## KANSAS CORPORATION COMMISSION ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST

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De		•	,		Test Dat	e:			. AP	l No. 15		
Deliverabilty				10/24/2					5-20797 <b>- 00</b> (	00		
Company Red Hills Resources, Inc.							Lease Theis C				1-34	Well Number
County Clark	Location NE SW NE		Section 34		TWP 34S		RNG (E/W) · 25W		Acres Attributed 320			
ield 1cKinney			Reservoi <b>Mississ</b>		i	,		thering Connec <b>Midstream</b>	ction .	DEC A		
Completion Date 5/22/1984				Plug Bad 6000	ck Total Dep	th .		Packer : None	Set at	• .	KOO.	
.5"				Internal I 4.05"	Diameter	Set a	at .	Perforations 5669-5675		Acres Attributed 320 RECE ection  DEC 07 To 5734-5740		
ubing Size Weight 3/8" 4.7#				Internal I 1.995"	Diameter 		Set at Perforations 5714		orations	То	-,	
Acid fra	ac	(Describe)			Salt w				Pump U <b>No</b>	nit or Traveling F	Plunger? Yes	·/ No
roducing Thru (Annulus / Tubing)				% (	Carbon Dioxi	de ·		% Nitrogen		Gas Gravity - G		
rertical Depth(H)					Pressure Taps					(Meter Run) (Prover) Size		
ressure	Buildup	: Shut in _	10/24	2	0_12_at_5	:00 pm	(AM) (PM)	Taken10	)/25	20	12 <sub>at</sub> 5:00 p	m (AM) (PM)
Vell on L			-			and the second second						(AM) (PM)
	T					OBSERVE	D SURFACE	E DATA ·		. D	ouration of Shut-	inHours
Static / Dynamic Property	Orific Size (inche	Meter Prover Pressure		Pressure Differential in Inches H <sub>2</sub> 0	Flowing Temperature t	Well Head Temperature t	Casing Wellhead Pressure (P <sub>w</sub> ) or (P <sub>i</sub> ) or (P <sub>c</sub> ) psig psia		Tubing Wellhead Pressure (P <sub>w</sub> ) or (P <sub>t</sub> ) or (P <sub>c</sub> ) psig psia		Duration (Hours)	Liquid Produced (Barrels)
Shut-In							40	pola .	Parg	psia		<del>                                     </del>
Flow												
						FLOW STR	EAM ATTRI	BUTES	J			
Plate Coeffiec	ient p)	Circle one: Meter or Prover Pressu psia		Press Extension ✓ P <sub>m</sub> x h	Grav Faci F	vity T	EAM ATTRI Flowing emperature Factor F <sub>11</sub>	Devi	ation ctor	Metered Flow R (Mcfd)	GOR (Cubic Fer Barrel)	Flowing Fluid Gravity G <sub>m</sub>
Plate Coeffiec (F <sub>b</sub> ) (F	ient p)	Meter or Prover Pressu		Extension	Fact F <sub>c</sub>	vily T	Flowing emperature Factor F <sub>II</sub>	Devi Fa F	ctor	B	(Cubic Fee	et/ Fluid Gravity
Plate Coeffiec (F <sub>b</sub> ) (F Mcfd	ient p)	Meter or Prover Pressu	) <sup>2</sup> =	Extension  ✓ P <sub>m</sub> x h	Fact F <sub>c</sub>	ow) (DELIV	Flowing emperature Factor F <sub>II</sub>	Devi Fa F	ctor pv ATIONS	B	(Cubic Fed Barrel)	et/ Fluid Gravity G <sub>m</sub>
Plate Coeffiec (F <sub>b</sub> ) (F Mcfd	ient p)	Meter or Prover Pressu psia	) <sup>2</sup> = Choo	Extension	Factor Fa	ow) (DELIV	Flowing emperature Factor F <sub>11</sub> :  ERABILITY) 6 (P  Backpres Slop  Ass	Devi Fa F	ctor pv ATIONS	R (Mcfd)	(Cubic Fer Barrel)	et/ Fluid Gravity G <sub>m</sub>
Plate Coeffiec  ( $F_b$ ) ( $F_b$	ient p)	Meter or Prover Pressu psia	) <sup>2</sup> = Choo	Extension  P <sub>m</sub> xh  : ass formula 1 or 2:  1. P <sub>c</sub> <sup>2</sup> - P <sub>e</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> · P <sub>c</sub> <sup>2</sup>	Facing Fa	OW) (DELIVI	Flowing emperature Factor F <sub>11</sub> :  ERABILITY) 6 (P  Backpres Slop  Ass	CALCUL  c - 14.4) +  sure Curve e = "n" or igned	ATIONS 14.4 =	R (Mcfd)	(Cubic Fer Barrel) (P <sub>a</sub> ) <sup>2</sup>	et/ Fluid Gravity G  P = 0.207  P = Open Flow Deliverability Equals R x Antilog
Plate Coeffiec  ( $F_b$ ) ( $F_b$	ient p)	Meter or Prover Pressu psia	) <sup>2</sup> = Choo	Extension  P <sub>m</sub> xh  : ass formula 1 or 2:  1. P <sub>c</sub> <sup>2</sup> - P <sub>e</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> · P <sub>c</sub> <sup>2</sup>	Facing Fa	OW) (DELIVI	Flowing emperature Factor F <sub>11</sub> :  ERABILITY) 6 (P  Backpres Slop  Ass	CALCUL  c - 14.4) +  sure Curve e = "n" or igned	ATIONS 14.4 =	R (Mcfd)	(Cubic Fer Barrel) (P <sub>a</sub> ) <sup>2</sup>	et/ Fluid Gravity G  P = 0.207  P = Open Flow Deliverability Equals R x Antilog
Plate Coeffice  ( $F_b$ ) ( $F_b$ ) ( $F_c$	ient (,)	Meter or Prover Pressu psia	)2 = Choo	Extension  P <sub>m</sub> xh  : : :: :: :: :: :: :: :: :: :: :: ::	Facing Fa	OW) (DELIVI	Flowing emperature Factor F <sub>11</sub> :  ERABILITY) 6 (P  Backpres Slop  Ass	CALCUL  c - 14.4) + ssure Curve e = "n" or origned and Slope	ATIONS 14.4 =	R (Mcfd)	(Cubic Fer Barrel) (P <sub>a</sub> ) <sup>2</sup>	et/ Fluid Gravity G <sub>m</sub> R = 0.207 R = Open Flow Deliverability Equals R x Antilog (Mcfd)
Plate Coeffice  ( $F_b$ ) ( $F_b$ ) ( $F_c$	P <sub>3</sub> ) <sup>2</sup> P <sub>4</sub> ) <sup>2</sup> vundersig	Meter or Prover Pressurpsia  (Pw (Pc)2-(Pw)2	)2 = Choo	Extension  P <sub>m</sub> x h  :  new formula 1 or 2:  1. P <sub>c</sub> <sup>2</sup> - P <sub>e</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> - P <sub>c</sub> <sup>2</sup> ed by: P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup> Mcfd @ 14.6	Facing Fa	OW) (DELIVIE)  P.2 P.2	Flowing emperature Factor F <sub>11</sub> .  ERABILITY)  6 (P Backpres Slop Ass Standa  Deliverabile is duly aut	CALCUL  c - 14.4) + sure Curve e = "n" or or igned and Slope	ATIONS 14.4 =	R (Mcfd)	(Cubic Fer Barrel)  (P <sub>a</sub> ) <sup>2</sup> Antilog	et/ Fluid Gravity G <sub>m</sub> P = 0.207 P = Open Flow Deliverability Equals R x Antilog (Mcfd)
Plate Coeffice $(F_b)$ (F Mcfd $(F_c)^2 = \frac{(P_c)^2 - (F_c)^2}{(P_c)^2 - (F_c)^2}$	P <sub>3</sub> ) <sup>2</sup> P <sub>4</sub> ) <sup>2</sup> vundersig	Meter or Prover Pressurpsia  (P <sub>w</sub> (P <sub>o</sub> ) <sup>2</sup> - (P <sub>w</sub> ) <sup>2</sup>	)2 = Choo	Extension  P <sub>m</sub> x h  :  new formula 1 or 2:  1. P <sub>c</sub> <sup>2</sup> - P <sub>e</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> - P <sub>c</sub> <sup>2</sup> ed by: P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup> Mcfd @ 14.6	Facing Fa	OW) (DELIVIE)  P.2 P.2	Flowing emperature Factor F <sub>11</sub> .  ERABILITY)  6 (P Backpres Slop Ass Standa  Deliverabile is duly aut	CALCUL  c - 14.4) + sure Curve e = "n" or or igned and Slope	ATIONS 14.4 =	R (Mcfd)	(Cubic Fer Barrel)  (P <sub>a</sub> ) <sup>2</sup> Antilog	et/ Fluid Gravity G <sub>m</sub> P = 0.207 P = Open Flow Deliverability Equals R x Antilog (Mcfd)
Plate Coeffice $(F_b)$ (F Mcfd $(F_c)^2 = \frac{(P_c)^2 - (F_c)^2}{(P_c)^2 - (F_c)^2}$	P <sub>3</sub> ) <sup>2</sup> P <sub>4</sub> ) <sup>2</sup> vundersig	Meter or Prover Pressursia  (Pw (Po)2 - (Pw)2	chock divident	Extension  P <sub>m</sub> x h  : ase formula 1 or 2: 1. P <sub>c</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> ded by: P <sub>c</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> Mcfd @ 14.6  ehalf of the report is true	Facing Fa	OW) (DELIVIE)  P.2 P.2	Flowing emperature Factor F <sub>11</sub> .  ERABILITY)  6 (P Backpres Slop Ass Standa  Deliverabile is duly aut	CALCUL  c - 14.4) + sure Curve e = "n" or or igned and Slope	ATIONS 14.4 =	R (Mcfd)	(Cubic Fer Barrel)  (P <sub>a</sub> ) <sup>2</sup> Antilog	et/ Fluid Gravity G <sub>m</sub> P = 0.207 P = Open Flow Deliverability Equals R x Antilog (Mcfd)
Plate Coeffice  ( $F_b$ ) ( $F_c$	P <sub>3</sub> ) <sup>2</sup> P <sub>4</sub> ) <sup>2</sup> vundersig	Meter or Prover Pressursia  (Pw (Po)2 - (Pw)2	)2 = Choo	Extension  P <sub>m</sub> x h  : ase formula 1 or 2: 1. P <sub>c</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> ded by: P <sub>c</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup> Mcfd @ 14.6  ehalf of the report is true	Facing Fa	OW) (DELIVIE)  P.2 P.2	Flowing emperature Factor F <sub>11</sub> .  ERABILITY)  6 (P Backpres Slop Ass Standa  Deliverabile is duly aut	CALCUL  c - 14.4) + sure Curve e = "n" or or igned and Slope	ATIONS 14.4 =	R (Mcfd)	(Cubic Fer Barrel)  (P <sub>a</sub> ) <sup>2</sup> Antilog	et/ Fluid Gravity G <sub>m</sub> P = 0.207 P = Open Flow Deliverability Equals R x Antilog (Mcfd)

## DEC 07 2012

KCC WICHITA
I declare under penalty of perjury under the laws of the state of Kansas that I am authorized to request
exempt status under Rule K.A.R. 82-3-304 on behalf of the operator Red Hills Resources, Inc.
and that the foregoing pressure information and statements contained on this application form are true and
correct to the best of my knowledge and belief based upon available production summaries and lease records
of equipment installation and/or upon type of completion or upon use being made of the gas well herein named.
I hereby request a one-year exemption from open flow testing for the Theis C 1-34
gas well on the grounds that said well:
(Check one)
is a coalbed methane producer
is cycled on plunger lift due to water
is a source of natural gas for injection into an oil reservoir undergoing ER
is on vacuum at the present time; KCC approval Docket No.
is not capable of producing at a daily rate in excess of 250 mcf/D
I further agree to supply to the best of my ability any and all supporting documents deemed by Commission
staff as necessary to corroborate this claim for exemption from testing.
Date: 12/1/2012
Date: 12/1/2012
Signature: Wallace HM Kaply
Title: Vice- President
Httle: vice- Fresident

## Instructions:

If a gas well meets one of the eligibility criteria set out in KCC regulation K.A.R. 82-3-304, the operator may complete the statement provided above in order to claim exempt status for the gas well.

At some point during the current calendar year, wellhead shut-in pressure shall have been measured after a minimum of 24 hours shut-in/buildup time and shall be reported on the front side of this form under **OBSERVED SURFACE DATA**. Shut-in pressure shall thereafter be reported yearly in the same manner for so long as the gas well continues to meet the eligibility criterion or until the claim of eligibility for exemption **IS** denied.

The G-2 form conveying the newest shut-in pressure reading shall be filed with the Wichita office no later than December 31 of the year for which it's intended to acquire exempt status for the subject well. The form must be signed and dated on the front side as though it was a verified report of annual test results.