

**STATE OF KANSAS - CORPORATION COMMISSION**  
**ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST**

FORM O-2  
8-7-58  
15-091-20232-0000  
6-20-89

TYPE TEST:  Deliverability  Open Flow TEST DATE: 8-3-83

COMPANY: Bovina Petroleum Eng. LEASE: Cohu WELL NO.: #1

COUNTY: Johnson LOCATION: NW NE SECTION: 32- TWP: 13 RNO: 23 ACRES:

FIELD:  RESERVOIR:  PIPELINE CONNECTION:

COMPLETION DATE: 3-5-81 PLUG BACK TOTAL DEPTH:  PACKER SET AT:

CASINO SIZE: WT.  I.D.  SET AT  PERF. 588-593 TO 606-616

TUBING SIZE: WT.  I.D.  SET AT  PERF.  TO

TYPE COMPLETION (Describe):  TYPE FLUID PRODUCTION:

PRODUCING THRU:  RESERVOIR TEMPERATURE, F:  BAR. PRESS - P<sub>a</sub>: 14.4 Psia

GAS GRAVITY - G<sub>g</sub>: .605 STATE CORPORATION COMMISSION CARBON DIOXIDE:  NITROGEN:  API GRAVITY OF LIQUID:

VERTICAL DEPTH (ft):  TYPE METER CONN.:  (METER RUN)(PROVER) SIZE: 2" orifice well tester

SHUT-IN PRESSURE: SHUT IN 8-2 AT 1345 (AM)(PM) TAKEN 8-2 AT 1330 (AM)(PM)

FLOW TEST: STARTED 8-2 AT 1400 (AM)(PM) TAKEN 8-3 AT 1330 (AM)(PM)

**OBSERVED DATA** DURATION OF SHUT-IN:  HR.

SHUT-IN OR FLOW	ORIFICE SIZE in.	(METER) (PROVER) PRESSURE psig	DIFF. in. (h <sub>w</sub> )(h <sub>d</sub> )	FLOWING TEMP. t	WELL-HEAD TEMP. t	CASINO WELLHEAD PRESS.		TUBING WELLHEAD PRESS.		DURATION HOURS	LIQUID PROD. Bbls.
						psig	(P <sub>w</sub> )(P <sub>i</sub> )(P <sub>c</sub> ) psia	psig	(P <sub>w</sub> )(P <sub>i</sub> )(P <sub>c</sub> ) psia		
SHUT-IN								156	170.4		
FLOW	1/8	85						135	149.4	23.5	

**RATE OF FLOW CALCULATIONS**

COEFFICIENT (F <sub>p</sub> )(F <sub>o</sub> ) Mold	(METER) (PROVER) PRESSURE psia	EXTENSION $\sqrt{P_{mshw}}$	GRAVITY FACTOR $\gamma_g$	FLOWING TEMP. $T_L$	DEVIATION FACTOR $F_{pv}$	RATE OF FLOW R Mold	GOR	Q <sub>m</sub>
	2" orifice well tester		1.286			42.7		

**(OPEN FLOW) (DELIVERABILITY) CALCULATIONS**

(P<sub>c</sub>)<sup>2</sup> = 29.0 (P<sub>w</sub>)<sup>2</sup> = 22.3 P<sub>d</sub> = 87.7 % (P<sub>c</sub> - 14.4) + 14.4 = 170.4 (P<sub>d</sub>)<sup>2</sup> = 28.8

$\frac{(P_c)^2 - (P_w)^2}{(P_c)^2 - (P_d)^2}$	$(P_c)^2 - (P_w)^2$	$\frac{P_c^2 - P_d^2}{P_c^2 - P_w^2}$	LOG [ ]	"n"	n x LOG [ ]	ANTILOG	OPEN FLOW DELIVERABILITY EQUALS R x ANTILOG Mold
28.8	6.5	4.43077	.646479	.850	.549507	3.54411	151.3

OPEN FLOW 151 Mofd @ 14.65 psia DELIVERABILITY 151.3 Mofd @ 14.65 psia

The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated therein, and that said report is true and correct.

Executed this the \_\_\_\_\_ day of \_\_\_\_\_, 19\_\_\_\_.

\_\_\_\_\_  
Witness (if any)

\_\_\_\_\_  
For Commission

\_\_\_\_\_  
For Company

\_\_\_\_\_  
Checked by