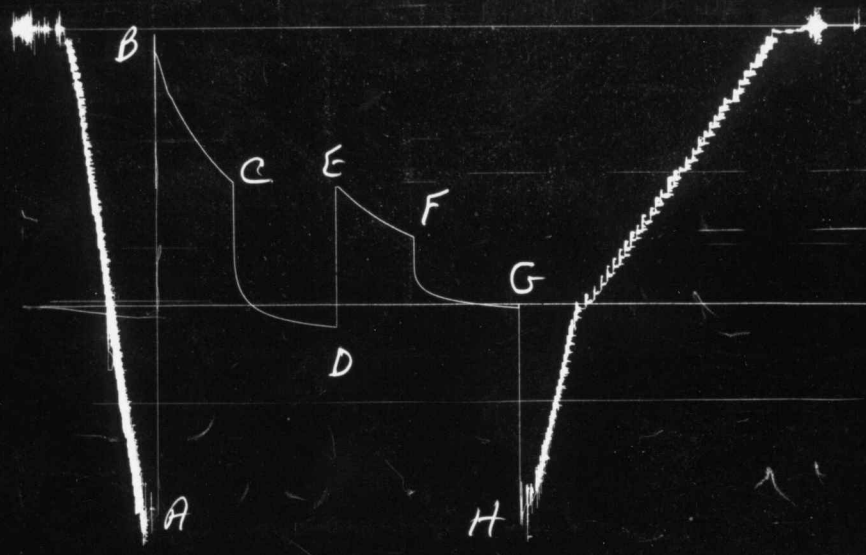


419534-7342

BT 7342
TKT# 419534

GAUGE NO: 7342 DEPTH: 3474.0 BLANKED OFF: NO HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		1713.5			
B	INITIAL FIRST FLOW		60.2			
C	FINAL FIRST FLOW		535.0	44.0	44.5	F
C	INITIAL FIRST CLOSED-IN		535.0			
D	FINAL FIRST CLOSED-IN		1057.8	60.0	59.0	C
E	INITIAL SECOND FLOW		567.2			
F	FINAL SECOND FLOW		734.4	45.0	45.0	F
F	INITIAL SECOND CLOSED-IN		734.4			
G	FINAL SECOND CLOSED-IN		991.2	60.0	60.4	C
H	FINAL HYDROSTATIC		1699.7			



419534-7341

BT. 7341
TKT# 419534

GAUGE NO: 7341 DEPTH: 3512.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	1714	1729.7			
B	INITIAL FIRST FLOW	75	86.3			
C	FINAL FIRST FLOW	561	556.2	44.0	44.5	F
C	INITIAL FIRST CLOSED-IN	561	556.2			
D	FINAL FIRST CLOSED-IN	1081	1076.7	60.0	59.0	C
E	INITIAL SECOND FLOW	561	573.8			
F	FINAL SECOND FLOW	747	754.8	45.0	45.0	F
F	INITIAL SECOND CLOSED-IN	747	754.8			
G	FINAL SECOND CLOSED-IN	1006	1010.6	60.0	60.4	C
H	FINAL HYDROSTATIC	1714	1714.9			

EQUIPMENT & HOLE DATA

FORMATION TESTED: KANSAS CITY "A"
 NET PAY (ft): 3.0
 GROSS TESTED FOOTAGE: 28.0
 ALL DEPTHS MEASURED FROM: KELLY BUSHING
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.875
 ELEVATION (ft): 2235.0
 TOTAL DEPTH (ft): 3515.0
 PACKER DEPTH(S) (ft): 3481, 3487
 FINAL SURFACE CHOKE (in): _____
 BOTTOM HOLE CHOKE (in): 0.750
 MUD WEIGHT (lb/gal): 9.50
 MUD VISCOSITY (sec): 43
 ESTIMATED HOLE TEMP. (°F): _____
 ACTUAL HOLE TEMP. (°F): 96 @ 3510.0 ft

TICKET NUMBER: 41953400

DATE: 10-1-86 TEST NO: 3

TYPE DST: OPEN HOLE

HALLIBURTON CAMP: _____
 HAYS _____

TESTER: MEL CHILDERS

WITNESS: TIM PRIEST

DRILLING CONTRACTOR: _____
 ABERCROMBIE #4 _____

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

SAMPLER DATA

Psig AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): 37.4 @ 60°F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____

RECOVERED:

1921' OF CLEAN GASSY OIL
 125' OF MUD CUT OIL (35% MUD)

MEASURED FROM
 TESTER VALVE

REMARKS:

TICKET NO: 41953400
 CLOCK NO: 4205 HOUR: 12



GAUGE NO: 7342
 DEPTH: 3474.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	60.2			
2	3.0	124.0	63.7		
3	6.0	190.2	66.2		
4	9.0	230.0	39.8		
5	12.0	268.7	38.7		
6	15.0	304.6	35.9		
7	18.0	336.0	31.4		
8	21.0	365.9	29.9		
9	24.0	392.1	26.2		
10	27.0	418.3	26.3		
11	30.0	440.9	22.6		
12	33.0	463.7	22.7		
13	36.0	485.1	21.4		
14	39.0	503.5	18.4		
15	42.0	520.9	17.4		
C 16	44.5	535.0	14.1		
FIRST CLOSED-IN					
C 1	0.0	535.0			
2	1.0	864.6	329.6	1.0	1.656
3	2.0	892.1	357.1	1.9	1.371
4	3.0	910.9	375.9	2.8	1.198
5	4.0	925.6	390.6	3.7	1.082
6	5.0	936.8	401.8	4.5	0.993
7	6.0	946.5	411.5	5.3	0.927
8	7.0	955.1	420.1	6.0	0.869
9	8.0	962.6	427.6	6.8	0.818
10	9.0	969.5	434.5	7.5	0.775
11	10.0	974.8	439.8	8.2	0.737
12	12.0	984.4	449.4	9.5	0.672
13	14.0	992.8	457.8	10.7	0.620
14	16.0	999.8	464.8	11.8	0.578
15	18.0	1006.5	471.5	12.8	0.540
16	20.0	1011.3	476.3	13.8	0.508
17	22.0	1016.0	481.0	14.7	0.480
18	24.0	1020.7	485.7	15.6	0.456
19	26.0	1025.2	490.2	16.4	0.433
20	28.0	1027.6	492.6	17.2	0.414
21	30.0	1031.4	496.4	17.9	0.395
22	35.0	1038.1	503.1	19.6	0.356
23	40.0	1043.8	508.8	21.1	0.325
24	45.0	1048.8	513.8	22.4	0.299
25	50.0	1052.6	517.6	23.6	0.277
26	55.0	1056.3	521.3	24.6	0.258
D 27	59.0	1057.8	522.8	25.4	0.244
SECOND FLOW					
E 1	0.0	567.2			

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
2	3.0	568.6	1.4		
3	6.0	578.2	9.6		
4	9.0	593.8	15.7		
5	12.0	611.1	17.3		
6	15.0	626.2	15.0		
7	18.0	640.3	14.1		
8	21.0	654.5	14.2		
9	24.0	666.9	12.4		
10	27.0	679.0	12.1		
11	30.0	689.3	10.3		
12	33.0	699.5	10.1		
13	36.0	709.2	9.8		
14	39.0	719.0	9.8		
15	42.0	727.4	8.5		
F 16	45.0	734.4	7.0		
SECOND CLOSED-IN					
F 1	0.0	734.4			
2	1.0	877.0	142.6	1.0	1.967
3	2.0	893.6	159.2	2.0	1.655
4	3.0	903.2	168.9	2.9	1.487
5	4.0	911.2	176.8	3.8	1.371
6	5.0	917.8	183.4	4.8	1.274
7	6.0	922.5	188.1	5.6	1.203
8	7.0	927.5	193.1	6.5	1.139
9	8.0	931.4	197.0	7.3	1.086
10	9.0	934.5	200.2	8.1	1.042
11	10.0	938.3	203.9	9.0	0.999
12	12.0	943.5	209.1	10.6	0.928
13	14.0	947.5	213.2	12.1	0.870
14	16.0	951.7	217.3	13.5	0.821
15	18.0	956.4	222.0	15.0	0.777
16	20.0	959.0	224.6	16.3	0.739
17	22.0	961.1	226.7	17.6	0.706
18	24.0	964.1	229.7	18.9	0.675
19	26.0	966.6	232.2	20.1	0.648
20	28.0	968.6	234.2	21.3	0.623
21	30.0	971.1	236.8	22.5	0.601
22	35.0	975.8	241.4	25.2	0.551
23	40.0	979.5	245.1	27.6	0.511
24	45.0	982.9	248.6	30.0	0.476
25	50.0	986.8	252.5	32.1	0.446
26	55.0	988.1	253.8	34.1	0.420
G 27	60.4	991.2	256.8	36.1	0.395

REMARKS:

TICKET NO: 41953400

CLOCK NO: 3930 HOUR: 12



GAUGE NO: 7341














DEPTH: 3512.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	86.3			
2	3.0	133.8	47.6		
3	6.0	200.4	66.6		
4	9.0	246.7	46.3		
5	12.0	284.6	37.9		
6	15.1	320.2	35.6		
7	18.0	352.0	31.7		
8	21.0	382.0	30.1		
9	24.0	409.6	27.6		
10	27.0	435.5	25.8		
11	30.0	459.5	24.0		
12	33.0	483.2	23.7		
13	36.0	503.7	20.6		
14	39.0	517.2	13.5		
15	42.0	535.3	18.1		
C 16	44.5	556.2	21.0		
FIRST CLOSED-IN					
C 1	0.0	556.2			
2	1.0	887.8	331.5	1.0	1.643
3	2.0	915.9	359.6	1.9	1.367
4	3.0	934.0	377.7	2.8	1.203
5	4.0	948.7	392.5	3.7	1.086
6	5.0	959.2	403.0	4.5	0.999
7	6.0	969.4	413.2	5.3	0.925
8	7.0	976.9	420.7	6.1	0.865
9	8.0	983.4	427.2	6.8	0.819
10	9.0	989.5	433.3	7.5	0.774
11	10.0	995.9	439.6	8.2	0.736
12	12.0	1005.4	449.2	9.5	0.673
13	14.0	1014.0	457.7	10.7	0.621
14	16.0	1020.1	463.9	11.8	0.578
15	18.0	1025.7	469.4	12.8	0.541
16	20.0	1030.6	474.4	13.8	0.509
17	22.0	1035.4	479.1	14.7	0.481
18	24.0	1039.8	483.6	15.6	0.455
19	26.0	1043.7	487.5	16.4	0.434
20	28.0	1046.7	490.4	17.2	0.414
21	30.0	1050.0	493.7	17.9	0.396
22	35.0	1056.5	500.2	19.6	0.357
23	40.0	1061.9	505.7	21.1	0.325
24	45.0	1066.6	510.3	22.4	0.299
25	50.0	1070.6	514.3	23.6	0.277
26	55.0	1074.1	517.9	24.6	0.258
D 27	59.0	1076.7	520.5	25.4	0.244
SECOND FLOW					
E 1	0.0	573.8			

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND FLOW - CONTINUED					
2	3.0	580.3	6.5		
3	6.0	597.9	17.6		
4	9.0	616.0	18.1		
5	12.0	631.5	15.5		
6	15.0	646.7	15.1		
7	18.0	660.8	14.1		
8	21.0	673.8	13.0		
9	24.0	686.2	12.4		
10	27.0	697.9	11.6		
11	30.0	708.9	11.1		
12	33.0	719.2	10.3		
13	36.0	729.0	9.8		
14	39.0	738.5	9.6		
15	42.0	747.3	8.7		
F 16	45.0	754.8	7.5		
SECOND CLOSED-IN					
F 1	0.0	754.8			
2	1.0	900.4	145.6	1.0	1.967
3	2.0	916.0	161.2	2.0	1.651
4	3.0	924.8	170.0	2.9	1.490
5	4.0	933.3	178.5	3.8	1.368
6	5.0	939.7	184.9	4.8	1.275
7	6.0	943.6	188.8	5.6	1.205
8	7.0	948.8	194.0	6.5	1.138
9	8.0	952.2	197.4	7.3	1.088
10	9.0	955.5	200.7	8.2	1.039
11	10.0	959.0	204.2	9.0	0.999
12	12.0	964.3	209.5	10.6	0.929
13	14.0	968.5	213.7	12.1	0.870
14	16.0	972.1	217.3	13.6	0.818
15	18.0	976.0	221.2	15.0	0.776
16	20.0	978.6	223.8	16.3	0.739
17	22.0	981.4	226.6	17.7	0.705
18	24.0	984.0	229.2	19.0	0.675
19	26.0	986.5	231.7	20.2	0.648
20	28.0	988.5	233.7	21.3	0.623
21	30.0	990.7	235.9	22.5	0.601
22	35.0	994.6	239.9	25.1	0.552
23	40.0	999.3	244.5	27.7	0.510
24	45.0	1002.3	247.5	30.0	0.476
25	50.0	1005.3	250.5	32.1	0.446
26	55.0	1008.0	253.2	34.1	0.420
G 27	60.4	1010.6	255.8	36.1	0.395

REMARKS:

TICKET NO. 41953400

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	2860.5	
4		FLEX WEIGHT.....	4.500	2.950	346.7	
50		IMPACT REVERSING SUB.....	5.750	2.750	1.0	3208.0
4		FLEX WEIGHT.....	4.500	2.950	252.9	
5		CROSSOVER.....	5.000	2.950	1.0	
12		DUAL CIP VALVE.....	5.000	0.870	6.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	3472.0
80		AP RUNNING CASE.....	5.000	2.250	4.1	3474.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3481.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3487.0
20		FLUSH JOINT ANCHOR.....	5.000	2.370	20.4	
83		HT-500 TEMPERATURE CASE.....	5.000		1.5	3510.0
81		BLANKED-OFF RUNNING CASE.....	5.000		4.3	3512.0
TOTAL DEPTH					3515.0	

EQUIPMENT DATA

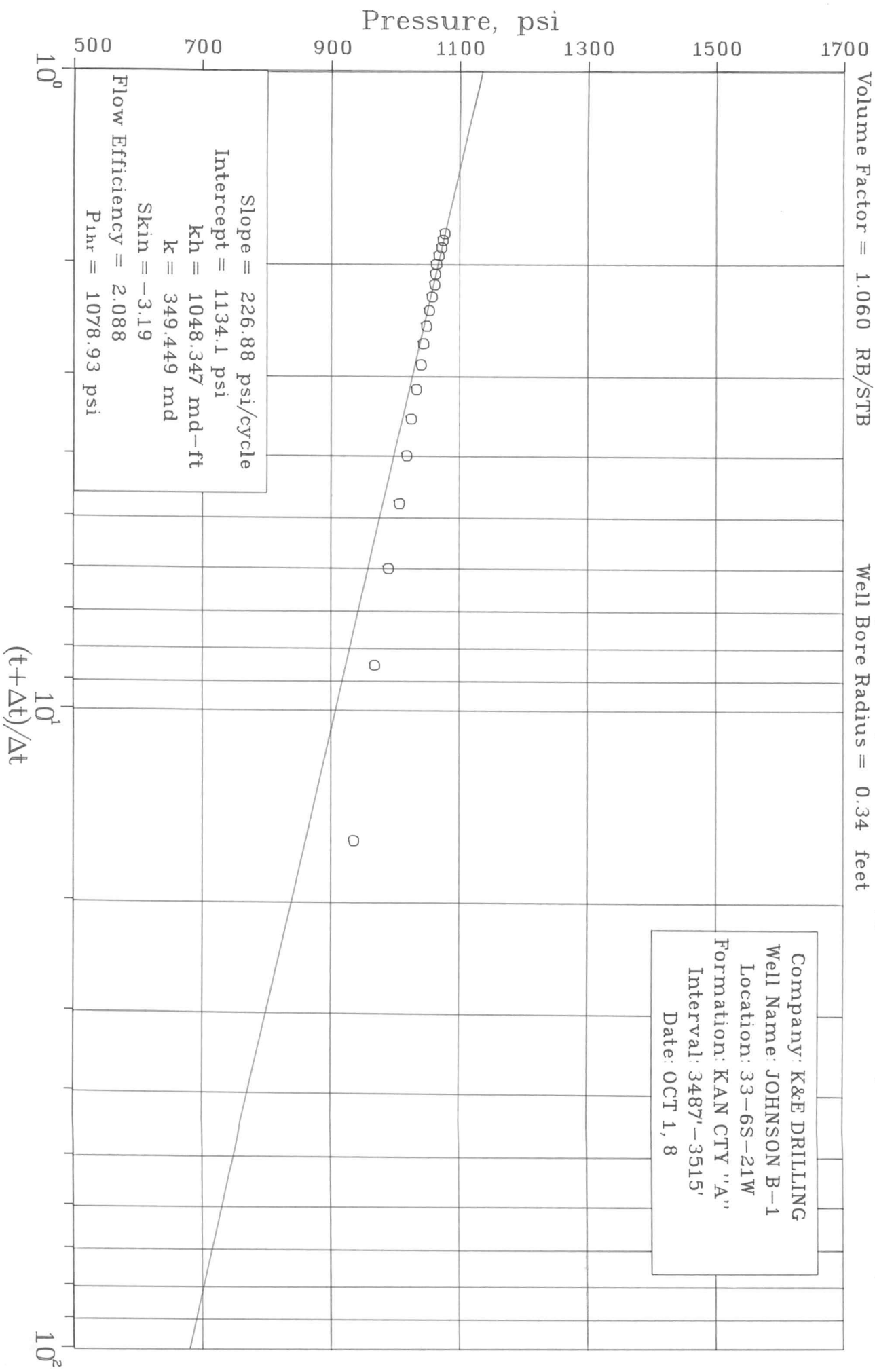
INITIAL

End Points = 1.789 1.882
Oil Flow Rate = 345.000 BOPD
Volume Factor = 1.060 RB/STB

Viscosity = 4.000 cp
Compressibility = 2.50×10^{-5} 1/psi
Well Bore Radius = 0.34 feet

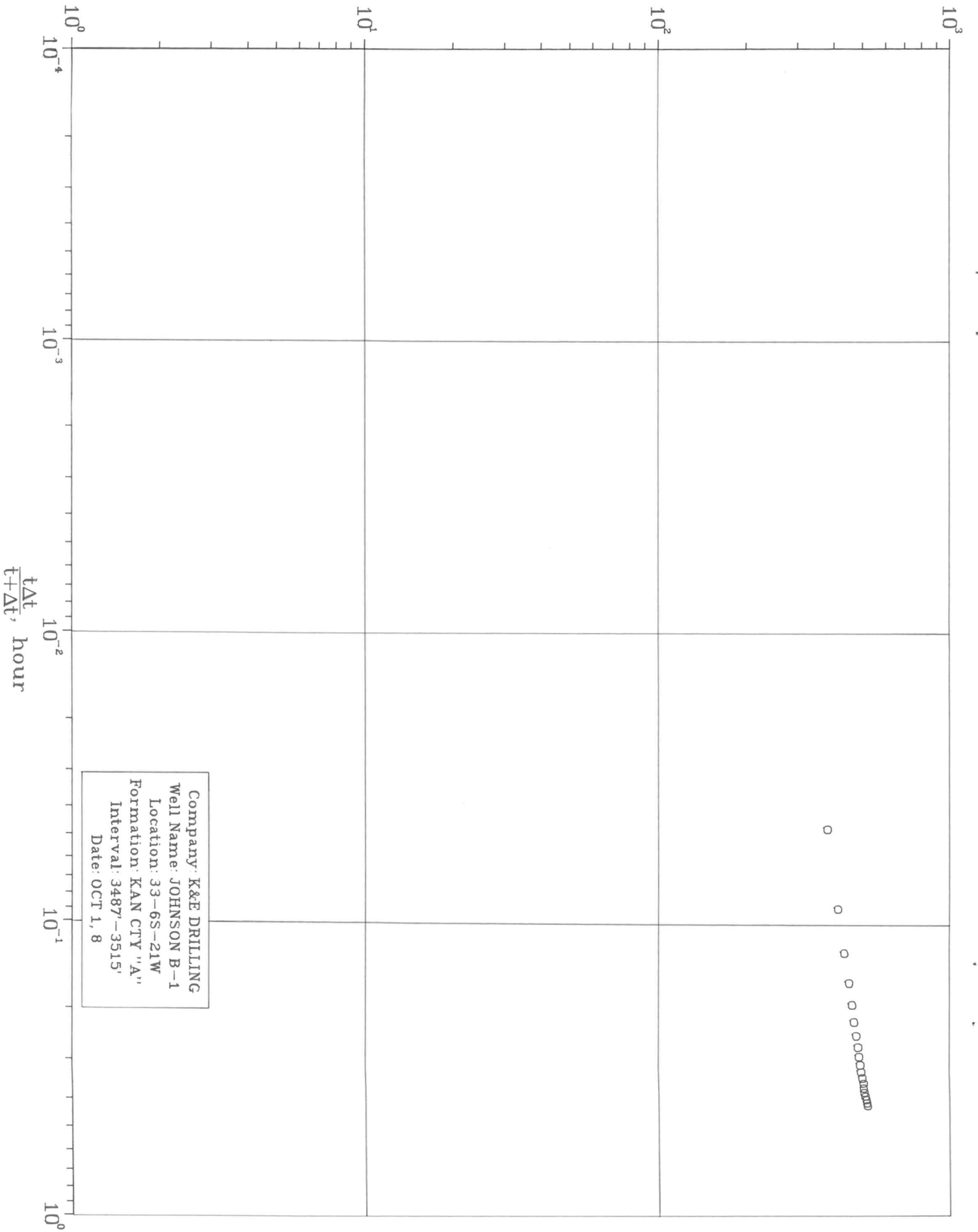
Porosity = 0.15
Net Pay = 3. feet

Company: K&E DRILLING
Well Name: JOHNSON B-1
Location: 33-6S-21W
Formation: KAN CTY "A"
Interval: 3487'-3515'
Date: OCT 1, 8



Slope = 226.88 psi/cycle
 Intercept = 1134.1 psi
 $kh = 1048.347$ md-ft
 $k = 349.449$ md
 Skin = -3.19
 Flow Efficiency = 2.088
 $P_{1hr} = 1078.93$ psi

Δp , psi



Company: K&E DRILLING
Well Name: JOHNSON B-1
Location: 33-6S-21W
Formation: KAN CTY "A"
Interval: 3487'-3515'
Date: OCT 1, 8

PANL

10/02/86

WELL IDENTIFICATION

K&E DRILLING

JOHNSON B-1

33-6S-21W

KAN CTY "A"

3487'-3515'

OCT 1, 8

1 CIP

TEST INFORMATION

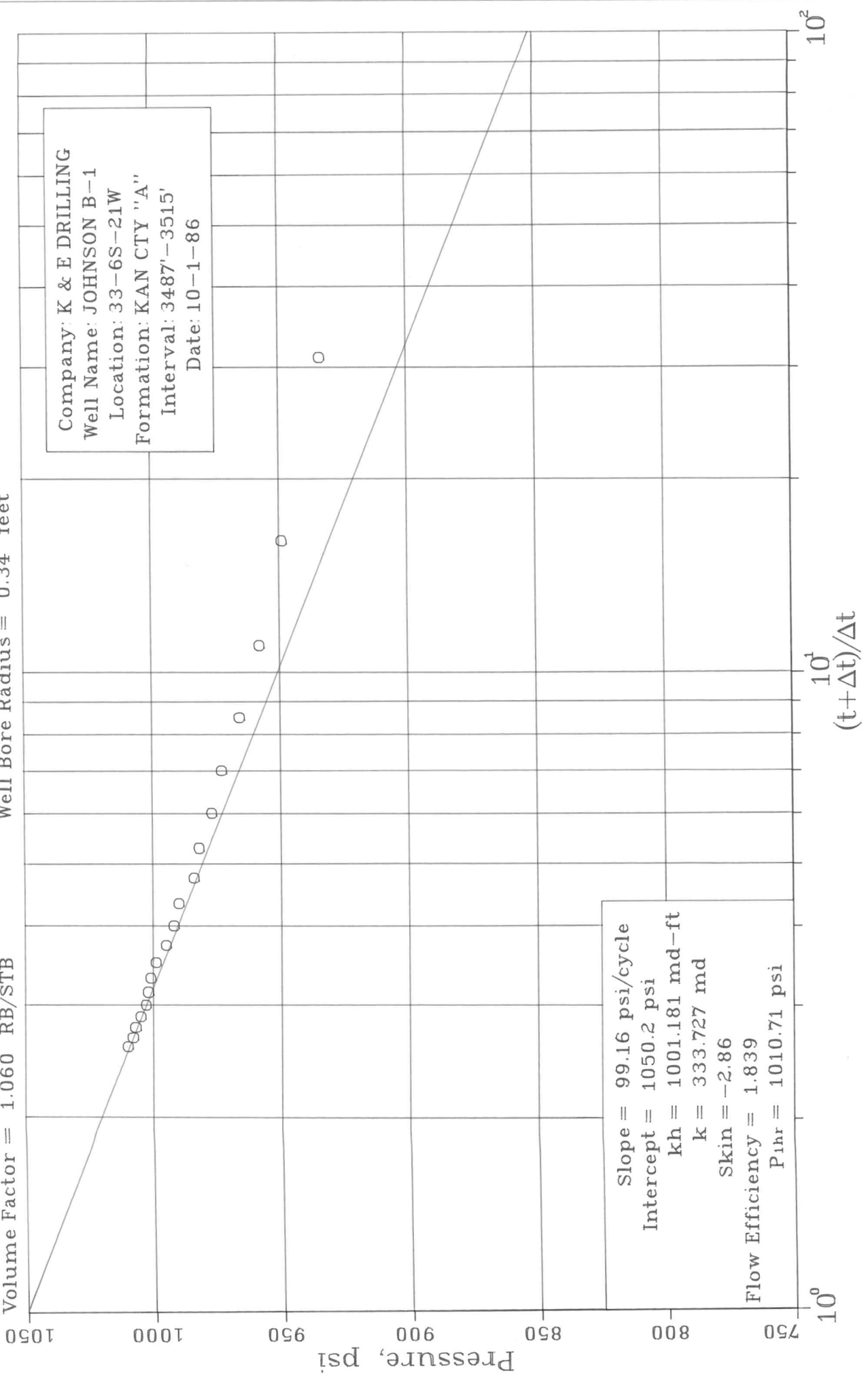
TEST TYPE BUILD UP
 WELL TYPE OIL
 FLOW TIME 0.8 HOURS

DT (HOUR)	SQRT DT	(T+DT)/DT	P (PSI)	DP (PSI)
0.002	0.041	451.000	556.00	0.0
0.050	0.224	16.000	936.00	380.00
0.100	0.316	8.500	969.00	413.00
0.150	0.387	6.000	990.00	434.00
0.200	0.447	4.750	1007.00	451.00
0.250	0.500	4.000	1018.00	462.00
0.300	0.548	3.500	1025.00	469.00
0.350	0.592	3.143	1033.00	477.00
0.400	0.632	2.875	1040.00	484.00
0.450	0.671	2.667	1044.00	488.00
0.500	0.707	2.500	1049.00	493.00
0.550	0.742	2.364	1053.00	497.00
0.600	0.775	2.250	1057.00	501.00
0.650	0.806	2.154	1061.00	505.00
0.700	0.837	2.071	1062.00	506.00
0.750	0.866	2.000	1064.00	508.00
0.800	0.894	1.937	1068.00	512.00
0.850	0.922	1.882 -	1072.00	516.00
0.900	0.949	1.833	1074.00	518.00
0.950	0.975	1.789 -	1077.00	521.00

FINAC

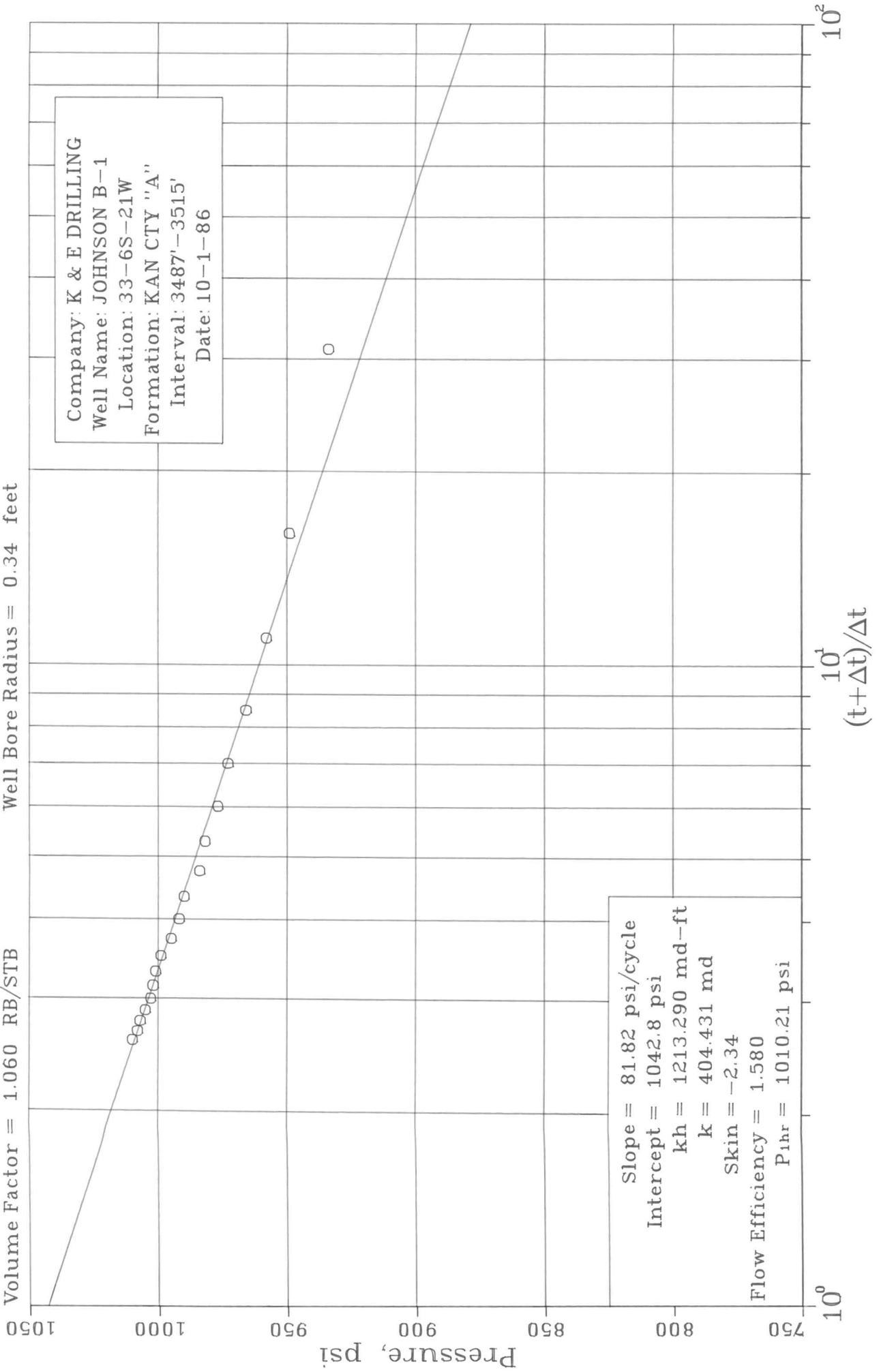
End Points = 2.579 2.765
 Oil Flow Rate = 144.000 BOPD
 Volume Factor = 1.060 RB/STB
 Viscosity = 4.000 cp
 Compressibility = 2.50×10^{-5} 1/psi
 Well Bore Radius = 0.34 feet
 Porosity = 0.15
 Net Pay = 3. feet

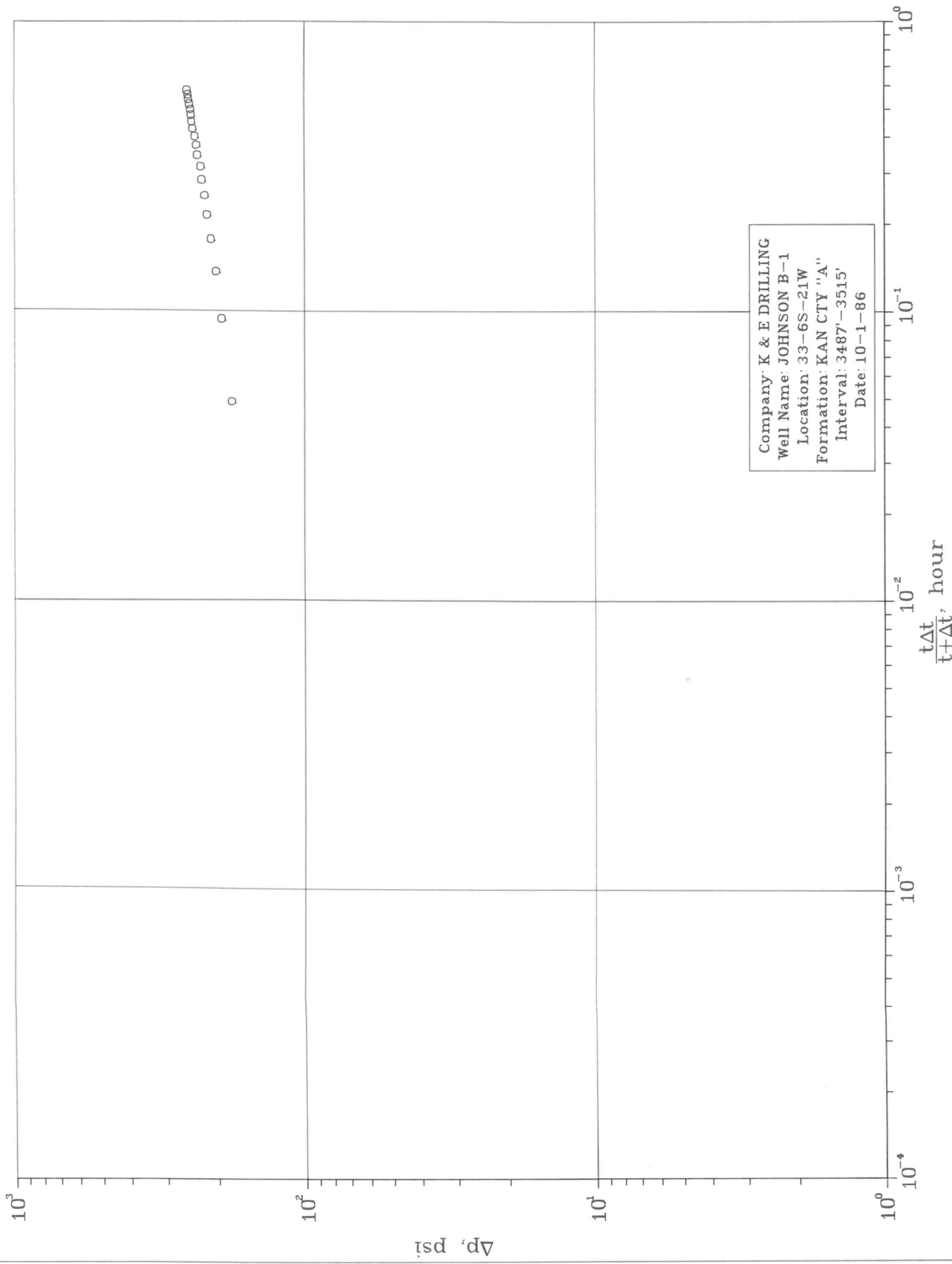
Company: K & E DRILLING
 Well Name: JOHNSON B-1
 Location: 33-6S-21W
 Formation: KAN CTY "A"
 Interval: 3487'-3515'
 Date: 10-1-86



End Points = 3.000 3.727 Porosity = 0.15
 Oil Flow Rate = 144.000 BOPD Net Pay = 3. feet
 Volume Factor = 1.060 RB/STB Compressibility = 2.50×10^{-5} 1/psi
 Viscosity = 4.000 cp Well Bore Radius = 0.34 feet

Company: K & E DRILLING
 Well Name: JOHNSON B-1
 Location: 33-6S-21W
 Formation: KAN CTY "A"
 Interval: 3487'-3515'
 Date: 10-1-86





10³

10²

10¹

10⁰

Δp, psi

10⁻⁴

10⁻³

10⁻²

10⁻¹

10⁰

$\frac{t\Delta t}{t+\Delta t}$, hour

PANL

10/02/86

WELL IDENTIFICATION

K & E DRILLING

JOHNSON B-1

33-6S-21W

KAN CTY "A"

3487'-3515'

10-1-86

2-CIP

TEST INFORMATION

TEST TYPE BUILD UP
 WELL TYPE OIL
 FLOW TIME 1.5 HOURS

DT (HOUR)	SQRT DT	(T+DT)/DT	P (PSI)	DP (PSI)
0.002	0.041	900.999	756.00	0.0
0.050	0.224	31.000	934.00	178.00
0.100	0.316	16.000	949.00	193.00
0.150	0.387	11.000	958.00	202.00
0.200	0.447	8.500	966.00	210.00
0.250	0.500	7.000	973.00	217.00
0.300	0.548	6.000	977.00	221.00
0.350	0.592	5.286	982.00	226.00
0.400	0.632	4.750	984.00	228.00
0.450	0.671	4.333	990.00	234.00
0.500	0.707	4.000	992.00	236.00
0.550	0.742	3.727	995.00	239.00
0.600	0.775	3.500	999.00	243.00
0.650	0.806	3.308	1001.00	245.00
0.700	0.837	3.143	1002.00	246.00
0.750	0.866	3.000	1003.00	247.00
0.800	0.894	2.875	1005.00	249.00
0.850	0.922	2.765	1007.00	251.00
0.900	0.949	2.667	1008.00	252.00
0.950	0.975	2.579	1010.00	254.00

TEMPERATURE

RECORDER

CHART



10° each circle

EQUATIONS FOR DST GAS WELL ANALYSIS

Indicated Flow Capacity

$$kh = \frac{.001637 Q_g T}{m}$$

md-ft

Average Effective Permeability

$$k = \frac{kh}{h}$$

md

Skin Factor

$$S = 1.151 \left[\frac{m(P^*) - m(P_i)}{m} - \text{LOG} \left(\frac{k(t/60)}{\phi \mu c_i r_w^2} \right) + 3.23 \right]$$

Damage Ratio

$$DR = \frac{m(P^*) - m(P_i)}{m(P^*) - m(P_i) - 0.87 mS}$$

Indicated Flow Rate (Maximum)

$$AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_i)}$$

MCFD

Indicated Flow Rate (Minimum)

$$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_i)}}$$

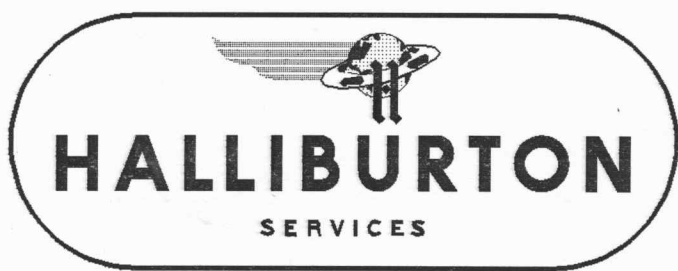
MCFD

Approx. Radius of Investigation

$$r_i = 0.032 \sqrt{\frac{k(t/60)}{\phi \mu c_i}}$$

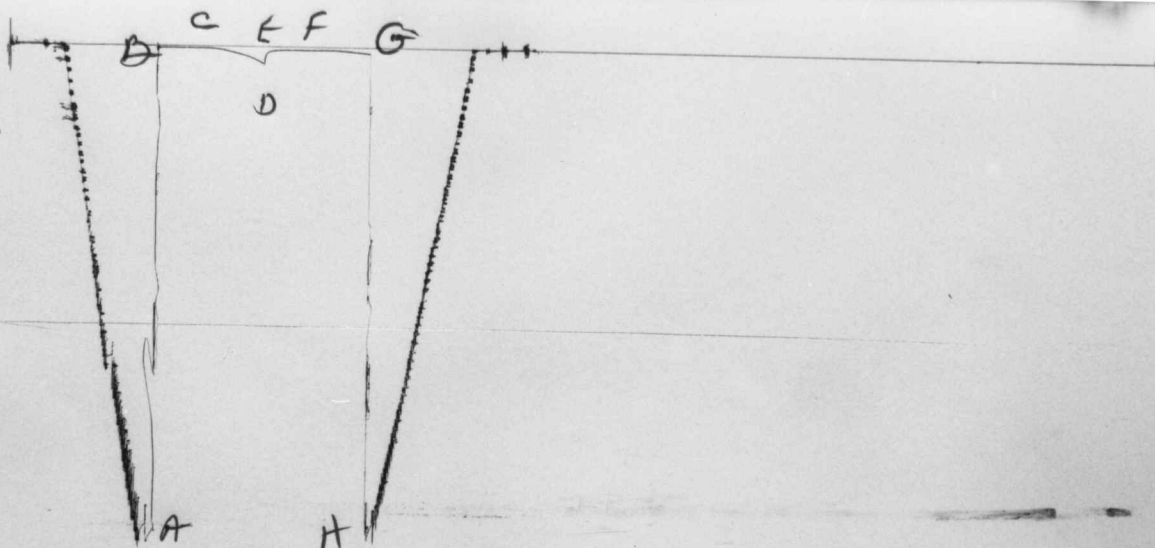
ft

JOHNSON "B"
 LEASE NAME
 WELL NO. 1
 TEST NO. 4
 LEGAL LOCATION
 SEC. - TWP. - RNG. 33-6-21
 FIELD AREA
 COUNTY GRAHAM
 STATE KANSAS
 DR
 LEASE OWNER/COMPANY NAME
 3514.0 - 3540.0
 TESTED INTERVAL
 WELLS & PETROLEUM INCORPORATED



TICKET NO. 41953500
 06-OCT-86
 HAYS

FORMATION TESTING SERVICE REPORT

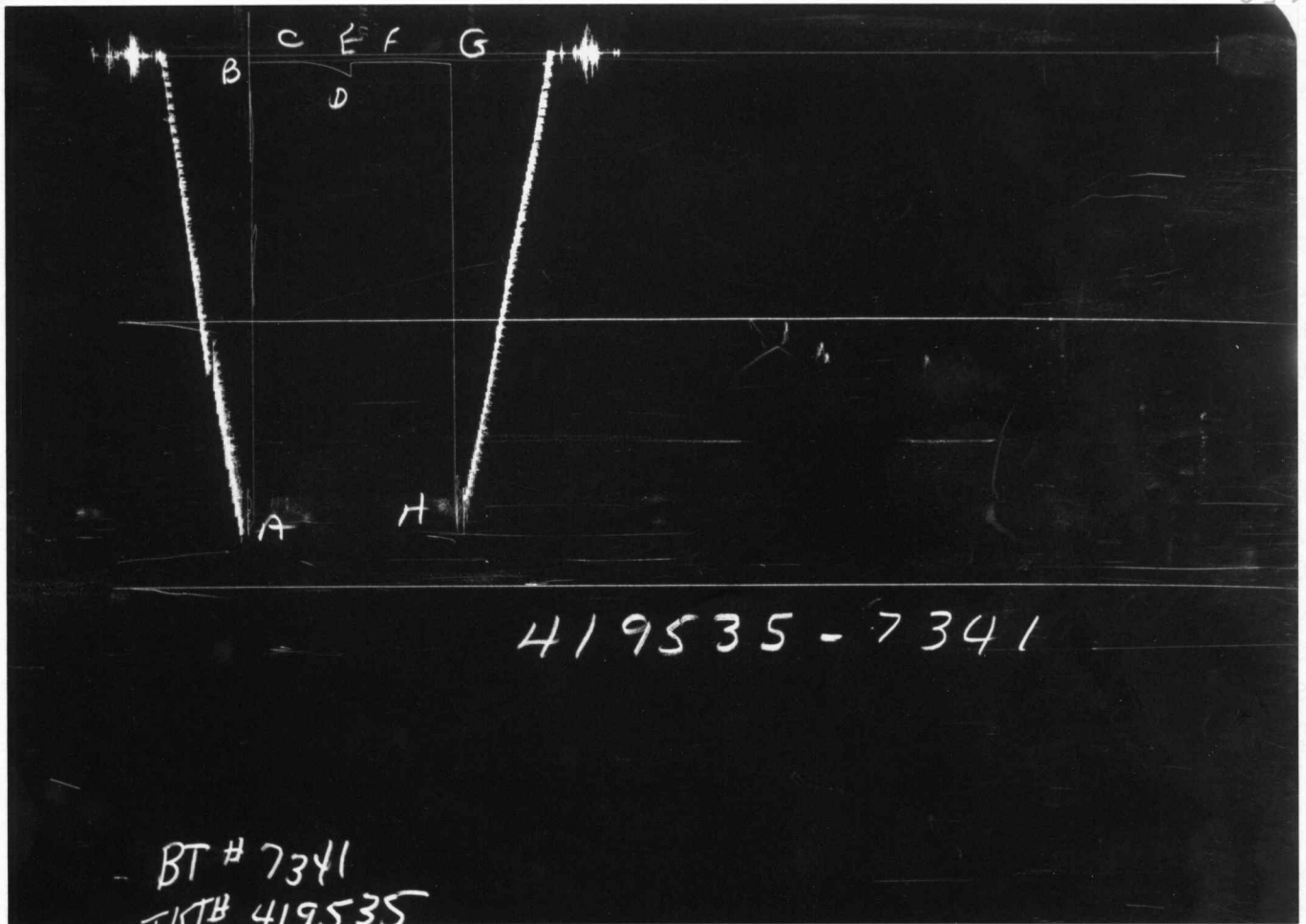


419535-7342

BT# 7342
TKT# 419535

GAUGE NO: 7342 DEPTH: 3501.0 BLANKED OFF: NO HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		1736.5			
B	INITIAL FIRST FLOW		7.8			
C	FINAL FIRST FLOW		7.8	30.0	30.0	F
C	INITIAL FIRST CLOSED-IN		7.8			
D	FINAL FIRST CLOSED-IN		61.3	30.0	30.0	C
E	INITIAL SECOND FLOW		47.7			
F	FINAL SECOND FLOW		12.0	30.0	30.0	F
F	INITIAL SECOND CLOSED-IN		12.0			
G	FINAL SECOND CLOSED-IN		20.6	30.0	30.0	C
H	FINAL HYDROSTATIC		1705.1			



GAUGE NO: 7341 DEPTH: 3537.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	1751	1750.9			
B	INITIAL FIRST FLOW	19	24.6	30.0	30.0	F
C	FINAL FIRST FLOW	19	24.6			
C	INITIAL FIRST CLOSED-IN	19	24.6	30.0	30.0	C
D	FINAL FIRST CLOSED-IN	75	81.3			
E	INITIAL SECOND FLOW	19	36.5	30.0	30.0	F
F	FINAL SECOND FLOW	19	27.4			
F	INITIAL SECOND CLOSED-IN	19	27.4	30.0	30.0	C
G	FINAL SECOND CLOSED-IN	37	36.7			
H	FINAL HYDROSTATIC	1733	1715.2			

EQUIPMENT & HOLE DATA

FORMATION TESTED: _____
 NET PAY (ft): 3.0
 GROSS TESTED FOOTAGE: 26.0
 ALL DEPTHS MEASURED FROM: KELLY BUSHING
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.875
 ELEVATION (ft): 2235.0
 TOTAL DEPTH (ft): 3540.0
 PACKER DEPTH(S) (ft): 3508, 3514
 FINAL SURFACE CHOKE (in): _____
 BOTTOM HOLE CHOKE (in): 0.750
 MUD WEIGHT (lb/gal): 9.30
 MUD VISCOSITY (sec): 46
 ESTIMATED HOLE TEMP. (°F): _____
 ACTUAL HOLE TEMP. (°F): 95 @ 3535.0 ft

TICKET NUMBER: 41953500
 DATE: 10-2-86 TEST NO: 4
 TYPE DST: OPEN HOLE
 HALLIBURTON CAMP: _____
HAYS
 TESTER: MEL CHILDERS
 WITNESS: TIM PRIEST
 DRILLING CONTRACTOR: _____
ABERCROMBIE #4

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

SAMPLER DATA

Pstg AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ @ _____ °F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____














RECOVERED:

10' OF MUD

MEASURED FROM TESTER VALVE

REMARKS:

TICKET NO. 41953500

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	2887.5	
4		FLEX WEIGHT.....	4.500	2.950	346.7	
50		IMPACT REVERSING SUB.....	5.750	2.750	1.0	3235.0
4		FLEX WEIGHT.....	4.500	2.950	252.9	
5		CROSSOVER.....	5.000	2.950	1.0	
12		DUAL CIP VALVE.....	5.000	0.870	6.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	3499.0
80		AP RUNNING CASE.....	5.000	2.250	4.1	3501.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3508.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3514.0
20		FLUSH JOINT ANCHOR.....	5.000	2.370	18.4	
83		HT-500 TEMPERATURE CASE.....	5.000		1.5	3535.0
81		BLANKED-OFF RUNNING CASE.....	5.000		4.3	3537.0
TOTAL DEPTH					3540.0	

EQUIPMENT DATA

TEMPERATURE

RECORDER

CHART



10° each circle

EQUATIONS FOR DST GAS WELL ANALYSIS

Indicated Flow Capacity

$$kh = \frac{.001637 Q_g T}{m}$$

md-ft

Average Effective Permeability

$$k = \frac{kh}{h}$$

md

Skin Factor

$$S = 1.151 \left[\frac{m(P^*) - m(P_i)}{m} - \text{LOG} \left(\frac{k(t/60)}{\phi \mu c_i r_w^2} \right) + 3.23 \right]$$

Damage Ratio

$$DR = \frac{m(P^*) - m(P_i)}{m(P^*) - m(P_i) - 0.87 mS}$$

Indicated Flow Rate (Maximum)

$$AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_i)}$$

MCFD

Indicated Flow Rate (Minimum)

$$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_i)}}$$

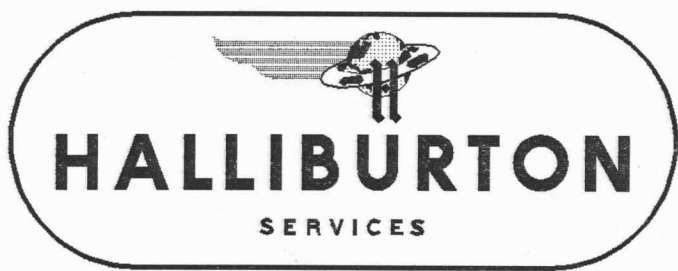
MCFD

Approx. Radius of Investigation

$$r_i = 0.032 \sqrt{\frac{k(t/60)}{\phi \mu c_i}}$$

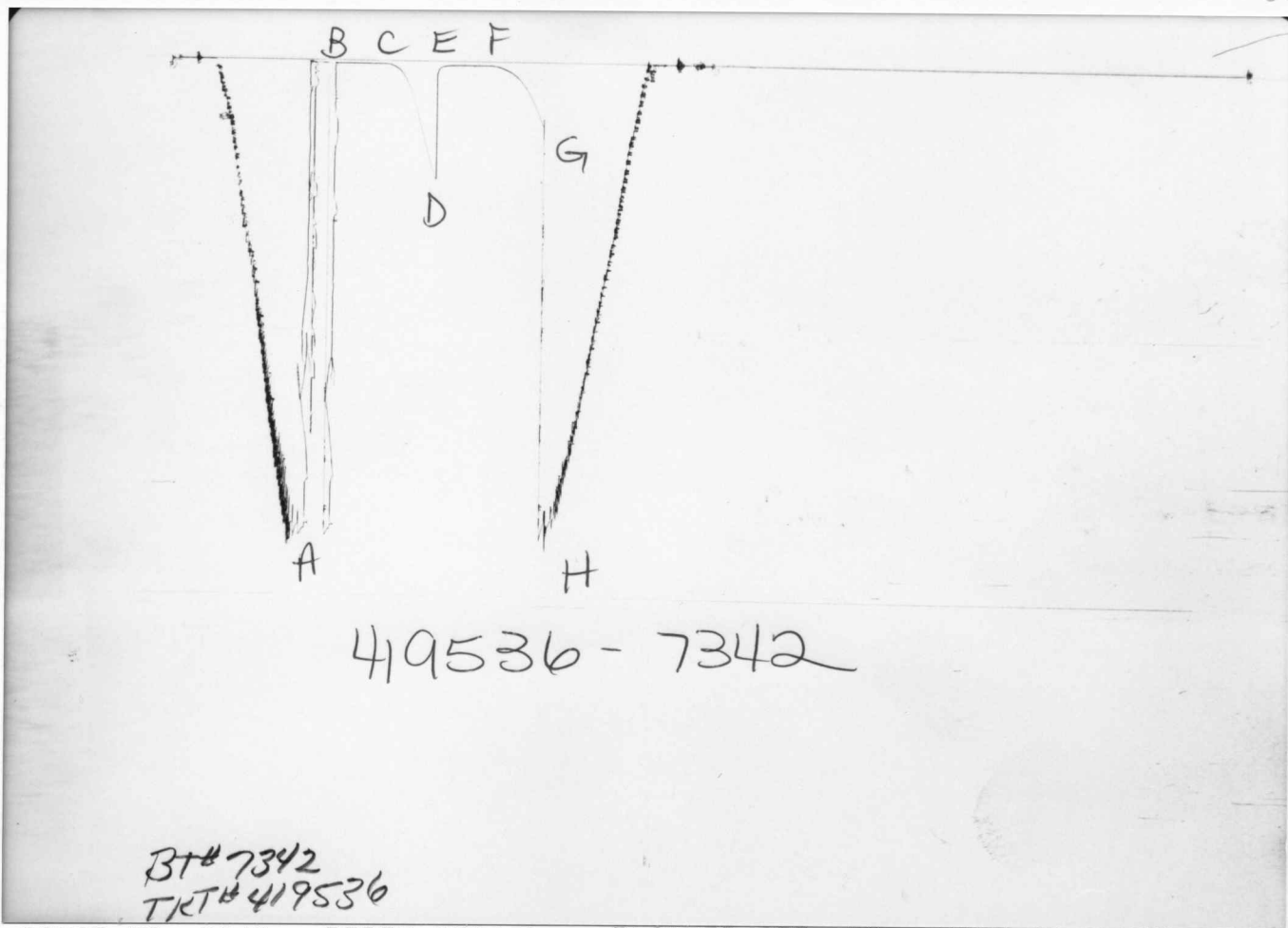
ft

JOHNSON "B"
 LEASE NAME
 WELL NO. 1
 TEST NO. 5
 LEGAL LOCATION 33 - 6 - 21
 SEC. - TWP. - RNG.
 FIELD AREA
 COUNTY GRAHAM
 STATE KANSAS
 PW
 3537.0 - 3565.0
 TESTED INTERVAL
 WELLS & PETROLEUM, INCORPORATED
 LEASE OWNER/COMPANY NAME



TICKET NO. 41953600
 06-OCT-86
 HAYS

FORMATION TESTING SERVICE REPORT

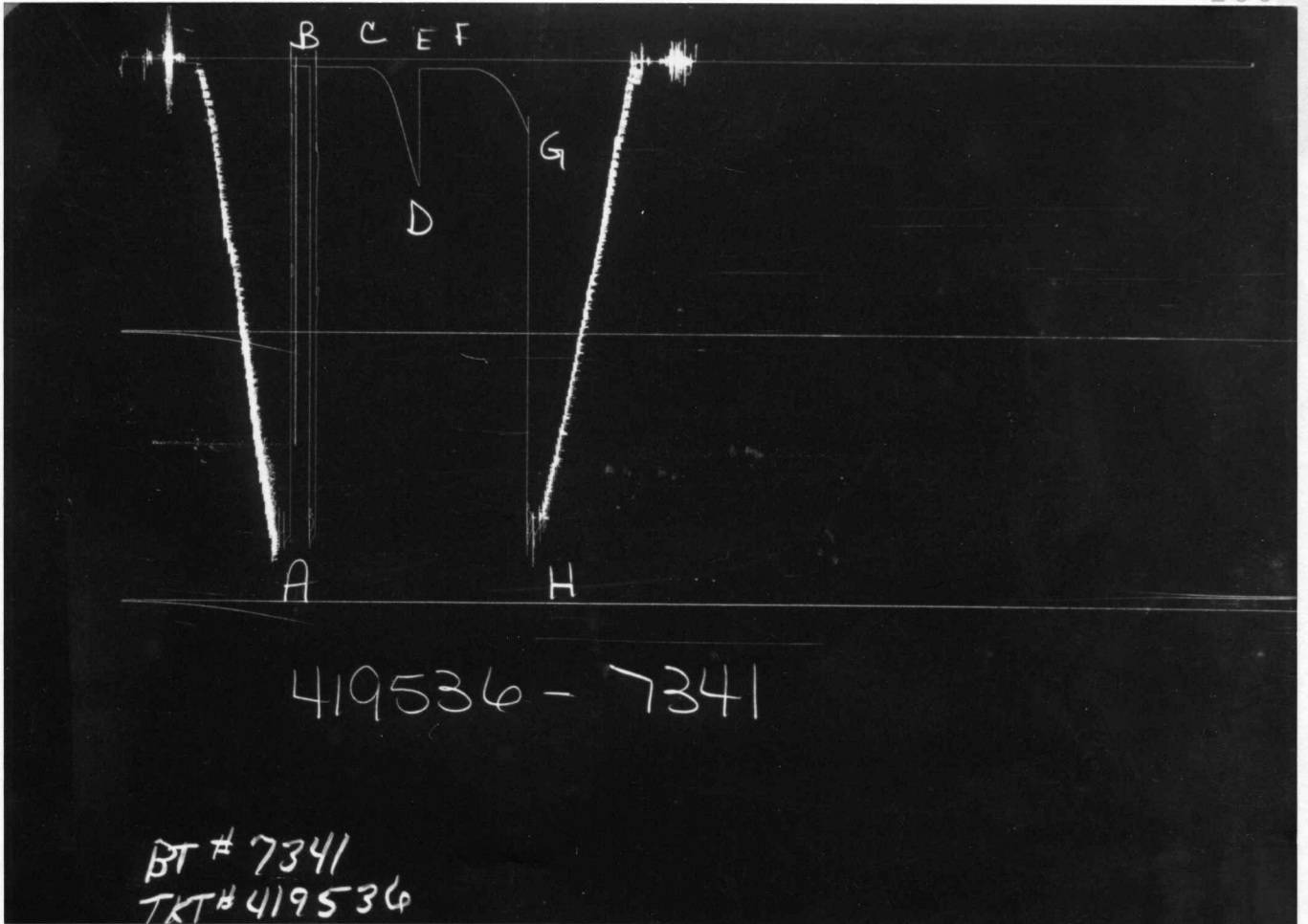


419536-7342

BT# 7342
TRT# 419536

GAUGE NO: 7342 DEPTH: 3524.0 BLANKED OFF: NO HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC		1748.1			
B	INITIAL FIRST FLOW		11.2			
C	FINAL FIRST FLOW		11.2	30.0	30.0	F
C	INITIAL FIRST CLOSED-IN		11.2			
D	FINAL FIRST CLOSED-IN		441.6	30.0	30.0	C
E	INITIAL SECOND FLOW		45.5			
F	FINAL SECOND FLOW		14.7	30.0	30.0	F
F	INITIAL SECOND CLOSED-IN		14.7			
G	FINAL SECOND CLOSED-IN		240.2	35.0	35.0	C
H	FINAL HYDROSTATIC		1720.1			



GAUGE NO: 7341 DEPTH: 3562.0 BLANKED OFF: YES HOUR OF CLOCK: 12

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	1770	1761.4			
B	INITIAL FIRST FLOW	19	27.0			
C	FINAL FIRST FLOW	19	30.3	30.0	30.0	F
C	INITIAL FIRST CLOSED-IN	19	30.3			
D	FINAL FIRST CLOSED-IN	468	466.6	30.0	30.0	C
E	INITIAL SECOND FLOW	19	37.0			
F	FINAL SECOND FLOW	19	34.2	30.0	30.0	F
F	INITIAL SECOND CLOSED-IN	19	34.2			
G	FINAL SECOND CLOSED-IN	262	267.4	35.0	35.0	C
H	FINAL HYDROSTATIC	1751	1729.9			

EQUIPMENT & HOLE DATA

FORMATION TESTED: KANSAS CITY
 NET PAY (ft): 6.0
 GROSS TESTED FOOTAGE: 28.0
 ALL DEPTHS MEASURED FROM: KB
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.875
 ELEVATION (ft): 2235.0
 TOTAL DEPTH (ft): 3565.0
 PACKER DEPTH(S) (ft): 3531, 3537
 FINAL SURFACE CHOKE (in): _____
 BOTTOM HOLE CHOKE (in): 0.750
 MUD WEIGHT (lb/gal): 9.30
 MUD VISCOSITY (sec): 46
 ESTIMATED HOLE TEMP. (°F): _____
 ACTUAL HOLE TEMP. (°F): 94 @ 3560.0 ft

TICKET NUMBER: 41953600
 DATE: 10-2-86 TEST NO: 5
 TYPE DST: OPEN HOLE
 HALLIBURTON CAMP: HAYS
 TESTER: MEL CHILDERS
 WITNESS: TIM PRIEST
 DRILLING CONTRACTOR: ABERCROMBIE #4

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

SAMPLER DATA

Pstg AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ @ _____ °F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____














RECOVERED:

10 FEET OF MUD

MEASURED FROM
TESTER VALVE

REMARKS:

TICKET NO. 41953600

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	4.500	3.826	2910.5	
4		FLEX WEIGHT.....	4.500	2.950	346.7	
50		IMPACT REVERSING SUB.....	5.750	2.750	1.0	3258.0
4		FLEX WEIGHT.....	4.500	2.950	252.9	
5		CROSSOVER.....	5.000	2.950	1.0	
12		DUAL CIP VALVE.....	5.000	0.870	6.0	
60		HYDROSPRING TESTER.....	5.000	0.750	5.0	3522.0
80		AP RUNNING CASE.....	5.000	2.250	4.1	3524.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3531.0
70		OPEN HOLE PACKER.....	6.750	1.530	5.8	3537.0
20		FLUSH JOINT ANCHOR.....	5.000	2.370	20.4	
83		HT-500 TEMPERATURE CASE.....	5.000		1.5	3560.0
81		BLANKED-OFF RUNNING CASE.....	5.000		4.3	3562.0
TOTAL DEPTH					3565.0	

EQUIPMENT DATA

TEMPERATURE

RECORDER

CHART



10° each circle

EQUATIONS FOR DST GAS WELL ANALYSIS

Indicated Flow Capacity $kh = \frac{.001637 Q_g T}{m}$ md-ft

Average Effective Permeability $k = \frac{kh}{h}$ md

Skin Factor $S = 1.151 \left[\frac{m(P^*) - m(P_i)}{m} - \text{LOG} \left(\frac{k (t/60)}{\phi \mu c_r w^2} \right) + 3.23 \right]$

Damage Ratio $DR = \frac{m(P^*) - m(P_i)}{m(P^*) - m(P_i) - 0.87 mS}$

Indicated Flow Rate (Maximum) $AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_i)}$ MCFD

Indicated Flow Rate (Minimum) $AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_i)}}$ MCFD

Approx. Radius of Investigation $r_i = 0.032 \sqrt{\frac{k (t/60)}{\phi \mu c_i}}$ ft