## KANSAS CORPORATION COMMISSION ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST

Type Test: Open F				cj	OO HISHOUN		rerse Side)				
T Derives	Flow rabilty			Test Date:	12-10	s - 20	11	API N	lo. 15 - /7	5-2/979	-0000
Company	1615	CASEL	Geroc	4 57 O N	)	Lease	ISINGE	-R		W	ell Number
	-			Section	<del></del>	TWP		RNG (E/M	n	A	cres Attributed
County.		5/4 4	SNW	//	•	3/		3			560
Field	<u> </u>			Reservoir				Gas Gathe	ering Connec	tion	
THIRTY	V DAIS	SAST		CHES	tee Si	2		De	P MIOS	REAM	
Completion I				Plug Back	Total Depth			Packer Se			
11-5-	2008			560	00				<u>47</u>		
Casing Size		Weight		Internal D		Set a		Perfora	ations 547	70 TO	195
4.5"	5" 10.5#		4.095"		58/2		Perforations		To 5495		
Tubing Size	- 11	Weight	<i>D</i> .	Internal D	lameter 995 "	Set a	nt -460	Perrora		ENDED	
2.375	<u> </u>		7		Production			Puma Uni	- ·	Plunger? Yes /	No
Type Comple	etion (De	scribe)			r./Con	n erni et e		i amp om		No	
Singi		ulus / Tubing)			arbon Dioxid			% Nitroge	n	Gas Gra	vity - G
	•	ulus / tening/			. 245			Š.	165	.66	3 <b>3</b>
1/48			<del></del>			ure Taps				Meter R	un (Prover) Size
Vertical Dept	3 <i>1</i> Z									2.0	67
340	7				10:00	- Trage		/9-/	<u> </u>	J. 0 11	
Pressure Bu	uildup: S	Shut in	2	) <u>//</u> at	70.00	(PM)	Taken		20 1	ai	= (MI)(FM)
Well on Line	e: 5	Started	2	at		(AM) (PM)	Taken		20	at	(AM) (PM)
					OBSERVE	SURFAC	E DATA			Duration of Shut-i	n Hour
Static /	/ Orifice Circle one: Pressure			Flowing Well Head		Casing		Tubing		Duration	Liquid Produced
Dynamic :	Size	Meter Prover Pressur	Differential e in		Temperature	Wellhead Pressure (P_) or (P <sub>i</sub> ) or (P <sub>a</sub> )		Wellhead Pressure $(P_w)$ or $(P_t)$ or $(P_c)$		(Hours)	(Barrels)
Property (	(inches)	psig (Pm)	Inches H <sub>2</sub> 0	t	t	paig	psla	palg	psta	<u> </u>	
Shut-In				-			Mage.	782	796.4	24	
						T					
Flow					<u> </u>						
Flow					FLOW STR	EAM ATTI	RIBUTES				
Flow		Circle one:	Press	Grav	uttv	Flowing		lation	Matered Flow		Flowing
Plate Coefficcien	n	Meter or	Extension	Fac	rity 1		Dev Fa	ctor	R	(Cubic Fed	Fluid
Plate Coefficcien (F <sub>b</sub> ) (F <sub>p</sub> )	n				rity 1	Flowing emperature	Dev Fa	· .			et/ Fluid
Plate Coefficcien	n	Meter or over Pressure	Extension	Fac	rity 1	Flowing Temperature Factor	Dev Fa	ctor	R	(Cubic Fed	et/ Fluid Gravity
Plate Coefficcien (F <sub>s</sub> ) (F <sub>p</sub> )	n	Meter or over Pressure	Extension	Fac	rity T	Flowing emperature Factor F <sub>11</sub>	Dev Fe	ector F <sub>pv</sub>	R	(Cubic Fe Barrel)	et/ Fluid Gravity G <sub>m</sub>
Plate Coefficien (F <sub>b</sub> ) (F <sub>p</sub> ) Mcfd	n	Meter or over Pressure psla	Extension	Fac F	ow) (DELIV	Flowing Femperature Factor F <sub>f1</sub>	Dev Fe	ATIONS	R	(Cubic Fe Barrel)	Fluid Gravity G <sub>m</sub>
Plate Coefficcien (F <sub>b</sub> ) (F <sub>p</sub> )	n	Metar or over Pressure pala $(P_w)^2 =$	Extension	(OPEN FL	ow) (DELIV	Flowing Femperature Factor F <sub>11</sub>	Pov Fe 1  Y) CALCUI  (P <sub>c</sub> - 14.4) -	ATIONS	R	(Cubic Fe Barrel)	Fluid Gravity G <sub>m</sub>
Plate Coefficien (F <sub>b</sub> ) (F <sub>p</sub> ) Mcfd	Pro	Metar or over Pressure pala $(P_w)^2 =$	Extension  P <sub>m</sub> x h	(OPEN FL	ow) (DELIV	Flowing femperature Factor F <sub>11</sub> ERABILIT % Backp	Y) CALCUI (P <sub>c</sub> - 14.4) +	ATIONS	R (Mcfd)	(Cubic Fer Barrel) (P <sub>a</sub> )	Fluid Gravity G <sub>m</sub> 2 = 0.207 2 = Open Flow Deliverability
Plate Coefficien (F <sub>b</sub> ) (F <sub>p</sub> ) Mcfd  (P <sub>o</sub> ) <sup>2</sup> =	Pro	Metar or over Pressure psla $(P_{w})^{2} =$	Extension  Pmxh  : Choose formula 1 or 3	(OPEN FL P <sub>d</sub> =  LOG of tormula 1. or 2.	OW) (DELIV	Flowing Femperature Factor F <sub>11</sub> ERABILIT % Backp	Per	ATIONS	R (Mcfd)	(Cubic Fe Barrel)	Pluid Gravity G <sub>m</sub> 2 = 0.207 2 = Open Flow Deliverability Equals R x Antibo
Plate Coefficien (F <sub>b</sub> ) (F <sub>p</sub> ) Mctd  (P <sub>o</sub> ) <sup>2</sup> =	Pro	Metar or over Pressure pala $(P_w)^2 =$ $P_v)^2 - (P_w)^2$	Extension  P <sub>m</sub> x h  : Choose formula 1 or:  1. P <sub>6</sub> -P <sub>8</sub>	(OPEN FL P <sub>d</sub> =  t: LOG of tormula 1. or 2. and divide	OW) (DELIV	Flowing Femperature Factor F <sub>11</sub> ERABILIT % Backp	Y) CALCUI (P <sub>c</sub> - 14.4) +	ATIONS	R (Mcfd)	(Cubic Fer Barrel) (P <sub>a</sub> )	Fluid Gravity G <sub>m</sub> 2 = 0.207
Plate Coefficien (F <sub>b</sub> ) (F <sub>p</sub> ) Motd  (P <sub>o</sub> ) <sup>2</sup> =	Pro	Metar or over Pressure pala $(P_w)^2 =$ $P_v)^2 - (P_w)^2$	Extension  P <sub>m</sub> x h  : Choose formula: 1 or: 1. P <sub>e</sub> <sup>2</sup> -P <sub>e</sub> <sup>2</sup> 2. P <sub>e</sub> <sup>2</sup> -P <sub>e</sub> <sup>2</sup>	(OPEN FL P <sub>d</sub> =  t: LOG of tormula 1. or 2. and divide	OW) (DELIV	Flowing Femperature Factor F <sub>11</sub> ERABILIT % Backp	Per	ATIONS	R (Mcfd)	(Cubic Fer Barrel) (P <sub>a</sub> )	Fluid Gravity G <sub>m</sub> 2 = 0.207 2 = Open Flow Deliverability Equals R x Antilog
Plate Coefficien (F <sub>b</sub> ) (F <sub>p</sub> ) Mctd  (P <sub>o</sub> ) <sup>2</sup> =	Pro	Metar or over Pressure pala $(P_w)^2 =$ $P_v)^2 - (P_w)^2$	Extension  P <sub>m</sub> x h  : Choose formula: 1 or: 1. P <sub>e</sub> <sup>2</sup> -P <sub>e</sub> <sup>2</sup> 2. P <sub>e</sub> <sup>2</sup> -P <sub>e</sub> <sup>2</sup>	(OPEN FL P <sub>d</sub> =  t: LOG of tormula 1. or 2. and divide	OW) (DELIV	Flowing Femperature Factor F <sub>11</sub> ERABILIT % Backp	Per	ATIONS	R (Mcfd)	(Cubic Fer Barrel) (P <sub>a</sub> )	Fluid Gravity G <sub>m</sub> 2 = 0.207 2 = Open Flow Deliverability Equals R x Antilog
Plate Coefficien (F <sub>b</sub> ) (F <sub>p</sub> ) Mctd  (P <sub>o</sub> ) <sup>2</sup> =	: : : : : : : : : : : : : : : : : : :	Metar or over Pressure pala $(P_w)^2 =$ $P_v)^2 - (P_w)^2$	Extension  P <sub>m</sub> x h  : Choose formula: 1 or: 1. P <sub>e</sub> <sup>2</sup> -P <sub>e</sub> <sup>2</sup> 2. P <sub>e</sub> <sup>2</sup> -P <sub>e</sub> <sup>2</sup>	(OPEN FL  P <sub>d</sub> =  t: LOG of tormula 1. or 2. and divide by:	OW) (DELIV	Flowing Femperature Factor F <sub>11</sub> ERABILIT % Backp	Per	ATIONS	R (Mcfd)	(Cubic Fer Barrel) (P <sub>a</sub> )	Open Flow Deliverability Equals R x Antilog (Mcfd)
Plate Coefficien (F <sub>o</sub> ) (F <sub>o</sub> ) Mcfd  (P <sub>o</sub> ) <sup>2</sup> =  (P <sub>o</sub> ) <sup>2</sup> - (P <sub>o</sub> ) Open Flow The un	Pro	Metar or over Pressure pala $(P_{w})^{2} = P_{w}^{2} \cdot (P_{w})^{2}$ and authority, o	Extension  P <sub>m</sub> x h  : Choose formula 1 or 2  1. P <sub>2</sub> -P <sub>2</sub> 2. P <sub>2</sub> -P <sub>2</sub> Avided by: P <sub>2</sub> -P <sub>3</sub> Mcfd ② 14	(OPEN FL  Pd =  COMPANDA  LOG of formula 1 or 2 and divide by:  .85 psia	OW) (DELIV	Flowing Femperature Factor Fit  ERABILIT  Backp Si Star  Deliver	Y) CALCUI (P <sub>c</sub> - 14.4) + ressure Curviope = *n*	ATIONS 14.4 =	R (Mdd)	(Cubic Fer Barrel)  {P <sub>a</sub> }  (P <sub>d</sub> )	Open Flow Deliverability Equals R x Antilog (Modd)
Plate Coefficien (F <sub>o</sub> ) (F <sub>o</sub> ) Mcfd  (P <sub>o</sub> ) <sup>2</sup> =  (P <sub>o</sub> ) <sup>2</sup> - (P <sub>o</sub> ) Open Flow The un	Pro	Metar or over Pressure pala $(P_{w})^{2} = P_{w}^{2} \cdot (P_{w})^{2}$ and authority, o	Extension  P <sub>m</sub> x h  : Choose formula 1 or 2  1. P <sub>a</sub> <sup>2</sup> -P <sub>a</sub> <sup>2</sup> 2. P <sub>a</sub> <sup>2</sup> -P <sub>a</sub> <sup>2</sup> divided by: P <sub>a</sub> <sup>2</sup> -P <sub>a</sub> Mcfd ② 14	(OPEN FL  Pd =  COMPANDA  LOG of formula 1 or 2 and divide by:  .85 psia	OW) (DELIV	Flowing Femperature Factor Fit  ERABILIT  Backp Si Star  Deliver	Y) CALCUI (P <sub>c</sub> - 14.4) + ressure Curviope = *n*	ATIONS 14.4 =	R (Mdd)	(Cubic Fer Barrel)  (P <sub>a</sub> )  (P <sub>d</sub> )  Antilog	Open Flow Deliverability Equals R x Antibot (Mctd)
Plate Coefficien (F <sub>o</sub> ) (F <sub>o</sub> ) Mcfd  (P <sub>o</sub> ) <sup>2</sup> =  (P <sub>o</sub> ) <sup>2</sup> - (P <sub>o</sub> ) Open Flow The un	Pro	Metar or over Pressure pala $(P_{w})^{2} = P_{w}^{2} \cdot (P_{w})^{2}$ and authority, o	Extension  P <sub>m</sub> x h  : Choose formula 1 or 2  1. P <sub>2</sub> -P <sub>2</sub> 2. P <sub>2</sub> -P <sub>2</sub> Avided by: P <sub>2</sub> -P <sub>3</sub> Mcfd ② 14	(OPEN FL  Pd =  COMPANDA  LOG of formula 1 or 2 and divide by:  .85 psia	OW) (DELIV	Flowing Femperature Factor Fit  ERABILIT  Backp Si Star  Deliver	Y) CALCUI (P <sub>c</sub> - 14.4) + ressure Curviope = *n*	ATIONS 14.4 =	R (Mcfd)	(Cubic Fer Barrel)  (Pa)  (Pa)  Antilog  Mcfd © 14.65 psort and that he had the series are all the series ar	Open Flow Deliverability Equals R x Antilor (Mcfd)
Plate Coefficien (F <sub>o</sub> ) (F <sub>o</sub> ) Mcfd  (P <sub>o</sub> ) <sup>2</sup> =  (P <sub>o</sub> ) <sup>2</sup> - (P <sub>o</sub> ) Open Flow The un	Pro	Metar or over Pressure pala $(P_{w})^{2} = P_{w}^{2} \cdot (P_{w})^{2}$ and authority, o	Extension  P <sub>m</sub> x h  : Choose formula 1 or:  1. P <sub>c</sub> <sup>2</sup> -P <sub>c</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> -P <sub>c</sub> divided by: P <sub>c</sub> <sup>2</sup> -P <sub>c</sub> Mcfd	(OPEN FL  Pd =  COMPANDA  LOG of formula 1 or 2 and divide by:  .85 psia	OW) (DELIV	Flowing Femperature Factor Fit  ERABILIT  Backp Si Star  Deliver	Y) CALCUI (P <sub>c</sub> - 14.4) + ressure Curviope = *n*	ATIONS 14.4 =	R (Mcfd)	(Cubic Fer Barrel)  {P <sub>a</sub> }  (P <sub>d</sub> )	Open Flow Deliverability Equals R x Antilog (Modd)

DEC 1 9 2011 KCC WICHITA

exemple and the correct of equal to the correct of equ	declare under penalty of perjury under the laws of the state of Kansas that I am authorized to request pt status under Rule K.A.R. 82-3-304 on behalf of the operator <u>EAGLE CREEK CORPOLATION</u> nat the foregoing pressure information and statements contained on this application form are true and ct to the best of my knowledge and belief based upon available production summaries and lease records sipment installation and/or upon type of completion or upon use being made of the gas well herein named. Thereby request a one-year exemption from open flow testing for the <u>GEISINGER</u> 4-1/1 rell on the grounds that said well:
	is a coalbed methane producer is cycled on plunger lift due to water is a source of natural gas for injection into an oil reservoir undergoing ER is on vacuum at the present time; KCC approval Docket No. is not capable of producing at a daily rate in excess of 250 mcf/D further agree to supply to the best of my ability any and all supporting documents deemed by Commission as necessary to corroborate this claim for exemption from testing.
Date: _	12-16-11
	Signature: Lullust  Title: Resident

Instructions:

If a gas well meets one of the eligibility criteria set out in KCC regulation K.A.R. 82-3-304, the operator may complete the statement provided above in order to claim exempt status for the gas well.

At some point during the current calendar year, wellhead shut-in pressure shall have been measured after a minimum of 24 hours shut-in/buildup time and shall be reported on the front side of this form under **OBSERVED SURFACE DATA**. Shut-in pressure shall thereafter be reported yearly in the same manner for so long as the gas well continues to meet the eligibility criterion or until the claim of eligibility for exemption IS denied.

The G-2 form conveying the newest shut-in pressure reading shall be filed with the Wichita office no later than December 31 of the year for which it's intended to acquire exempt status for the subject well. The form must be signed and dated on the front side as though it was a verified report of annual test results.