

**KANSAS CORPORATION COMMISSION**  
**ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST**

FORM G-2  
(Rev.8/98)

TYPE TEST:

- Open Flow  
 Deliverability

TEST DATE: 9/13/2013

API No. 15-119-21342-00-00

Company Herman L. Loeb LLC		Lease Henry Taylor			Well Number 3-28	
County Meade	Location 1453'FNL 1401'	Section 38	TWP 34s	RNG (E/W) 26	Acres Attributed	
Field McKinney	Reservoir Chester Sand	Gas Gathering Connection DCP				
Completion Date 8/10/2013	Plug Back Total Depth 6495	Packer Set at none				
Casing Size 5.500	Weight 17.000	Internal Diameter 4.892	Set at 6576	Perforations 6425	To 6432	
Tubing Size 2.875	Weight 6.500	Internal Diameter 2.441	Set at 6440	Perforations	To	
Type Completion (Describe) perf	Type Fluid Production trace water	Pump Unit or Traveling Plunger? no				
Producing Thru (Annulus/Tubing) tubing	% Carbon Dioxide 0.210	% Nitrogen 9.038		Gas Gravity- Gg 0.672		
Vertical Depth (ft) 6428	Pressure Taps	Meter Run Size 3.068				
Pressure Buildup: Shut in	8/15/2012@1200	TAKEN	9/12/2012@1715			
Well on Line: Started	9/12/2012@1715	TAKEN	9/13/2013@2100			

**OBSERVED SURFACE DATA**

Static/ Dynamic Property	Orifice Size in.	Meter Pressure psig	Pressure Diff. In. H <sub>2</sub> O	Flowing Temp. t.	WellHead Temp. t.	Casing WellHead Press. (P <sub>w</sub> ) (P <sub>t</sub> ) (P <sub>c</sub> )		Tubing WellHead Press. (P <sub>w</sub> ) (P <sub>t</sub> ) (P <sub>c</sub> )		Duration (Hours)	Liquid Prod. Barrels
						psig	psia	psig	psia		
Shut-in						1710	1724	1706	1720		
Flow	1.250	95.1	8.10	65		1432	1446	1092	1106		4.2

**FLOW STREAM ATTRIBUTES**

COEFFICIENT (F <sub>b</sub> ) Mcf/d	(METER) PRESSURE psia	EXTENSION $\sqrt{P_m \times H_w}$	GRAVITY FACTOR F <sub>g</sub>	FLOWING TEMP FACTOR F <sub>t</sub>	DEVIATION FACTOR F <sub>pv</sub>	RATE OF FLOW R Mcf/d	GOR	G <sub>m</sub>
7.771	109.5	29.78	1.2199	0.9952	1.0090	283		0.672

**(OPEN FLOW)(DELIVERABILITY) CALCULATIONS**

(P<sub>c</sub>)<sup>2</sup> = 2973.6      (P<sub>w</sub>)<sup>2</sup> = 2092.1      P<sub>d</sub> = 6.3      %      (P<sub>c</sub> - 14.4) + 14.4 =      (P<sub>a</sub>)<sup>2</sup> = 0.207  
(P<sub>d</sub>)<sup>2</sup> = 11.98

$(P_c)^2 - (P_a)^2$ or $(P_c)^2 - (P_d)^2$	$(P_c)^2 - (P_w)^2$	$\frac{(P_c)^2 - (P_a)^2}{(P_c)^2 - (P_d)^2}$ or $\frac{(P_c)^2 - (P_a)^2}{(P_c)^2 - (P_w)^2}$	LOG	Backpressure Curve Slope "n" ----- or ----- Assigned Standard Slope	n x LOG	Antilog	Open Flow Deliverability = R x Antilog Mcf/d
2973.35	881.48	3.373	0.5280	0.551	0.2909	1.954	553
2961.57	881.48	3.360	0.5263	0.551	0.2900	1.950	552

OPEN FLOW      553      Mcfd @ 14.65 psia      DELIVERABILITY      552      Mcfd @ 14.65 psia

The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated herein and that said report is true and correct. Executed this the 30 day of Sept, 2013

\_\_\_\_\_  
Witness (if any)

RECEIVED  
KANSAS CORPORATION COMMISSION

\_\_\_\_\_  
For Company

\_\_\_\_\_  
For Commission

**OCT 02 2013**

CONSERVATION DIVISION  
WICHITA, KS

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Checked by