## Kansas Corporation Commission One Point Stabilized Open Flow or Deliverability Test

	Type Test:					(506	Instructi	ions on	Reverse	e Side)					
County   Location   Section   TWP   RNG (E/W)   Acres Attributed   Seward   1331 FNL & 1250 FWL   & 8   345   33W   Acres Attributed   640   6	=				Test Date:	05/	11/2011			API No.		15175219680000			
Seward   1331 FNL & 1250 FWL   8   348   33W   640		Ainc	A L I	λĴ					LD A 4				w	ell Number	
Seward   1331 FNL & 1250 FWL   8   348   33W   640	County		Locati	ion	Se	ction		TWP		Ŕ	NG (E/W)		Ac	res Attributed	
SALLEY  Morrow/Chester  Plug Back Total Depth Packer Set at  Packer Set at  Packer Set at  Perforations  To  A1/2"  10.5# 4.052" 6,620" 6,632" 6,620" 6,637"  Total Depth Fill Perforations  To  2 3/8"  Tubing Size Weight Internal Diameter Set at  1.995"  1.995"  1.995" 6,179"  Tubing Size Weight Internal Diameter Set at  1.995" 6,179"  Tubing Size Weight Internal Diameter Set at  1.995" 6,179"  Type Completion (Describe)  Type Seam Pump  Producing Thru (Armutus 17ubing)  % Carbon Dioxide  Annutus  Wertical Depth (H)  Pressure Taps Finance  1.900  Finance  Shut in  0.5/10  20 at  0.187%  0.187	•	133 <sup>-</sup>													
Sezion   Casing Size   Weight   Internal Diameter   Set at   Perforations   To   6,140"							hester								
4 1/2"  10.5# 4.052" 6,620' 6,037' 6,140'  Tubing Size Weight Internal Diameter Set at 2/3"  17ye Completion (Describe)  Type Fluid Production  WATER  1995" 6,179'  Type Completion (Describe)  Type Fluid Production  WATER  Pump Unit or Traveling Plunger?  Yes - Beam Pump  Producing Trunk (Annutus / Tubing)  Annutus  Vertical Depth (H)  Flore  Pressure Taps  (Meter Run) (Prover) Size 3.068'  Pressure Buildup: Shut in 05/10 20 11 at 9:00  Well on Line: Shut in 05/10 20 at Taken 05/11 20 11 at 9:00  Well on Line: Shut in 05/10 20 at Taken 05/11 20 11 at 9:00  OBSERVED SURFACE DATA  OBSERVED S	•								P	acker Set at					
2 3/8"   4.7#   1.995"   6,179"				Int								· -			
Producing Thru (Annulus / Tubing) Annulus  **Net Carbon Dioxide** **O.187%** **O.187%** **O.187%** **O.187%* **O.187	Tubing Size Weight				Internal Diameter					Perforations		То			
Vertical Depth (H)	Type Completion (Describe)					Type Fluid Production				. P					
Pressure Buildup:   Shut in   05/10   20   11   at   9:00   Taken   05/11   20   11   at   9:00   at										%	-		, ,		
Pressure Buildup: Shut in 05/10 20 11 at 9:00 Taken 05/11 20 11 at 9:00  Well on Line: Shut in 20 at Taken 20 at T									s						
OBSERVED SURFACE DATA   Duration of Shut-in   24   Hours	Pressure B	Buildup:	Shut in	05/1	0 20	11 a				Taken	05/11	20 11	l at 9	:00	
Static   Orticle Dynamic Stze Property (nches)   Pressure Property (nches)   Pressure Property (nches)   Property Pressure Prope	Well on Lir	ne:	_	-				-		_		20	at	<del></del>	
State / Dynamic State / Prover Pressure / Press / Pr		<del></del>	·		<del></del>	(	OBSERV	ED SU	RFACE	DATA		Duration of	f Shut-in	24 Hours	
Property (nches) palg (Pm) inches H <sub>2</sub> O t t palg pals pals (Hours) (Berrels)  Shut-In 133.2 147.6 24  Flow STREAM ATTRIBUTES  FLOW STREAM ATTRIBUTES  FLOW STREAM ATTRIBUTES  Plate Conficient (F <sub>2</sub> (F <sub>2</sub> ) Meter or Prover Pressure pals P <sub>2</sub> x h F <sub>6</sub> F <sub>6</sub> F <sub>8</sub> Flowing Factor F <sub>8</sub> F <sub>8</sub> Flowing Factor F <sub>8</sub> (Cubic Feet/Barrel) Gravity G <sub>8</sub> (P <sub>6</sub> ) <sup>2</sup> = 0.207  (P <sub>6</sub> ) <sup>2</sup> - (P <sub>4</sub> ) <sup>3</sup> (P <sub>4</sub> ) <sup>3</sup> (P <sub>4</sub> ) <sup>2</sup> - (P <sub>4</sub> ) <sup>3</sup> (P <sub>4</sub> ) <sup>3</sup> - P <sub>4</sub> P <sub>2</sub> P <sub>4</sub> P <sub>5</sub> P <sub>4</sub> P <sub>5</sub> P <sub>7</sub> P <sub>7</sub> P <sub>7</sub> P <sub>7</sub> P <sub>7</sub> P <sub>8</sub>		Ortfice Meter Differe			Differential	ntial Flowing Well F		lead Wellhead Pressu		d Pressure	Wellhead Pressure		D. matter	Libraria Conduced	
Flow STREAM ATTRIBUTES  Flowing Coefficient Coefficient (F <sub>a</sub> )(F <sub>a</sub> ) Motor or Prover Pressure pela P <sub>a</sub> x h F <sub>a</sub>															
FLOW STREAM ATTRIBUTES  Plats Coefficient (F <sub>a</sub> )(F <sub>a</sub> ) Moder or Prover Pressure pala  (P <sub>a</sub> ) <sup>2</sup> = 0.0  (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) - (P <sub>a</sub> ) - (P <sub>a</sub> ) <sup>2</sup> (P <sub>a</sub> ) - (P <sub>a</sub>	Shut-In								133.2	147.6			24		
Plate Confficient Confficient (F <sub>a</sub> )(F <sub>a</sub> ) Mctd Prover Pressure pale  (P <sub>a</sub> ) <sup>2</sup> = 0.0  (P <sub>a</sub> ) <sup>2</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup>3</sup> Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) Prover (P <sub>a</sub> ) <sup>3</sup> - (P <sub>a</sub> ) <sup></sup>	Flow										1				
Coefficient (F <sub>0</sub> ) (F <sub>0</sub>	i					F	LOW ST	ream	ATTRIE	BUTES					
(P <sub>c</sub> ) <sup>2</sup> = #VALUE! : (P <sub>w</sub> ) <sup>2</sup> = 0.0 : P <sub>d</sub> = % (P <sub>c</sub> - 14.4) + 14.4 = : (P <sub>d</sub> ) <sup>2</sup> = 0  (P <sub>d</sub> ) <sup>2</sup> · (P <sub>d</sub> ) <sup>3</sup>   (P <sub>d</sub> ) <sup>2</sup> · (P <sub>e</sub> ) <sup>2</sup>   Choose Formuta 1 or 2: 1.0G of formuta 1 or 2: 1.0 or 1. P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup>   P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup>   1. or 2. and divide by: P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup>   P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup>   P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup>   P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup>   P <sub>e</sub> <sup>2</sup> · P <sub>e</sub> <sup>2</sup>	Coefficien (F <sub>b</sub> ) (F <sub>p</sub> )	ıt i	Meter or Exter Prover Pressure		nsion	n Factor		actor serature	Factor		R			Fluid Gravity	
(P <sub>c</sub> ) <sup>2</sup> = #VALUE! : (P <sub>w</sub> ) <sup>2</sup> = 0.0 : P <sub>d</sub> = % (P <sub>c</sub> - 14.4) + 14.4 = : (P <sub>d</sub> ) <sup>2</sup> = 0  (P <sub>e</sub> ) <sup>2</sup> - (P <sub>e</sub> ) <sup>3</sup>   (P <sub>e</sub> ) <sup>2</sup> - (P <sub>e</sub> ) <sup>2</sup>   Choose Formula 1 or 2: 1.0G of formula 1 or 2: 1.0 or															
Choose Formula 1 or 2: 1, P <sub>a</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> or (P <sub>e</sub> ) <sup>2</sup> - (P <sub>e</sub> ) <sup>2</sup> (P <sub>e</sub> ) <sup>2</sup> - (P <sub>e</sub> ) <sup>2</sup> Choose Formula 1 or 2: 1, P <sub>a</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> 2, P <sub>a</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> divided by: P <sub>a</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> divided by: P <sub>a</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> Copen Flow  Open Flow  Open Flow  Open Flow  Open Flow  Standard Slope  The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated therein, and that said report is true and correct.  Executed this the  21 day of  OXY USA-Inc:  For Company  David Ogden Oxy USA Incire	(P <sub>c</sub> ) <sup>2</sup> = #V	'ALUE! :	(P <sub>w</sub> ) <sup>2</sup> :	= 0.0			W) (DEL		-			:	-		
The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated therein, and that said report is true and correct. Executed this the 21 day of July 2011.  OXY USA-Inc:  For Company  David Ogden Oxy USA Inc.	(P <sub>e</sub> ) <sup>2</sup> - (P <sub>e</sub> ) or (P <sub>e</sub> ) <sup>2</sup> - (P <sub>e</sub> )	(P <sub>1</sub> ) <sup>2</sup>	(P <sub>e</sub> ) <sup>2</sup> - (P <sub>e</sub> ) <sup>2</sup>		P <sub>6</sub> <sup>2</sup>	formula 1. or 2. nd divide	P <sub>e</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup>	-	Slope = "n" Or Assigned		xŁOG		Antillog	Deliverability Equals R x Antilog	
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Witness  David Ogden Oxy USA Inc.			The undersign	ed authority	, on behalf of I	the Company		he is duly	y authorize			d that he has k		. 2011 .	
David Ogden Oxy USA Inc.			1.641	inase.										$\overline{}$	
For Commission									_		David (	C	6-1	c/	

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KCC WICHITA

I declare under penalty of perjury under the laws of the state of Kansas that I am authorized to request exempt status under Rule C.A.R. 82-3-304 on behalf of the operator  OXY USA Inc. and that the foregoing pressure information and statements ontained on this application form are true and correct to the best of my knowledge and belief based upon available production summaries and lease records of equipment installation and/or upon type of completion or upon use being made of the gas well herein named.  I hereby request a one-year exemption from open flow  FITZGERALD A 4  for the gas well on the grounds that aid well:
(Check one)
is a coalbed methane producer
is cycled on plunger lift due to water
is a source of natural gas for injection into an oil reservoir undergoing ER
is on a vacuum at the present time; KCC approval Docket No.
is not capable of producing at a daily rate in excess of 250 mcf/D
I further agree to supply to the best of my ability any and all supporting documents deemed by Commission staff as necessary to comborate this claim for exemption from testing.
Date: July 21, 2011
David Ogden
Signature: OXY USA Inc
Title: Gas Business Coordinator

Instructions: If a gas well meets one of the eligibility criteria set out in the KCC regulation K.A.R. 82-3-304, the operator may complete the statement provided above in order to claim exempt status for the gas well.

At some point during the current calendar year, wellhead shut-in pressure shall have been measured after a minimum of 24 hours shut-in/buildup time and shall be reported on the front side of this form under OBSERVED SURFACE DATA. Shut-in pressure shall thereafter be reported yearly in the same manner for so long as the gas well continues to meet the eligibility criterion or until the claim of eligibility for exemption IS denied.

The G-2 form conveying the newest shut-in pressure reading shall be filed with the Wichlta office no later than December 31st of the year for which it's intended to acquire exempt status for the subject well. The form must be signed and dated on the front side as though it was a verified report of annual test results.

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