KANSAS CORPORATION COMMISSION
ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST
(See Instructions on Reverse Side)

Type Test:

[✓] Open Flow

[ ] Deliverabilty

Test Date: 7/28/2013

API No. 15: 15-187-21224-00-00

Company	Lease	Well Number
Linn Operating Inc	Spurgeon	4 ATU-71

County	Location	Section	TWP	RNG (E/W)	Acres Attributed
Stanton	NW NW NW NW	16	28S	39W	640

Field	Reservoir	Gas Gathering Connection
Hugoton-Panoma	Chase	Jayhawk Gas Plant

Completion Date	Plug Back Total Depth	Packer Set at
6/20/2013	2580	NA

Casing Size	Weight	Internal Diameter	Set at	Perforations	To
5.5	15.5	4.95	3084	2297	2468

Tubing Size	Weight	Internal Diameter	Set at	Perforations	To
NA	NA	NA	NA	NA	NA

Type Completion (Describe)	Type Fluid Production	Pump Unit or Traveling Plunger? Yes / No
Single	Dry Gas	NO

Producing Thru (Annulus / Tubing)	% Carbon Dioxide	% Nitrogen	Gas Gravity - G_g
Annulus	.0729	16.2999	.7280

Vertical Depth(H)	Pressure Taps	(Meter Run) (Prover) Size
	Flange	3.068

Pressure Buildup: Shut in 7/28 20 13 at 11:00 AM (AM) (PM) Taken 7/31 20 13 at 11:00 AM (AM) (PM)

Well on Line: Started 7/31 20 13 at 11:00 AM (AM) (PM) Taken 8/1 20 13 at 11:00 AM (AM) (PM)

OBSERVED SURFACE DATA

Duration of Shut-in 72 Hours

Static / Dynamic Property	Orifice Size (inches)	Circle one: Meter Prover Pressure psig (Pm)	Pressure Differential in Inches H_2O	Flowing Temperature t	Well Head Temperature t	Casing Wellhead Pressure (P_w) or (P_t) or (P_c) psig	psia	Tubing Wellhead Pressure (P_w) or (P_t) or (P_c) psig	psia	Duration (Hours)	Liquid Produced (Barrels)
Shut-In	1	43.2	43.2	73	73	43.2	57.6	NA	NA	72	0
Flow	1	37.0	37.0	73	73	37.0	51.4	NA	NA	24	0

FLOW STREAM ATTRIBUTES

Plate Coeffiecient (F_b) (F_p) Mcfd	Circle one: Meter or Prover Pressure psia	Press Extension $\sqrt{P_m \times h}$	Gravity Factor F_g	Flowing Temperature Factor F_{tt}	Deviation Factor F_{pv}	Metered Flow R (Mcfd)	GOR (Cubic Feet/ Barrel)	Flowing Fluid Gravity G_m
4.912	51.4	32.697	1.172	.9877	1	185.928	0	0

(OPEN FLOW) (DELIVERABILITY) CALCULATIONS

$(P_c)^2 =$ 3.3178 : $(P_w)^2 =$ 2.6420 : $P_d =$ ___ % $(P_c - 14.4) + 14.4 =$ ___ :

$(P_a)^2 =$ 0.207

$(P_d)^2 =$ ___

$(P_c)^2 - (P_a)^2$ or $(P_c)^2 - (P_d)^2$	$(P_c)^2 - (P_w)^2$	Choose formula 1 or 2. 1. $P_c{}^2 - P_a{}^2$ 2. $P_c{}^2 - P_d{}^2$ divided by: $P_c{}^2 - P_w{}^2$	LOG of formula 1. or 2. and divide by: $P_c{}^2 - P_w{}^2$	Backpressure Curve Slope = "n" ------ or ------ Assigned Standard Slope	n x LOG [ ]	Antilog	Open Flow Deliverability Equals R x Antilog (Mcfd)
3.1108	.6758	4.607	.663	.85	.5636	3.6609	680.6675

Open Flow	Mcfd @ 14.65 psia	Deliverability	Mcfd @ 14.65 psia

The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated therein, and that said report is true and correct. Executed this the 1st day of August , 20 13 .

Shawn Hildreth

For Company

Witness (if any)

For Commission

Checked by

CONSERVATION DIVISION
WICHITA, KS