## KANSAS CORPORATION COMMISSION ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST

	en Flow							_				
De!	liverabilty	Test Date:				API No. 15 15-047- <b>22-25- 21,576 - 0</b> 000					0	
Company McCoy F		m Corporation				Lease Smith "E	3"		7.00		Well Number	
County Location Edwards C SW NW			Section 30		TWP 26S		RNG (E/W) 17W			Acres Attributed		
ield					Reservoir				Gas Gathering Connec			
Bordewic Completic			Kinderhook Sa Plug Back Total					Oneok Packer Set at				
0/15/08	·	W-i-t-	4677'		Diameter Set			None Perfora				
Casing Size 4-1/2"		10.5#			Internal Diameter		Set at 4723'		tions	то 4610'		
Tubing Size Weight 2-3/8" 4.7#				Internal [	Diameter		Set at Perfor		tions	То		
	pletion (	Describe)			d Production			Pump Unit Pump U		Plunger? Yes	/ No	
<u> </u>					Gas & Water % Carbon Dioxide			% Nitrogen			Gas Gravity - G <sub>g</sub>	
/ertical D	enth/H)				Proce	ure Taps				(Motor C	Run) (Prover) Size	
ertical D	epartrij				7 1633	uie iaps				(Meter 1	num (Frover) Size	
Pressure	Buildup:	Shut in	8/6 2	0 13 at 1	0:30 AM	(AM) (PM)	Taken	8/7	20	13 at 10:30	AM (AM) (PM)	
Vell on Li	ine:	Started	20	) at		(AM) (PM)	Taken		20	at	(AM) (PM)	
					OBSERVE	D SURFACE	DATA			Duration of Shut-	in 24 Hou	
Static /	Orifice	Circle ane: Meter	Pressure Differential	Flowing	Well Head	Casing Wellhead Pressure		Tubing Wellhead Pressure		Duration	Liquid Produced	
Oynamic Property	Size (inches)	Prover Pressure		Temperature t	Temperature t	(P <sub>w</sub> ) or (P <sub>t</sub>		(P <sub>w</sub> ) or (P <sub>t</sub> ) or (P <sub>c</sub> )		(Hours)	(Barrels)	
Shut-In						125#	poid	parg	раш	24		
Flow												
				· · · · · · · -	FLOW STR	EAM ATTRI	BUTES	·			- , .	
		Circle one: Meter at	Eutonoine		vity tor	emperature		oviation Metered Flor		y GOR (Cubic Fe	Flowing Fluid	
Plate Coeffieci						Factor F <sub>t1</sub>				(00000.00		
	,)   f	Prover Pressure psia	√ P <sub>m</sub> xh	F	,		1	pv	(Mcfd)	Barrel)	Gravity G <sub>m</sub>	
Coefficie (F <sub>b</sub> ) (F <sub>p</sub>	,)   f	Prover Pressure		F			1	pv		Barrel)	Gravity	
Coefficie (F <sub>b</sub> ) (F <sub>p</sub>	,)   f	Prover Pressure			OW) (DELIVI	F,	F				Gravity	
Coefficie (F <sub>b</sub> ) (F <sub>p</sub>	,)   f	Prover Pressure psia  (P_w)² =	✓ P <sub>m</sub> xh	(OPEN FLO		F <sub>ti</sub> ERABILITY) 6 (P	CALCUL	ATIONS 14.4 =	(Mcfd)		Gravity G <sub>m</sub> 2 = 0.207	
Coefficial $(F_b) (F_p) (F_p) (F_p)^2 = \frac{(P_p)^2 - (P_p)^2}{\sigma}$	·) F	Prover Pressure psia  (P_w)² =	P <sub>m</sub> x h  : naose formula 1 or 2:  1. P <sub>c</sub> <sup>2</sup> - P <sub>a</sub> <sup>2</sup>	(OPEN FLO	OW) (DELIVI	F <sub>f1</sub> ERABILITY)  6 (P  Backpres Slop	CALCUL	ATIONS 14.4 =	(Mcfd)	(P <sub>a</sub> ):	Gravity G <sub>m</sub> 2 = 0.207 2 = Open Flow Deliverability	
Coefficial (F <sub>b</sub> ) (F <sub>p</sub> Modd	·) F	(P <sub>w</sub> ) <sup>2</sup> =	P <sub>m</sub> x h	(OPEN FL)  P <sub>d</sub> =  LOG of formula 1. or 2. and divide	OW) (DELIVI	ERABILITY) 6 (P Backpres	CALCUL  c - 14.4) + sure Curve e = "n"	ATIONS 14.4 =	(Mcfd)	(P <sub>a</sub> )	Gravity G <sub>m</sub> 2 = 0.207 2 = Open Flow	
Coefficial $(F_b) (F_p) (F_p) (F_p)^2 = \frac{(P_p)^2 - (P_p)^2}{\sigma}$	·) F	(P <sub>w</sub> ) <sup>2</sup> =	: :: :: :: :: :: :: :: :: :: :: :: :: :	(OPEN FL)  P <sub>d</sub> =  LOG of formula 1. or 2. and divide	DW) (DELIVI	ERABILITY) 6 (P Backpres	CALCUL  c - 14.4) + ssure Curve e = "n" ar aigned	ATIONS 14.4 =	(Mcfd)	(P <sub>a</sub> ):	Gravity G <sub>m</sub> 2 = 0.207 2 =  Open Flow Deliverability Equals R x Antilog	
Coefficial $(F_b) (F_p) (F_p) (F_p)^2 = \frac{(P_p)^2 - (P_p)^2}{\sigma}$	·) F	(P <sub>w</sub> ) <sup>2</sup> =	: :: :: :: :: :: :: :: :: :: :: :: :: :	(OPEN FL)  P <sub>d</sub> =  LOG of formula 1. or 2. and divide	DW) (DELIVI	ERABILITY) 6 (P Backpres	CALCUL  c - 14.4) + ssure Curve e = "n" ar aigned	ATIONS 14.4 =	(Mcfd)	(P <sub>a</sub> ):	Gravity G <sub>m</sub> 2 = 0.207 2 =  Open Flow Deliverability Equals R x Antilog	
Coefficial $(F_b) (F_p) (F_p) (F_p)^2 = \frac{(P_p)^2 - (P_p)^2}{\sigma}$		(P <sub>w</sub> ) <sup>2</sup> =	: :: :: :: :: :: :: :: :: :: :: :: :: :	(OPEN FLO P <sub>d</sub> = LOG of formula 1. or 2. and divide by:	DW) (DELIVI	ERABILITY) 6 (P Backpres	CALCUL  c - 14.4) + sure Curve e = "n" or iigned and Slope	ATIONS 14.4 =	(Mcfd)	(P <sub>a</sub> ):	Gravity G <sub>m</sub> 2 = 0.207 2 =  Open Flow Deliverability Equals R x Antilo (Mcfd)	
Coefficci $(F_b)(F_p)$ Modd $P_c)^2 = \frac{P_c}{(P_c)^2 - (P_c)^2}$ Open Flow		Prover Pressure psia  (P_v)^2 = (P_c)^2 - (P_v)^2	P <sub>m</sub> x h  : naose formula 1 or 2:  1. P <sub>c</sub> <sup>2</sup> - P <sub>c</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> - P <sub>c</sub> <sup>2</sup> //ded by: P <sub>c</sub> <sup>2</sup> - P <sub>c</sub> <sup>2</sup> Mcfd @ 14.1	(OPEN FLO P <sub>d</sub> = LOG of formula 1. or 2 and divide by:	P <sub>c</sub> <sup>2</sup> - P <sub>*</sub> <sup>2</sup>	F <sub>II</sub> ERABILITY)  6 (P  Backpres Slop  Ass Standa  Deliverabi e is duly au	CALCUL c - 14.4) + sure Curve e = "n" or igned and Slope	ATIONS  14.4 =  n x LO	(Mcfd)	(P <sub>a</sub> ) <sup>2</sup> (P <sub>d</sub> ) <sup>2</sup> Antilog	Gravity G <sub>m</sub> 2 = 0.207 2 = Open Flow Deliverability Equals R x Antilog (Mcfd)	
Coeffication ( $F_b$ ) ( $F_p$ ) ( $F_p$ ) ( $F_p$ ) Mode $F_p$ ) ( $F_p$ ) $F_p$	· · · · · · · · · · · · · · · · · · ·	Prover Pressure psia  (P_v)^2 = (P_c)^2 - (P_v)^2	P <sub>m</sub> x h  : noose formula 1 or 2:  1. P <sub>c</sub> <sup>2</sup> - P <sub>c</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> - P <sub>c</sub> <sup>2</sup> Mcfd @ 14.1  behalf of the	(OPEN FLOG of tormula 1. or 2. and divide by:	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	F <sub>11</sub> ERABILITY)  6 (P  Backpres Stop  Ass Standa  Deliverabi e is duly au	CALCUL c - 14.4) + sure Curve e = "n" or igned and Slope	ATIONS  14.4 =	(Mcfd)	(P <sub>a</sub> ) <sup>2</sup> (P <sub>d</sub> )  Antilog  Mctd @ 14.65 psi	Gravity G <sub>m</sub> 2 = 0.207 2 = Open Flow Deliverability Equats R x Antilog (Mcfd)	
Coeffication ( $F_b$ ) ( $F_p$ ) ( $F_p$ ) ( $F_p$ ) Mode $F_p$ ) ( $F_p$ ) $F_p$	· · · · · · · · · · · · · · · · · · ·	Prover Pressure psia $(P_{w})^{2} = \underline{\qquad}$ $(P_{e})^{2} - (P_{w})^{2}$ $dn$ ed authority, on	P <sub>m</sub> x h  : noose formula 1 or 2:  1. P <sub>c</sub> <sup>2</sup> - P <sub>c</sub> <sup>2</sup> 2. P <sub>c</sub> <sup>2</sup> - P <sub>c</sub> <sup>2</sup> Mcfd @ 14.1  behalf of the	(OPEN FLOG of tormula 1. or 2. and divide by:	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	F <sub>11</sub> ERABILITY)  6 (P  Backpres Stop  Ass Standa  Deliverabi e is duly au	CALCUL c - 14.4) + sure Curve e = "n" or igned and Slope	ATIONS  14.4 =  n x LO	(Mcfd)	(P <sub>a</sub> ) <sup>2</sup> (P <sub>d</sub> )  Antilog  Mctd @ 14.65 psi	Gravity G <sub>m</sub> 2 = 0.207 2 = Open Flow Deliverability Equals R x Antilon (Mcfd)	

	eclare under penalty of perjury under the laws of the state of Kansas that I am authorized to request status under Rule K.A.R. 82-3-304 on behalf of the operator McCoy Petroleum Corporation
	at the foregoing pressure information and statements contained on this application form are true and
	to the best of my knowledge and belief based upon available production summaries and lease records
of equip	oment installation and/or upon type of completion or upon use being made of the gas well herein named.  ereby request a one-year exemption from open flow testing for the Smith "B" #1-30
	Il on the grounds that said well:
staff as	is a coalbed methane producer is cycled on plunger lift due to water is a source of natural gas for injection into an oil reservoir undergoing ER is on vacuum at the present time; KCC approval Docket No.  is not capable of producing at a daily rate in excess of 250 mcf/D  rther agree to supply to the best of my ability any and all supporting documents deemed by Commission necessary to corroborate this claim for exemption from testing.
	Signature: Signature: Vice President - Production

Instructions:

If a gas well meets one of the eligibility criteria set out in KCC regulation K.A.R. 82-3-304, the operator may complete the statement provided above in order to claim exempt status for the gas well.

At some point during the current calendar year, wellhead shut-in pressure shall have been measured after a minimum of 24 hours shut-in/buildup time and shall be reported on the front side of this form under **OBSERVED SURFACE DATA**. Shut-in pressure shall thereafter be reported yearly in the same manner for so long as the gas well continues to meet the eligibility criterion or until the claim of eligibility for exemption **IS** denied.

The G-2 form conveying the newest shut-in pressure reading shall be filed with the Wichita office no later than December 31 of the year for which it's intended to acquire exempt status for the subject well. The form must be signed and dated on the front side as though it was a verified report of annual test results.

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