

**KANSAS CORPORATION COMMISSION  
ONE POINT STABILIZED OPEN FLOW OR DELIVERABILITY TEST**

FORM G-2  
(Rev.8/98)

TYPE TEST:

- Open Flow  
 Deliverability

TEST DATE: 4/7/2018 API No. 5-007-24321-0000

Company Lotus Operating		Lease Charlie		Well Number 1	
County Barber	Location S/2 SW SW	Section 11	TWP 35	RNG (E/W) 13w	Acres Attributed 320
Field Stranathan-Hart		Reservoir Mississippi		Gas Gathering Connection ONEOK	
Completion Date 9/1/2017		Plug Back Total Depth 5118		Packer Set at none	
Casing Size 5.500	Weight 17.000	Internal Diameter 4.892	Set at 5157	Perforations 4852	To 4888
Tubing Size 2.875	Weight 6.500	Internal Diameter 2.441	Set at 4930	Perforations To	
Type Completion (Describe) Acid-Frac		Type Fluid Production oil-water		Pump Unit or Traveling Plunger? pumping unit	
Producing Thru (Annulus/Tubing) annulus		% Carbon Dioxide 0.116		% Nitrogen 1.197	
Vertical Depth (H) 4870		Pressure Taps flange		Meter Run Size 2.067	
Pressure Buildup: Shut in 4/3/2018@0800		TAKEN 4/6/2018@0800			
Well on Line: Started 4/6/2018@0800		TAKEN 4/7/2018@0945			

**OBSERVED SURFACE DATA**

Static/ Dynamic Property	Orifice Size in.	Meter Pressure psig	Pressure Diff. In. H <sub>2</sub> O	Flowing Temp. t.	WellHead Temp. t.	Casing WellHead Press. (P <sub>w</sub> ) (P <sub>t</sub> ) (P <sub>c</sub> )		Tubing WellHead Press. (P <sub>w</sub> ) (P <sub>t</sub> ) (P <sub>c</sub> )		Duration (Hours)	Liquid Prod. Barrels
						psig	psia	psig	psia		
Shut-in						443	457			72.0	
Flow	1.500	29.1	24.00	33	40	328	342			25.7	60.0

**FLOW STREAM ATTRIBUTES**

COEFFICIENT (F <sub>b</sub> ) Mcf/d	(METER) PRESSURE psia	EXTENSION $\sqrt{P_m \times H_w}$	GRAVITY FACTOR F <sub>g</sub>	FLOWING TEMP FACTOR F <sub>t</sub>	DEVIATION FACTOR F <sub>pv</sub>	RATE OF FLOW R Mcf/d	GOR	G <sub>m</sub>
11.410	43.5	32.31	1.2669	1.0270	1.0043	481	8598	1.059

**(OPEN FLOW)(DELIVERABILITY) CALCULATIONS**

(P<sub>c</sub>)<sup>2</sup> = 209.2      (P<sub>w</sub>)<sup>2</sup> = 117.7      P<sub>d</sub> = 6.4      %      (P<sub>c</sub> - 14.4) + 14.4 =      (P<sub>a</sub>)<sup>2</sup> = 0.207  
(P<sub>d</sub>)<sup>2</sup> = 0.85

$(P_c)^2 - (P_a)^2$ or $(P_c)^2 - (P_d)^2$	$(P_c)^2 - (P_w)^2$	$\frac{(P_c)^2 - (P_a)^2}{(P_c)^2 - (P_d)^2}$ or $\frac{(P_c)^2 - (P_a)^2}{(P_c)^2 - (P_w)^2}$	LOG	Backpressure Curve Slope "n" or Assigned Standard Slope	n x LOG	Antilog	Open Flow Deliverability = R x Antilog Mcf/d
209.01	91.50	2.284	0.3588	0.633	0.2271	1.687	812
208.37	91.50	2.277	0.3574	0.633	0.2263	1.684	811

OPEN FLOW      812      Mcfd @ 14.65 psia      DELIVERABILITY      811      Mcfd @ 14.65 psia

The undersigned authority, on behalf of the Company, states that he is duly authorized to make the above report and that he has knowledge of the facts stated herein and that said report is true and correct. Executed this the 12 day of April, 2018

Witness (if any) \_\_\_\_\_ Received \_\_\_\_\_ For Company \_\_\_\_\_  
For Commission \_\_\_\_\_

APR 17 2018  
DIVISION CONSERVATION DIVISION  
MICHITA, KS  
4-17-18