

# KANSAS CORPORATION COMMISSION

## ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST

Type Test:

(See Instructions on Reverse Side)

- Open Flow  
 Deliverability

Test Date:  
3/07 to 3/08/11

API No. 15  
007-22,846 - 0000

Company F.G.Holl Co. LLC		Lease Lemon Trust B			Well Number 1-20
County Barber	Location SESENE	Section 20	TWP 30S	RNG (E/W) 13W	Acres Attributed
Field		Reservoir Viola	Gas Gathering Connection Oneok		
Completion Date 4/14/05		Plug Back Total Depth 4735	Packer Set at none		
Casing Size 4.5	Weight	Internal Diameter	Set at 4784	Perforations 4498	To 4523
Tubing Size 2.375	Weight	Internal Diameter	Set at 4575	Perforations	To
Type Completion (Describe) single		Type Fluid Production Oil/SW	Pump Unit or Traveling Plunger? Yes / No Yes - pumping unit		
Producing Thru (Annulus / Tubing) annulus		% Carbon Dioxide .205	% Nitrogen 5.915	Gas Gravity - G <sub>g</sub> .6915	
Vertical Depth(H)		Pressure Taps flange		(Meter Run) (Prover) Size 2"	
Pressure Buildup: Shut in 3/04 20 11 at 10:30 am (AM) (PM) Taken 3/07 20 11 at 10:30 am (AM) (PM)					
Well on Line: Started 3/07 20 11 at 10:30 am (AM) (PM) Taken 3/08 20 11 at 10:30 am (AM) (PM)					

### OBSERVED SURFACE DATA

Duration of Shut-in 72 Hours

Static / Dynamic Property	Orifice Size (inches)	Circle one: Meter or Prover Pressure psig (Pm)	Pressure Differential in Inches H <sub>2</sub> O	Flowing Temperature t	Well Head Temperature t	Casing Wellhead Pressure (P <sub>w</sub> ) or (P <sub>1</sub> ) or (P <sub>c</sub> )		Tubing Wellhead Pressure (P <sub>w</sub> ) or (P <sub>1</sub> ) or (P <sub>c</sub> )		Duration (Hours)	Liquid Produced (Barrels)
						psig	psia	psig	psia		
Shut-in						93.8	108.2			72	
Flow	.750	71	4.2	39		87.51	101.9			24	

### FLOW STREAM ATTRIBUTES

Plate Coefficient (F <sub>s</sub> ) (F <sub>p</sub> ) Mcfd	Circle one: Meter or Prover Pressure psia	Press Extension $\sqrt{P_m \times h}$	Gravity Factor F <sub>g</sub>	Flowing Temperature Factor F <sub>t</sub>	Deviation Factor F <sub>pv</sub>	Metered Flow R (Mcfd)	GOR (Cubic Feet/ Barrel)	Flowing Fluid Gravity G <sub>m</sub>
2.779	85.4	18.94	1.203	1.021	-----	65		.6915

### (OPEN FLOW) (DELIVERABILITY) CALCULATIONS

(P<sub>c</sub>)<sup>2</sup> = 11.707 ; (P<sub>w</sub>)<sup>2</sup> = 10.383 ; P<sub>d</sub> = \_\_\_\_\_ % (P<sub>c</sub> - 14.4) + 14.4 = \_\_\_\_\_ ; (P<sub>d</sub>)<sup>2</sup> = 0.207 ; (P<sub>d</sub>)<sup>2</sup> = \_\_\_\_\_

(P <sub>c</sub> ) <sup>2</sup> - (P <sub>w</sub> ) <sup>2</sup> or (P <sub>c</sub> ) <sup>2</sup> - (P <sub>d</sub> ) <sup>2</sup>	(P <sub>c</sub> ) <sup>2</sup> - (P <sub>w</sub> ) <sup>2</sup>	Choose formula 1 or 2: 1. P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> - P <sub>d</sub> <sup>2</sup> divided by: P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	LOG of formula 1, or 2, and divide by: $\frac{P_c^2 - P_w^2}{P_c^2 - P_d^2}$	Backpressure Curve Slope = "n" or Assigned Standard Slope	n x LOG [ ]	Antilog	Open Flow Deliverability Equals R x Antilog (Mcfd)
11.500	1.324	8.686	.9388	.850	.7979	6.28	
				assigned			

Open Flow 408 Mcfd @ 14.65 psia X .50 = Deliverability 204 Mcfd @ 14.65 psia

The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated therein, and that said report is true and correct. Executed this the 25th day of March, 20 11.

\_\_\_\_\_  
Witness (if any)  
\_\_\_\_\_  
For Commission

*Guy Allen*  
\_\_\_\_\_  
For Company  
Checked by

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MAR 29 2011  
KCC WICHITA

## Daily Meter Analysis Summary

**4480093 - LEMONS TRUST B 1-20**  
February 2011

<b>Pressure Base:</b> 14.65	<b>Atmos Pressure:</b> 14.40	<b>Pressure:</b> 69.2
<b>Temp Base:</b> 60.00	<b>Contract Day:</b> 1	<b>Temperature:</b> 41.3
	<b>Contract Hour:</b> 9	

Day	Relative Density	Dry Heating Value	Wet Heating Value	As Del Heating Value	CO2	N2	C1	C2	C3	iC4	nC4	iC5	nC5	C6	C7	C8	C9	C10	HCDP	CCT	Wobbe	
1	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
2	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
3	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
4	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
5	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
6	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
7	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
8	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
9	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
10	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
11	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
12	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
13	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
14	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
15	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
16	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
17	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
18	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
19	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
20	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
21	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
22	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
23	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
24	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
25	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
26	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
27	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
28	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46
Avg	0.6915	1115.24	1095.72		0.205	5.915	81.641	5.920	2.747	0.330	1.000	0.245	0.416	0.922								1348.46

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\*\*\* End of Report\*\*\*

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