

STATE OF KANSAS -- CORPORATION COMMISSION  
ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST

FORM G-2  
8-7-53

1391

TYPE TEST:  Deliverability  Open Flow TEST DATE: 3/09/90 15-181-2028-00-00

COMPANY: GOODLAND GAS COMPANY LEASE: Armstrong WELLS NO.: 1-12A

COUNTY: Sherman LOCATION: SW 1/4, NW 1/4 SECTION: 12 TWP: 8S RNG: 40W ACRES:

FIELD: Goodland RESERVOIR: Niobrara PIPELINE CONNECTION: KNEnergy

COMPLETION DATE: 11-16-83 PLUG BACK TOTAL DEPTH: 1231 PACKER SET AT: None

CASING SIZE: 4 1/2" WT: 9.5#/ft. I.D.: SET AT: 1301 PERM: 1163 TO: 1190

TUBING SIZE: None WT: I.D.: SET AT: PERM: TO:

TYPE COMPLETION (Describe): Frac 82.600# Sd., 631 Bbls H2O TYPE FLUID PRODUCTION: Gas

PRODUCING THRU: Casing RESERVOIR TEMPERATURE F: BAR. PRESS - P<sub>a</sub>: Psia

GAS GRAVITY - G<sub>c</sub>: 0.5920 % CARBON DIOXIDE: 1.98 % NITROGEN: 2.790 API GRAVITY OF LIQUID: --

VERTICAL DEPTH (H): TYPE METER CONN.: Orifice-Flange (METER RUN) (PROVER) SIZE: 2.067

SHUT-IN PRESSURE: SHUT IN 2/9 1990 AT 10:55 (AM)(PM) TAKEN 2/12 1990 AT 8:25 (AM)(PM) X  
FLOW TEST: STARTED 2/22 1990 AT 8:00 (AM)(PM) TAKEN 2/23 1990 AT 8:00 (AM)(PM) X

OBSERVED DATA DURATION OF SHUT-IN: 72 HR.

SHUT-IN OR FLOW	ORIFICE SIZE in.	(METER) (PROVER) PRESSURE psig	DIFF. In. (h <sub>w</sub> )	FLOWING TEMP. t	WELL-HEAD TEMP. t	CASING WELLHEAD PRESS		TUBING WELLHEAD PRESS		DURATION HOURS	LIQUID PROD. Bbls.
						psig	(P <sub>w</sub> )(P <sub>c</sub> )(P <sub>d</sub> ) psia	psig	(P <sub>w</sub> )(P <sub>c</sub> )(P <sub>d</sub> ) psia		
SHUT-IN	--	--	--	--	--	29	43.4	--	--	72	--
FLOW	0.75	17	10.2	37	--	15	29.4	--	--	24	--

RATE OF FLOW CALCULATIONS

COEFFICIENT (F <sub>s</sub> ) (F <sub>g</sub> ) Mcfd	(METER) (PROVER) PRESSURE psia	EXTENSION $\sqrt{P_m \times h_w}$	GRAVITY FACTOR F <sub>g</sub>	FLOWING TEMP. FACTOR Ft	DEVIATION FACTOR F <sub>pv</sub>	RATE OF FLOW R Mcfd	GOR	G <sub>m</sub>
2.779	31.4	17.93	1.2997	1.023	1.0015	66	--	--

(OPEN FLOW) (DELIVERABILITY) CALCULATIONS

(P<sub>c</sub>)<sup>2</sup> = 1.884 (P<sub>w</sub>)<sup>2</sup> = 0.864 P<sub>d</sub> = -- % (P<sub>c</sub> - 14.4) + 14.4 = -- (P<sub>d</sub>)<sup>2</sup> = 0.207

$\frac{(P_c)^2 - (P_d)^2}{(P_c)^2 - (P_w)^2}$	$\frac{P_c^2 - P_w^2}{P_c^2 - P_w^2}$	$\frac{P_c^2 - P_d^2}{P_c^2 - P_w^2}$	LOG [ ]	"n"	n x LOG [ ]	ANTILOG	OPEN FLOW DELIVERABILITY EQUALS R x ANTILOG Mcfd
1.677	1.019	1.645	0.216	0.85	0.184	1.53	101

OPEN FLOW Mcfd @ 14.65 psia DELIVERABILITY Mcfd @ 14.65 psia

The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated therein, and that said report is true and correct.

Executed this the 31<sup>st</sup> day of Dec, 1990

*John P. Sanders*  
For Company

Witness (if any)  
For Commission

Commissioner  
Kansas

Checked by