

**KANSAS CORPORATION COMMISSION  
ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST**

FORM G-2  
(Rev. 8/88)

TYPE TEST:

- Open Flow  
 Deliverability

TEST DATE: 9/13/2013

API No. 16-057-20761-00-00

Company Ritche Exploration		Lease Pinkney-Rohr			Well Number 1	
County Ford	Location 1210' FNL 907'	Section 8	TWP 28s	RNG (E/W) 22W	Acrees Attributed	
Field	Reservoir Miss	Gas Gathering Connection <b>Ford Gathering System, LLC</b>				
Completion Date 11/7/2011	Plug Back Total Depth 5098	Packer Set at none				
Casing Size 4.500	Weight 10.600	Internal Diameter 4.052	Set at 516'	Perforations 5022	To 5038	
Tubing Size 2.375	Weight 4.700	Internal Diameter 1.995	Set at 5024	Perforations To		
Type Completion (Describe) perf-aoid	Type Fluid Production	Pump Unit or Traveling Plunger? no				
Producing thru (Annulus/Tubing) tubing	% Carbon Dioxide 0.012	% Nitrogen 9.588		Gas Gravity- Gg 0.659		
Vertical Depth (ft) 6030	Pressure Taps flange	Meter Run Size 3.068				
Pressure Buildup: Shut in	9/9/2013 @ 1000	TAKEN	9/12/2013 @ 1000			
Well on Line: Started	9/12/2013 @ 1000	TAKEN	9/13/2013 @ 1000			

**OBSERVED SURFACE DATA**

Static/ Dynamic Property	Orifice Size in.	Meter Pressure psig	Pressure Diff. In. H <sub>2</sub> O	Flowing Temp. t.	Wellhead Temp. t.	Casing Wellhead Press. (P <sub>w</sub> ) (P <sub>c</sub> ) (P <sub>o</sub> )		Tubing Wellhead Press. (P <sub>w</sub> ) (P <sub>c</sub> ) (P <sub>o</sub> )		Duration (Hours)	Liquid Prod. Barrels
						psig	psia	psig	psia		
Shut-in						485	479	440	454	72.0	
Flow	0.500	31.9	53.60	58		35	49	35	49	24.0	

**FLOW STREAM ATTRIBUTES**

COEFFICIENT (F <sub>b</sub> ) Modd	(METER) PRESSURE psia	EXTENSION $\sqrt{P_m \times R_w}$	GRAVITY FACTOR F <sub>g</sub>	FLOWING TEMP FACTOR F <sub>t</sub>	DEVIATION FACTOR F <sub>pv</sub>	RATE OF FLOW R Modd	GOR	G <sub>n</sub>
1.214	46.3	49.82	1.2318	1.0019	1.0038	74		0.659

**(OPEN FLOW)(DELIVERABILITY) CALCULATIONS**

(P<sub>o</sub>)<sup>2</sup> = 229.8      (P<sub>w</sub>)<sup>2</sup> = 2.4      P<sub>d</sub> = 6.7      (P<sub>c</sub> - 14.4) + 14.4 =      (P<sub>a</sub>)<sup>2</sup> = 0.207  
(P<sub>d</sub>)<sup>2</sup> = 1.02

$(P_o)^2 - (P_w)^2$ or $(P_o)^2 - (P_d)^2$	$(P_o)^2 - (P_w)^2$	$\frac{(P_o)^2 - (P_w)^2}{(P_o)^2 - (P_d)^2}$ or $\frac{(P_o)^2 - (P_w)^2}{(P_o)^2 - (P_w)^2}$	100	Backpressure Curve Slope "n" or Assigned Standard Slope	n x 100	Antilog	Open Flow Deliverability = R x Antilog Modd
229.62	227.38	1.010	0.0042	0.850	0.0036	1.008	75
228.81	227.38	1.008	0.0027	0.850	0.0023	1.005	75

**OPEN FLOW**                      75                      Modd @ 14.65 psia                      **DELIVERABILITY**                      75                      Modd @ 14.65 psia

The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated herein and that said report is true and correct. Executed this the \_\_\_\_\_ day of \_\_\_\_\_, 20\_\_\_\_

\_\_\_\_\_  
Witness (if any)

\_\_\_\_\_  
For Commission

\_\_\_\_\_  
For Company

\_\_\_\_\_  
Checked by