

KANSAS CORPORATION COMMISSION  
 ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST

FORM G-2  
 (Rev. 8/98)

TYPE TEST:

- Open Flow  
 Deliverability

TEST DATE: 4/26/2016 API No. 15-025-21440-0000

Company R&B Oil & Gas		Lease Birney			Well Number 11-3-3	
County Clark	Location NE SW NE N		Section 11	TWP 31s	RNG (E/W) 2	Acres Attributed 40
Field Calvary Creek		Reservoir Iona	Gas Gathering Connection DCP			
Completion Date 10/8/2015		Plug Back Total Depth 5272		Packer Set at 5150		
Casing Size 4.500	Weight 10.500	Internal Diameter 4.052	Set at 6345	Perforations 5171	To 5176	
Tubing Size 2.375	Weight 4.700	Internal Diameter 1.995	Set at 5168	Perforations 5163	To 5164	
Type Completion (Describe) workover		Type Fluid Production water		Pump Unit or Traveling Plunger? no		
Producing Thru (Annulus/Tubing) tubing		% Carbon Dioxide 0.086		% Nitrogen 8.418		Gas Gravity- Gg 0.652
Vertical Depth (H) 5173		Pressure Taps flange			Meter Run Size 3.068	
Pressure Buildup: Shut in		4/22/2016@0900		TAKEN	4/25/2016@0900	
Well on Line: Started		4/25/2016@0900		TAKEN	4/27/2016@0900	

OBSERVED SURFACE DATA

Static/ Dynamic Property	Orifice Size in.	Meter Pressure psig	Pressure Diff. In. H <sub>2</sub> O	Flowing Temp. t.	WellHead Temp. t.	Casing WellHead Press. (P <sub>w</sub> ) (P <sub>d</sub> ) (P <sub>c</sub> )		Tubing WellHead Press. (P <sub>w</sub> ) (P <sub>d</sub> ) (P <sub>c</sub> )		Duration (Hours)	Liquic Prod Barrel
						psig	psia	psig	psia		
Shut-in								855	869	72.0	
Flow	1.500	33.2	8.80	67	60			707	721	27.0	

FLOW STREAM ATTRIBUTES

COEFFICIENT (F <sub>b</sub> ) Mcf/d	(METER) PRESSURE psia	EXTENSION $\sqrt{P_m \times H_w}$	GRAVITY FACTOR Fg	FLOWING TEMP FACTOR Ft	DEVIATION FACTOR Fpv	RATE OF FLOW R Mcf/d	GOR	G <sub>m</sub>
14.410	47.6	20.47	1.2384	0.9933	1.0035	364		0.652

(OPEN FLOW)(DELIVERABILITY) CALCULATIONS

(P<sub>c</sub>)<sup>2</sup> = 755.9      (P<sub>w</sub>)<sup>2</sup> = 523.6      P<sub>d</sub> = 3.8      %      (P<sub>c</sub> - 14.4) + 14.4 =      (P<sub>a</sub>)<sup>2</sup> = 0.207  
 (P<sub>d</sub>)<sup>2</sup> = 1.10

$(P_c)^2 - (P_a)^2$ or $(P_c)^2 - (P_d)^2$	$(P_c)^2 - (P_w)^2$	$\frac{(P_c)^2 - (P_a)^2}{(P_c)^2 - (P_d)^2}$ or $\frac{(P_c)^2 - (P_a)^2}{(P_c)^2 - (P_w)^2}$	LOG	Backpressure Curve Slope "n" ----- or ----- Assigned Standard Slope	n x LOG	Antilog	Open Flow Deliverability = R x Antilog Mcf/d
755.65	232.24	3.254	0.5124	0.924	0.4734	2.975	1083
754.75	232.24	3.250	0.5119	0.924	0.4730	2.971	1081

OPEN FLOW 1083 Mcfd @ 14.65 psia      DELIVERABILITY 1081 Mcfd @ 14.65 psia

The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated herein and that said report is true and correct. Executed this the 5 day of May, 2016

Witness (if any) \_\_\_\_\_  
 For Commission \_\_\_\_\_  
 Received KANSAS CORPORATION COMMISSION  
 MAY 10 2016  
 CONSERVATION DIVISION  
 WICHITA, KS  
 For Company \_\_\_\_\_  
 Checked by \_\_\_\_\_